Pick an instrument for your task. Want one that can diagnose and calibrate itself? Or the one that combines several functions? How about the new breed of battery powered types that match power efficiency with portability? Do you require an instrument that won’t hurt other equipment or you. For more details, see p. 50.
Now in the only full line of super low profile SIP Resistor Networks.

If you haven’t designed in Single In-line Package resistor networks because of their high profile, take another look. THE HEIGHT ON BOURNS SIPs IS ONLY .190 INCH! And that’s standard for all 6, 8 and 10 pin configurations with:

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It gives you 7 function generator waveforms over a frequency range of 0.0001 Hz to 13 MHz. It’s GPIB compatible, has a microprocessor-controlled interface, plus a 5½-digit synthesizer option.

We’ll give you more details in the next installment. Meanwhile, circle the inquiry card or contact us direct. Wavetek, P.O. Box 651, San Diego, CA 92112. Phone (714) 279-2200. Or TWX 910-335-2007.
We invite you to convince yourself... place your order now and check our product performance, reliability and delivery... at the lowest prices!

For complete specs, performance curves and drawings, see pgs 151-303 of the 1976-77 Microwaves Product Data Directory.
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Cover: Cover designed by Art Director, Bill Kelly.

The dream of design engineers is to develop, debug, and integrate hardware and software in their actual product environment—from day one. Thereby dramatically shortening the development time—and development cost—of their microcomputer-based products.

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With ICE-80 and ICE-30 Intellec's in-circuit emulation modules, you exercise your complete hardware/software prototype under control of high level diagnostic software. ICE-80 plugs into the 8080 socket in your prototype system and runs it in real time. Under Intellec system control, you single-step your system program, using Intellec's memory and I/O as though they were part of the prototype system. Powerful debug functions are extended into your system and you can examine or modify your system memory or Intellec memory using symbolic references instead of machine addresses.
lets you see what your it's still on the bench.

The Intellec system includes its own 8080 processor, memory, and a full range of peripherals designed to ease your development task. These include diskette operating system, CRT/keyboard, line printer, universal PROM programmer, high speed papertape reader, the in-circuit emulation modules, (ICE-80 and ICE-30) and interfaces for teletypewriter and high speed tape punch.

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intell
Microcomputers. First from the beginning.
Tucked in the corner of this Pulsar Watch is a miniature capacitor which is used to trim the crystal. This Thin-Trim capacitor is one of our 9410 series, has an adjustable range of 7 to 45 pf, and is .200" x .200" x .050" thick.

The Thin-Trim concept provides a variable device to replace fixed tuning techniques and cut-and-try methods of adjustment. Thin-Trim capacitors are available in a variety of lead configurations making them easy to mount.

A smaller version of the 9410 is the 9402 series with a maximum capacitance value of 25 pf. These are perfect for applications in sub-miniature circuits such as ladies' electronic wrist watches and phased array MIC's.
Wolfe's Law

Buried deep in some secluded mountain cave, there must be an archive where silent monks guard the profundities of our industry. This is where one should find Murphy's Law (if anything can go wrong, it will) and its corollaries. Here, too, one should find Wolfe's Law, propounded by the Vice-President of Gould Inc. and General Manager of the Centralab Electronics Div. Those less versed in the philosophical underpinnings of our industry should know that Wolfe's Law states that: "It requires more effort to change something than not to change it."

The principal corollaries belabor the obvious:
- The effort expended by the person who wants to change something is the square of the effort expended by the person who doesn't want it changed.
- Success is inversely proportional to resistance.

Engineers, wake up: You are being raped

Recently, it seems, we have been deluged with a flood of Engineering Design Contests. There have been Microprocessor Contests, FPLA Contests, PLL Contests, etc. At first glance, these contests would seem to be a way for the engineer to exercise some creativity, while possibly winning a prize for his efforts. In reality, they are a great rip-off of the working engineer.

Who benefits from these contests? Clearly, only the contest sponsor. The sponsor gains in three ways. First, he obtains—at virtually no cost—an enormous library of applications data. Second, those engineers submitting contest entries are more likely to use the sponsor's product than the product of a competitor. Third, the sponsor can now attract even more business because he can provide a great wealth of applications literature.

The engineer is getting raped and doesn't realize it. If the engineer charged a consulting fee for the effort that goes into a contest entry, he would likely do better than if he had won first prize. Yet the chance of "getting something for nothing" is enticing engineers to give away their services.

This brain picking would never work in any other profession. Imagine a large law firm asking independent lawyers to prepare a brief on a pending case. The lawyer who prepares the best brief wins a calculator.

Or think of a pharmaceutical company asking doctors to develop a new drug. The best one wins a trip to Florida. How insane that engineers don't realize that these so-called contests amount to the same thing.

If engineers are ever to obtain a truly professional status, they must start acting like professionals and stop giving away their services.

Alan Rosenbaum
Manager of Computer Products
General Microwave Corp.
155 Marine St.
Farmingdale, NY 11735

You want to be better, I want you to be better

I was intrigued by your editorial, "We Want to Be Better" (ED No. 17, August 16, 1976, p. 59), in... (continued on page 11)
The only microcomputer with the power of a PDP-11. The PDP-11/03.

If you've been looking for a microcomputer with minicomputer power at a micro price, join the hundreds of OEMs who've already found it with the DIGITAL microcomputer. The PDP-11/03.

The 11/03 gives you everything you could ask for in a small computer. High performance. High reliability. And a low price — just $1,357 in quantities of 50. And that micro price buys you mini features that quickly translate into benefits OEMs appreciate. Features like full PDP-11 instructions with eight general purpose registers for fast program development. RAM (MOS or Core) and PROM memories that let you match the memory with the application. Hardware vectored interrupts with stack processing for real computer power. And multiple-sourced components for sure delivery.

Buying our 11/03 also buys you the chance to start small without staying small. Because you can add up to 32K words of memory, fast floating point instructions, and more. Whenever you and your customers are ready.

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You can also take advantage of Digital's OEM Referral program — your chance to take on an international marketing and support team without hiring them. The OEM Referral program can help you locate new custom-
ers and new markets around town and around the world. And it can all start with the PDP-11/03. So if you’re looking for a proven microcomputer with proven power and performance, get the micro with all the power and performance of a PDP-11.

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CIRCLE NUMBER 8
which you stressed that ED, unlike some of its competitors, admits to its editorial gaffs. Such honesty is commendable and certainly reinforces the reader's faith in your fine publication.

I wish to call attention to the article on CRTs in the same issue. Your editor wrote, "Almost as diverse a selection of CRTs is available from RCA's Industrial Tube Div., Lancaster, PA, and RCA's Electronic Components Div., Harrison, NJ." Historically, that statement would have been redundant since the Industrial Tube Division in Lancaster was a part of Electronic Components, headquartered in Harrison. But in March 1975, when RCA reorganized its Electronic Components activity, the Industrial Tube organization became an integral part of RCA Electro-Optics and Devices, now an organizational entity within the Solid State Division. It is therefore proper to identify RCA Electro-Optics and Devices, Lancaster, PA, as the CRT supplier.

Walter B. Dennen
Manager, News and Information
RCA
Solid State Division
Route 202
Somerville, NJ 08876

Charlie and Clarence, and Clark and Jack

You may have had a good reason to oversimplify the concept of modern management in your "Scientific Management" editorial (ED No. 18, September 1, 1976, p. 61)—possibly to make a point with a specific segment of your readers. However, I'd appreciate equal time for the other viewpoint.

My position is Senior Engineer. Contrary to the flavor of your editorial, my preference, as a worker, would be the modern concepts. These include extensive group interaction, group participation in management decision making, self-scheduling and personal development.

A manager who claims to use the latest tools, but in fact is using only the latest bookkeeping methods, does not merit the manage-

The management team I work for claims to be from the modern school. Nevertheless, the work is done without planning, production-line style, open door policy "with authorization," and one-way communication with the single goal of keeping the boss out of trouble. All the management books I've read place this philosophy in the old school.

Concerning your editorial specifically, you refer to "Charlie" as responsible for his staff, running things smoothly, getting things done and using the best tools. "Clarence" on the other hand is a production pusher with computer-generated numbers to prove his point.

If you would play engineer for a while and list side by side the comparative philosophies from the old and new schools, theory X vs theory Y, oldest vs latest tools, your own management articles possibly, I think you'd find yourself forced to put Clarence in the old school sporting some fancy new gadgets. Charlie would also be old-school.

If you want to meet a new schooler, look at Clarence's replacement, "Clark." who spent the first 2 weeks getting to know his staff, meeting their families, outlining their future objectives, organizing their likes, dislikes, observations, ideas. Clark identified "Chuck" as the group's self-appointed spokesman and asked him to help organize the group's ideas into working projects to iron out any bugs. Production was in fact down because so much time was being devoted to organization and meetings.

Within a week, Clark came to see Jack with a list of things to discuss. Unfortunately, each item had a price tag, some quite high, at a bad time in the economy. But unlike other VPs, Jack was determined to back his middle managers as far as he could until they either could handle the rope themselves or hang from it. After the proposed machine modifications were made, production began at 2000 subassemblies a day with 5 rejects. A week of fine timing brought that to 2500 and usually 1 reject a week. And despite the apparent radical appearance of the get together, Jack himself showed up at the bowling alley to pass out

(continued on page 16)
1100 YEARS FROM NOW, YOU'LL STILL BE GLAD YOU BOUGHT OUR MEMORIES.

Eleven hundred years from now, our semiconductor memories will still be going strong.

Because right now we’re selling MOS memories with MTBFs per device of from 5 to 10 million hours. Which is well over 1100 years.

Our bipolar memories, on the other hand, will last a few centuries longer. Their MTBFs go up to 14 million hours.

And if you think these terrific figures are just wild claims like you’re used to seeing in semiconductor advertising, you probably haven’t heard about how we spec our products: in a word, conservatively.

Of course, all this industry-leading reliability wouldn’t mean very much if we didn’t deliver it in the kind of state-of-the-art products you need.

But we do.

We sell a comprehensive line of memories that includes everything from a family of 4K MOS RAMs with access times down to 135ns, to the industry’s first 2K EEPROM that can match the requirements of microprogrammed control applications.

For the full story, just contact one of our reps or distributors.

Preferably within the current millennium.

NEC Microcomputers, Inc., Five Militia Drive, Lexington, MA 02173. 617-862-6410.
Until now, if you needed a high performance timer/counter with all the capabilities and versatility of a lab instrument, you expected a high price. That is, unless you could do without time interval averaging capabilities or if you could get by without trigger hold-off or if you could compromise on triggering capabilities or if you didn’t mind the shortcomings of a plastic case. But, that’s the way it was with timer/counters. Today, our new PM 6620 series offers performance without compromise in a compact, package at compact prices.

All three models provide for:
- 80 MHz direct frequency counting
- Single shot period and time interval measurements with 100 ns resolution
- Period and time interval averaging over $10^2$, $10^3$, or $10^6$ intervals
- Ratio and conditional pulse counting
- Comprehensive trigger facilities with accurate trigger level setting.

But that's not all! Depending on your individual needs, select one of three models:
- PM 6622 with trigger hold-off for even more versatile T.I. measurements
- PM 6624 with 520 MHz frequency range
- PM 6625 with 1000 MHz frequency range

And it doesn't end there! Each model is available with either of four time base oscillators, BCD, IEEE Bus or analog output options, internal battery/charger, single or dual rack mounts and more.

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Our newest air variable capacitor's biggest feature:

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As you can plainly see, our new air variable capacitor is nearly as small as many sub-miniature ceramic trimmers. It also features the same mounting configuration which means you can use it in many of the same applications. But small size isn't the only reason for buying our new Micro T capacitor. Because it's air variable, it offers you great stability. Q is typically 1000 at 100 MHz. TC is +45±45 PPM/°C. And it's available in maximum capacities of 3, 6.5, 12.7, and 19.0 pF in either vertical or horizontal tuning PC and stripline mounting versions. What's more, it gives you all this for a very small price.

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ACROSS THE DESK

(continued from page 11)

various awards, a few bonuses to exceptional idea people and offer the entire group one extra week of paid vacation. In six months, Chuck took over as supervisor and Clark became manager of systems engineering.

Come on, George, sign up for some courses in the new school. We don't discriminate against old timers, nor do we believe that old gods can't learn some and contribute some. Just beware of the pseudo-new schoolers.

Bruce Nappi

Misplaced Caption Dept.

My company won't let us fly first class anymore.

Sorry. That's Honoré Daumier's "Third Class Carriage," which hangs in the Metropolitan Museum of Art in New York City.

And it tasted great

I am trying to locate a source for a product I used several years ago. It consisted of a chemical powder, which, when applied with a dampened cloth to bare clean copper, would deposit a plating on the copper similar to a finely tinned surface.

I vaguely recall a name like AMP-ON, but I am not certain. If you can advise me as to the best way to track down such a product, it will be greatly appreciated. Thank you.

Peter J. Farrell
Sperry Engineer

60 Elliot Ave.
Centereach, NY 11720
Somewhere Issaquah will be famous.

Someday, people will say, "Issaquah, Washington, that's the home of Data I/O!"

But that's "somewhere." Today, more people remember us for our PROM programmers than for our name. We understand. After all, the 1500 companies who use our machines need programmers—not a name. So here's what's behind "Data I/O:"

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Our Programmer VI lets you program from one to eight MOS PROMs simultaneously with the same, or different programs. (It can program an entire memory board in less than 30 seconds.)

Our new Programmer VIII is a completely portable, microprocessor-based unit. You can take it anywhere and easily update it year after year.

Our Programmer X is for Programmable Logic Arrays (PLA's). It features CRT display, multiple inputs and outputs, and error detection through both logical and array verification. It's also microprocessor based.

Our Romulator lets you emulate any PROM configuration on the market today, develop a complete program and debug it before you ever have to commit it to a PROM.

Data I/O offers a unique calibration standard which lets you calibrate to each PROM manufacturer's specs—before you program—for maximum yields and long term I-C reliability.

Data I/O total three point service
1. Every Data I/O customer receives a quarterly update on currently available PROMs.
2. Through our direct (computerized) mailing program, Data I/O customers are kept constantly up-to-date on PROM specification changes and technological innovations.
3. Nine field offices in the U.S. and 22 distributors worldwide provide our customers with direct sales support, installation, and operator training.

Get the facts...

If you would like to know more about our products or want copies of our quarterly PROM Comparison Chart and PROMBITS (our periodic technical bulletin on PROM applications and innovations), mail this coupon or call one of our offices. Data I/O Corporation, P.O. Box 308, Issaquah, Washington 98027.

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CIRCLE NUMBER 14

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data domain.
Biomation’s new logic analyzers give you both.

When your job is to interface, integrate and program a complex new digital logic system, you want as much information as you can get.

That’s why we’re providing a new set of tools which let you display timing information as well as logic word content—in the language of your choice.

Our new 1650-D logic analyzer gives you 16 channels at 50MHz. Our 851-D gives you 8 channels at the same speed. Accessories can now give you a logic state (1’s and 0’s) display of any 16 stored words; hex or octal translation; and a vector map of memory contents. The 8 and 16-channel logic analyzers feature:

- Pretrigger and delayed trigger recording
- Trigger point can be easily identified
- Latch record mode for fast pulse capture
- Combinational triggering (true or false)
- Movable display cursor that stays with the data when you switch display modes
- Display expansion, mixed or full, X5, X10 or X20

These are complex instruments and we can’t give you all significant details here. But please write, call, or use the reader service card. We want to get this useful information into your hands. Biomation, 10411 Bubb Road, Cupertino, CA 95014, (408) 255-9500. TWX: 910-338-0226.

Biomation’s new 1650-D produces a repetitive display output reconstructing precisely 500 bits per line for a 16-line timing diagram on a conventional oscilloscope or CRT display. Separate selection of individual channel outputs allows viewing of 1, 2...16 channels at one time with automatic vertical expansion.

Map—each word in memory is transformed via two DAC’s to form a unique dot which characterizes that word. All 512 words of the 1650’s memory can be accessed for mapping. The cursor word is displayed as well as displayed at the top of the screen in alphanumeric form. The cursor may be moved to any of the points in the map for positive identification of that word. In addition, a map of only 16 words may be selected.

Logic state—provides memory address location, binary output of the 16 channels and selectable octal or hexadecimal translation. 16 words are displayed at one time with the cursor address location at the top of the screen. Movement of the cursor control allows accessing any 16 words of the entire 512 words stored in the 1650-D. The display control memory can store 16 words while a different set of 16 is selected from the 1650’s main memory (or a new recording is made). These two sets of 16 words can then be overlayed on the CRT. Any differences will blink and be easily identified.

Creating tools for technology
TEKTRONIX now has 5 ways to look at logic.

The New DF1 Formatter

First, we gave you the timing display and binary readout with our 7D01 Logic Analyzer. Now, with the DF1 Display Formatter, which is dedicated to the 7D01, you have five display formats to operate from, all in a 7000-Series mainframe. Now you can convert a timing display into tables of words in Binary, Hexadecimal, Octal... or a mapping configuration... whatever your application requires.

A STATE TABLE mode of operation produces standard tables of up to 16 lines of 16-bit words. Using the 7D01’s cursor, you can step through these tables word-by-word in Binary, Hex, or Octal. A 17th word is added to each table emerging from the 7D01’s memory, to serve as a “key” and indicate you are indeed scrolling correctly through the long memory. The 7D01’s fine cursor control steps the display line-by-line, while the coarse control advances it table-by-table.

One of the most powerful analytical capabilities provided by the STATE TABLE mode is that you can display two tables—a reference table of “proved” data plus a “new” data table drawn from a system under test—on the same CRT for side-by-side comparison. New data that is different from the reference data is automatically intensified... you immediately know faulty data exists, and you know its location.

With the DF1 you can map, not just one, but three ways. The ability to map FAST, SLOW, or MANUAL lets you quickly recognize a word of interest, track it, isolate it, then pinpoint it for detailed analysis. The importance of mapping is derived from the speed with which you can isolate problems.

The logic analyzer package shown (7603 Option 1, 7D01, DF1) starts as low as $5790. If you already own a 7000-Series mainframe, add the 7D01-1 (7D01/DF1 combination) for only $4390. Also consider that your money buys you these important 7D01 features: 1) Word recognition, 2) 16 channel operation, 3) 15-ns asynchronous timing resolution, 4) 4k formattable memory (4, 8 or 16 channels), and 5) High Z probes.

For more information or a demonstration of the DF1, contact a Tektronix Field Engineer near you. Or write Tektronix, Inc., P.O. Box 500, Beaverton, OR 97077.

United States sales prices are F.O.B. Beaverton, OR. For price and availability outside the United States, please contact the nearest Tektronix Field Office, Distributor, or Representative.
Mag tape systems plug into IEEE 488 bus

The first magnetic tape systems designed to plug directly into the IEEE 488 standard bus and compatible with IBM and ANSI tape standards use an 8080 microprocessor for full tape control and tape-to-bus interface.

Designed by Information and Applications, Beltsville, MD, the type 4600 systems have an 8080 control box with only 75 chips, according to Scott McPhillips, system designer. "An equivalent IBM type of controller uses about 260 IC's," notes McPhillips.

The microprocessor makes it easy to interpret bus commands from any 488 bus controller such as a calculator or instrument. One bus pair is dedicated to tape data, while another provides a separate channel for tape control and status information, according to McPhillips.

Addressed as a listener, the 4600 records data from the instrument or calculator talking on the bus. Addressed as a talker, it reads back the tape.

"The microprocessor has allowed us to implement everything that a large IBM controller does, including one-track error correction," adds McPhillips. More over, all of the control for the tape drive is in software.

Read errors are eliminated by a system that recovers the data by rereading with different thresholds. If the error persists, the system reconstructs the data with IBM-compatible parity and error-correction codes.

Should a tape defect cause a recording error or even a marginal signal, the data are automatically erased and rewritten further along the tape.

The error-correcting function requires only two pages of the program.

Other low-speed, off-line tape systems don't incorporate these read and write error-correction features. They may record compatible-check characters, but they don't make use of them, according to McPhillips.

The microprocessor also provides full read and write data buffering and free format-command processing. The data buffer holds an entire block of data and transfers it over the bus, character by character, whenever the appropriate instrument calls for it.

The 4600 systems are available with 7, 8-1/2 and 10-in. reels that use 0.5-in. wide, 1.5-mil computer tape. The 10-in. reels operate at 45 ips, and the other two at 25 ips. Data-transfer rates are 0 to 3000 byte/s for the large-reel machine and 0 to 2500 byte/s for the smaller ones.

JEDEC package outlines are now available

A complete collection of JEDEC-registered, solid-state package outlines and dimensional information has been issued by the Joint Electronic Device Engineering Council of the Electronic Industries Association (EIA) and the National Electronics Manufacturers Association (NEMA).

"JEDEC Registered and Standard Outlines for Semiconductor Devices" (JEDEC publication no. 95) supersedes and replaces EIA documents 12F, 13, 76 and RS-389.

The 600-page loose-leaf volume includes over 400 package outlines for diodes and transistors, microelectronic devices, uncovered devices (such as beam-lead components), carriers and magazines, gauges and military devices.

Complete dimensional information and detail drawings of all registered and standard package outlines come in both inch and metric versions with manufacturing tolerances. In addition, the volume contains illustrations, symbology and a guide for preparation of drawings. Indices and explanatory data are also provided for quick and accurate reference.

The collection can be ordered from EIA's Standard Sales Office, 2001 Eye St., NW, Washington, DC 20006, $42.50 per volume. An optional subscription service, which provides new and revised update sheets, is available for an additional $15 a year.

μ C-based switchboard helps cut phone bills

Promising to cut a large corporation's telephone bill by 30 to 50%, a computer-based system that controls and records a company's outbound, long-distance calls has been announced by Datapoint Corp., San Antonio, TX.

Infoswitch first checks the priority rating of a caller's identity number and tries to select the least expensive route using WATS, FX (foreign exchange), tie lines or other voice-communications facilities. Then, if all these circuits are busy—and the priority number warrants it—the call is put through via Direct Dial.
After the call, Infoswitch records the caller-identity number, the number dialed, the facilities used and the call’s duration on magnetic disc.

The heart of this economical system is a dual processor that employs a dedicated microcomputer for high-speed telephone switching and a Datapoint business computer for logging the calls, monitoring the system and generating management reports. A printer can be added for hard-copy output; a magnetic tape can be included for either storing accounting data on a long-term basis or transferring data to another processor.

The switching equipment consists of a Datapoint μP with a 300-ns cycle, a 16-k ROM program storage, a 4-k RAM temporary storage and a reed-relay switch matrix.

The processor—Datapoint’s 5500—uses either diskettes, which store 250,000 characters each, or a cartridge disc system that stores 5-million characters on each disc. Copy is printed out at a speed of 80 copies per second.

Additional phone features include 3-digit code numbers for numbers frequently called and multistage call holding—the computer holds the caller on a low-cost circuit until a line clears. Length of the hold depends on the caller’s priority number.

A 6-trunk system costs $35,000, a one-year lease $1113. A 55-trunk system costs $175,000.

**Army computer system a super problem solver**

A supercomputer with a demonstrated ability to achieve processing speeds of over 800-million instructions per second has been developed by System Development Corp., at its Huntsville, AL operation, with the help of Burroughs Corp. Known as Pepe (for parallel-element processing ensemble), the first system has been delivered to the Army’s Ballistic Missile Defense Advanced Technology Center in Huntsville, to carry out ballistic-missile-defense experiments and tests.

Although the Army’s Pepe system has a CDC 7600 master computer that is wired to control 288 slave elements, only 11 are operating to date. Each “slave” consists of three processors sharing a common data memory, and each processor has an arithmetic capability equivalent to a medium-scale scientific computer.

In general, the Pepe system employs parallel processing and associative-data techniques to take on problems so complex that their solutions require inherent parallelism and extensive computational power. Parallel processing allows the system to solve many lengthy scientific computations simultaneously. Associative data retrieval enables Pepe to perform multidimensional file searches.

Besides missile defense, weather forecasting, air-traffic control, image data processing, and signal processing can also benefit from the increased computational power.

While the Pepe system’s gate-level logic design and the electrical and mechanical design come from Burroughs, the specifications and architectural design to the register level come from SDC. SDC has developed the Army system’s support software and produced the real-time programs, and plans to run the ballistic missile defense experiments and tests.

**High-density RAM board has a good memory**

A RAM board with a capacity of more than 1.3 Mbits has been developed by Intel Corp., Santa Clara, CA. Unveiled at the recent Mini/Micro Computer Conference and Exposition in San Francisco, the high-density memory board contains 147 packages—80 of which are 16-kbit dynamic RAMs—in a board of area of less than 90 sq. in.

Designed for custom medical applications, the memory array is organized in 16-k words of 80 bits each and includes CRT refresh logic for up to five pixels. (A pixel is the number of bits required to support a single dot on the face of a CRT.)

The very tight package spacing is possible because the board consumes only 70 W when operating and 18 W in standby. Intel 2116 chips provide 400-ns access time and 500-ns cycle time at the board level.

This high-density memory board costs about 0.4¢ per bit in small quantities and 0.25¢ per bit in large quantities.

**Device emits all colors with applied voltage**

A new kind of light-emitting device that produces light of all the colors of the spectrum by simply changing its applied voltage has been developed at the Ford Motor Co. research laboratory in Dearborn, MI.

A thin-film device consisting of two layers of metals separated by an insulator, the component is not only compatible with silicon-fabrication technology, but ultimately should become mass-produced at a low cost, according to Shaun L. McCarthy, senior research scientist and creator of the light source with staff scientist John Lambe.

The device fabricated to date employs a 500-A-thick aluminum layer for one electrode, which is separated from a 300-A-thick metal electrode—silver, gold, lead, or indium—by an insulating aluminum oxide layer 30-A thick.

Applying 1.5 V across the device produces radiation at the red end of the spectrum. Increasing the voltage changes the color of the light through the orange into the blue at about 3 V. At 4 V, the optical energy radiated contains quanta of the full spectrum, and white light is visible.

The quantum efficiency of experimental devices is in the 0.001% range, much less than the 0.1% to 2% of off-the-shelf monochromatic LEDs. To excite radiation, the current used by the Ford researchers ranges from about 20 to 100 mA, which corresponds to the range of standard LEDs. But the Ford devices’ light output is substantially lower because of their lower-quantum efficiency.

While the potential quantum efficiency of the thin-film devices is estimated to be in the range of a few percent, it is currently restricted by having to couple energy out of the device. The radiation is produced by “inelastic tunneling” of the electrons through the insulating barrier.

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Electronic warfare to get more DOD attention

Procurement of electronic-warfare (EW) systems by the Defense Dept. will average at least $500-million annually over the next five years, said Dr. Malcolm Currie, director of defense research and engineering, at a meeting of the Association of Old Crows at the National Bureau of Standards, Gaithersburg, MD.

Two of the principal EW projects planned during this period are the Navy’s Tactical Airborne Signal Exploitation Systems (TASES) and the Air Force’s Compass Hammer program, which will take the lead in developing airborne electro-optical countermeasures. The two services will join forces in the Compass Go program to develop a common internal jammer for the Air Force’s F-16 air combat fighter and the Navy’s F-18 naval strike fighter, as well as any future fighters.

In the past, EW systems have been almost an afterthought in the development of new aircraft and other weapons, according to Currie. But a recent Pentagon directive, 46003, stipulates that electronic counter-countermeasures (ECCM) be specifically considered in the design of every new military system.

“ECCM must become an integral part of our planning—not a patchwork, subsequent add-on,” said Currie.

Present plans call for research and development for electronic warfare to increase 10% a year from its present base of about $250-million over the next five years.

More airports to get Category III ILS

Eight more U.S. airports will be upgraded to Category III instrument landing systems under a Federal Aviation Administration program to provide all-weather landing capability at key airports.

Category III operations require ILS guidance signals to permit landings without visual reference to the ground when the ceiling is zero and visibility on the runway is 700 feet.

The landing system uses solid-state components and includes a dual-channelizer, dual-channel glide slope and three dual-channel marker beacons. A far-field monitoring system detects any shift in localizer-course alignment.

The system will be produced by Wilcox Electric Inc., Kansas City, MO, according to the terms of a $3.7-million FAA contract. Deliveries will begin in late 1977 at a rate of two a month to New York Kennedy, Chicago O’Hare, Houston International, Kansas City International, Detroit Metropolitan, Seattle-Tacoma International, Los Angeles International and Portland International airports.

Four airports are already equipped with Category III equipment: Washington Dulles, Atlanta International, San Francisco International and
Denver Stapleton.

Under an earlier $8.7-million contract to Wilcox, the FAA’s largest single purchase of instrument-landing systems, the company will deliver 122 Category-I ILS units to smaller airports in early 1978. Category-I ILS requirements call for visibility of half a mile and the ability of the pilot to descend to a “decision height” of 200 feet, where he can see the runway and decide whether to land.

**Missile guidance to use satellite data**

A missile-guidance system that will use the future Navstar global positioning satellite to guide the missile to its target is being developed at the Air Force’s Armament Development and Test Center at Eglin Air Force Base, FL.

Small antennas on the missile’s surface will receive position information from the Navstars at frequencies between 1.2 and 1.5 GHz (L-band), which will help update the inertial systems during the mid-course portion of the missile’s flight.

The missile-guidance system is expected to be applied first to the GBU-15 glide bomb, a winged version of the television-guided “smart bombs” used in Vietnam, then to a number of other new tactical weapons, say officials at Eglin.

Hughes Missile Systems Group and Teledyne Systems have been funded about $1-million each for the first year of the three-year development program. By mid-1978, breadboard hardware should be produced for captive flight testing at Eglin on the F-4 fighter. Concurrently, the Air Force is developing an airborne computer for the new guidance system under its Digital Guided Weapons Program.

**Weather radio growth predicted**

By 1980, the National Oceanic and Atmospheric Administration’s weather-radio service will serve 90% of the U.S. population with more than 300 transmitters, predicts an Administration spokesman.

Limited originally to boaters and fishermen in the mid-1960s, the network not only provides storm and flood warnings via 100 stations, but is also, since 1975, the only Government-operated radio system designated by the White House to warn against nuclear attack. Signals are broadcast at 162.40, 162.55 and 162.475 MHz, and the average effective radius is about 40 miles, according to NOAA.

**Capital capsules:** Nippon Electric has been chosen by Intelsat to develop a 14-GHz mixer/intermediate-frequency amplifier with state-of-the-art microwave integrated circuitry for communications-satellite applications. . . . Despite a crash in a flight test on Oct. 4, the Air Force’s Air-Launched Cruise Missile (ALCM) development and pilot production are expected to be carried out concurrently next year to push up the initial operational capability date from December, 1981 to January, 1979. The inertial platform is being blamed for the crash, not the terrain contour-matching guidance. . . . The Air Force’s Avionics Laboratory plans to develop an infrared search-and-track system for continental air defense. . . . Texas Instruments and Honeywell are in the final competition for the AAQ-9 common forward-looking infrared (FLIR) to be used in the Pave Tack pods of the Air Force RF-4. The winner should be selected around the beginning of 1977.
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CIRCLE NUMBER 25
Can you evaluate µPs by examining their register architecture?

Recently introduced µPs contain many more internal data registers than the earlier ones. Some of them have over 64 registers and are apparently very powerful. But often the number of registers is not as important as how easily the registers can be addressed and their data manipulated, according to one µP vendor. So with differing considerations in mind, how does the user evaluate the different register architectures and decide which µP to use? Opinions vary.

"The types of operations that you can perform on registers, through the instruction set, decides whether one set of registers is more useful than another," says Mark Eliot, manager of applications at Zilog, Los Altos, CA.

"The simplest instruction would move data into and out of the registers. The Z-80 can move data to and from registers directly addressed as part of the instructions. Another instruction type permits registers to serve as pointers to memory—to hold addresses of memory locations.

"Other instructions let the registers perform ALU operations such as add, subtract, logic or increment," Eliot says.

"I think that evaluating µPs by looking at their registers is pretty much nonsense," retorts Lionel Smith, applications engineer at Intel.

Industrial microcomputer system doubles as development tool

A microcomputer system that is flexible enough to do prototype development and still inexpensive enough to serve as an OEM industrial controller has been developed by Logical Services. At the heart of the Servant microcomputer system is an 8080A-based CPU.

Some key features of the Servant 8 system include a light pen and an oscilloscope-drive output in addition to a full complement of front-panel controls and indicators. The light pen and an oscilloscope make it possible to examine and modify the contents of registers and memory locations without the use of a terminal.

There are seven condition switches that allow breakpoint insertion in programs to permit examination of registers and memory locations.

Software for the operating system consists of a monitor program that can be automatically accessed when power is turned on. Also available are an assembler, a debug routine, a text editor and specialized macro and application programs.

Among the optional plug-in modules currently available are: a 16-channel analog input, 8-bit output circuit; an IEEE Standard ASCII bus interface; and a universal breadboard that permits customization.

Price of the basic development system, which includes the CPU, control panel, 4-k RAM, a TTY interface, chassis and ROM software, is $2495. Individual module prices start at $50 for the breadboard card and go up to $350 for the control panel card. Delivery of all units is from stock.

But if you have to go to external locations, and you don’t have the addressing modes to get at the data, you are going to end up with a cumbersome system.

On the other hand, he says, “A machine that has a lot of addressing capability and registers but needs to access only a few variables would be a case of overkill. I don’t think there is any way of just looking at register architectures and coming to a decision based on that alone.”

---

**CMOS μP comes in a console with display and keyboard**

Now you can get RCA’s CMOS μP in a console with a hexadecimal keyboard and four-digit LEDs for inputting and displaying data. The console, dubbed the UC1800 from Infinite, Inc., is available in kit form ($249.95) or assembled ($495). The unit consists of a separate CPU board and display, keyboard, and switch control modules that plug together with flat cables.

The 5.5 x 8.5 in. CPU board contains the μP, all control logic, a regulated power supply, and a 72-contact rear-edge connector for system expansion.

The display module contains a voltage regulator, decoder and the seven-segment LED readouts. It measures 6.75 x 2.75 in.

The keyboard model contains hex keyswitches and encoding logic. The switch module contains additional pushbutton switches that control the UC1800.

With the console, you get a 200-page manual and debug software so you can examine memory and modify programs.

*Infinite, Inc., Dept. INR, P.O. Box 906, 151 Center St., Cape Canaveral, FL 32920. (305) 783-9600.*

**New bipolar chip eases system interrupt control**

Hardware control of the priority interrupt inputs to a microprocessor system are now possible with a new bipolar LSI chip introduced by Motorola. The device, called a Priority Interrupt Controller (PIC), eliminates the software interrupt-polling routine in systems containing eight or multiples of eight I/O devices.

Functionally, the PIC can change the interrupt vector, reserved in memory for hardware interrupts, into one of eight alternate vectors assigned to the I/O service routines. It modifies the low-order bytes of the reserved interrupt address. The second, third, fourth and fifth LSBs of the system address bus are used as inputs to the PIC; a bit pattern of 1100 (5th LSB to 2nd LSB, respectively) is required to initiate the vector translation.

The interrupt output of each I/O device is normally connected to one of eight prioritized latching inputs on the PIC. When enabled, each interrupt will cause a unique bit pattern to be generated and substituted for the 5th through 2nd LSB of the original interrupt vector. These eight alternate vectors are used to start the interrupt subroutines for the I/O devices.

A mask, which is programmed via the 5th through 2nd LSBs of the address bus, can be used to inhibit any or all of the interrupts at the eight inputs.

An output from the PIC, called the STRETCH signal, is available to lengthen a system clock cycle when accessing slow memories. When unselected, the PIC is transparent on
How to get a lot more into a lot less.

First, with 3 rows of contacts on .100 centers, Viking's unique Nordic 2-piece P/C board connectors and I/O I.C. panel plugs get a lot more contacts into a lot less space.

Second, our unusual polarizing system lets you key each mating pair to prevent cross mating with adjacent connectors of the same type. You can stack a series of Nordic connectors next to one another in cramped space and not worry that they might be cross mated.

Our full line includes 64 and 82 contact models as well as the 120. Contacts on I/O connectors are crimp, snap-in, removable, gold plated and use MIL-T-22520 tools.

Diallyl Phthalate is the insulator in most models. And all connectors are designed to meet conditions of MIL-C-55302.

If you need them right now, our distributors have most models in stock. For details, use the coupon and get our latest catalog.

O.K. Send me: □ Your latest catalog with details on the two-piece PC connectors ... and your nearest rep. I have some questions for him.

Name: ___________________________
Position: ________________________
Company: ________________________
Address: _________________________
City: ___________________ State: ______ Zip: __________

Viking CONNECTORS
Viking Industries, Inc., 21001 Nordhoff Street, Chatsworth, CA 91311

ELECTRONIC DESIGN 24, November 22, 1976
CIRCLE NUMBER 26
the address bus and will not affect the reserved interrupt vector. The PIC is offered in both ceramic and plastic 24-pin DIPs; the price is $7.50 (100-999 qty.) for the plastic version.

Motorola Semiconductor Products, Inc., P.O. Box 20294, Phoenix, AZ 85036. (602) 962-2151.

CIRCLE NO. 508

µP-controlled time clock remembers data until queried

A 6800 µP-controlled time clock keeps track of employee attendance and other information, then relays the data to a central computer.

The Smart Clock first reads up to 16 digits of Hollerith-coded data from an employee’s plastic ID badge or IBM card. Then the employee punches in five more digits via pushbuttons. The terminal stores this information, as well as the time, in its own battery-powered memory. It checks each transaction for validity, sounds an alarm and activates visual indicators if an error has occurred.

The unit communicates with the computer via RS-232C serial lines or with a 600-baud modem interface. If the central computer breaks down, the Smart Clock holds all the accumulated data, up to 14,000 characters, until the computer is again able to receive data.

Up to 64 Smart Clocks can be connected in series through one RS-232C, ASCII-coded, 20-mA current loop.

The unit price is $1600 for quantities of 10 to 24. Delivery takes 45 days.

Coastal Data, 1592 N.W. 159 St., Miami, FL 33169. (305) 625-7123.

CIRCLE NO. 509

Fortran compiler does its thing on an 8080 system

A Fortran compiler is reportedly the first to be resident on an 8080 system. The FORT 80 compiles a subset of ANSI Fortran IV, which produces 8080 machine-language object code.

It requires 16 kbytes of memory: 12 k for the compiler and the remainder for work space. The object code produced by the FORT/80 can be linked to additional machine language subroutines to make a complete program.

Symbolic names containing 1 to 31 characters may be used. However, only single and double-byte integer arithmetic is permitted.

A library of useful subroutines and functions comes with the compiler, including absolute values (ABS), random 8-bit numbers (RANDU), and the square root of positive and SQRT integers (SQRT).

The software is supplied either on a floppy disc or on paper tape, and costs $750.


CIRCLE NO. 510

Micro Capsules

A new version of a popular software language, called Basic Etc., is optimized for business and game programming. It comes from Binary Systems Inc., Richardson, TX. . . . An 8-bit µP that contains ROM, RAM, I/O and clock chip will be introduced by General Instruments, Hicksville, NY. The PIC-1650 fits in a 40-pin DIP. . . . A $60 prototyping kit from Intel Corp., Santa Clara, CA, contains chips for a 4-bit system. It has a 4040 µP, 4269 keyboard/display interface, and EPROM, RAM and I/O chips.
DARLINGTON POWER TRANSISTORS
The Designer's Choice from General Electric

### NPN - HIGH GAIN - ½ AMPERE

<table>
<thead>
<tr>
<th>GE TYPE</th>
<th>P_T</th>
<th>T_C = 25°C Max. (W)</th>
<th>V_CEO Min. (V)</th>
<th>h_FE @ 5V, 200 mA</th>
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<tr>
<td>D40C1</td>
<td>6.25</td>
<td>30</td>
<td>10,000</td>
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<td>• Very High Gain - 60k typical; High input impedance - 50k ohm typ; 1.2 watts P_T @ 25°C ambient.</td>
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### COMPLEMENTARY - 2 AMPERES

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<th>h_FE @ 5V, 5 Amps</th>
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<td>50</td>
<td>-80</td>
<td>1000</td>
<td>-</td>
<td></td>
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</table>

We'd like to show you our DARLINGTON POWER TRANSISTORS; for free sample, identify GE type and write on company letterhead to: General Electric Company, Semiconductor Products Dept., Electronics Park, 7-49, Syracuse, New York 13201.

GENERAL ELECTRIC

Electronic Design 24, November 22, 1976 39
Ask CONTROL DATA for the Floppy Disk Drive more major OEM's specify.

We have it.

One major OEM after another tested our Floppy Disk Drives. Ran them through rigorous evaluations. Compared them with competition. And chose ours. Either our Model 9400; or our Model 9404 with double-density capability.

Both have true IBM compatibility, with the write-current switched at track 43. Both offer ceramic heads; and hard and soft-sector capability. The 9400 has a star interface; the 9404 a daisy chain interface plus power reduction, write-protect option, and double-density capability.

Whether large OEM or small, we invite you to make your own tests and comparisons. Let us demonstrate our Floppy Disk Drives, right in your facility. Evaluate them, just as many major OEM's did. We know you'll make the same choice.

Two configurations available. Choose Model 9400 for single; Model 9404 for multiple drive applications. Model 9404 also offers double-density capability.

Ask the CDC OEM people

Call (405) 946-5421 or return coupon to: Terry J. Hardie, Control Data Corporation, 4000 NW 39th Street, Oklahoma City, OK 73112.
Connections were much simpler 200 years ago. Torch the fuse and the cannon fired.

Supplying the vital spark that makes a modern weapon system do its job is a lot more complicated.

That’s where we come in. For many years, primes and OEMs for military and aerospace products have depended on us to provide the vital links in their electronic systems—flat cable, etched circuitry, connectors, and total interconnection systems.

Our high-rel connections have to be the best. They’re used in systems like Phoenix, Maverick, Lance, Minuteman, AWACS, F-14, F-15, Space Shuttle, Viking, Sonobuoy, F-4, A-7, Condor, Standard Missile, F-18, AAH, Cruise Missile, F-8, Trident, Hobo, Sprint and many more.

To learn how we can serve your interconnection needs, contact Jack Maranto or Dave Cianciulli: Hughes Connecting Devices, 17150 Von Karman Ave., Irvine, CA 92714.

Or call (714) 549-5701.

Hughes Connecting Devices
CIRCLE NUMBER 29
HR-40
3 and 4 Channel
Strip Chart Recorder

OMNIGRAPHIC®
New from Houston Instrument

- Standard options available
- 10” or 250 mm recording width
- Disposable fiber tip cartridges in four colors
- All pens cover full chart width (Writing distance between channels only 2 mm)

Price from $3200.
Full scale response ¼ sec.
Choice of 2 interchangeable, plug in, input modules. 0.5mv to 200v full scale
Either English or Metric chart speeds
16 Switch selectable chart speeds 1 inch/min. to 24 inches/hr.
O.K., you guys, back to the old drawing board.

Just when you've made all your panel lamp decisions Monsanto comes along with LED lamps so light-efficient, with choice of color, that you'll have to take another look. They'll give you the same light with less power, or more light with the same power—whichever will do your application the most good.

They're the result of our patented nitrogen doping process for GaAsP on GaP substrates. We don't think you can find a better LED lamp, anywhere.

They come as T-1 and T-1 ¾ replacement lamps in standard red, bright red, green, yellow and orange. All those colors will give you great flexibility in design. And you'll get still more flexibility from their two lens choices and two lead lengths.

<table>
<thead>
<tr>
<th>Model Number</th>
<th>Color</th>
<th>Size</th>
<th>Luminous Intensity</th>
<th>Viewing Angle</th>
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<tbody>
<tr>
<td>5174B*</td>
<td>Orange</td>
<td>T-1</td>
<td>5.0 mcd</td>
<td>90°</td>
</tr>
<tr>
<td>5274B*</td>
<td>Green</td>
<td>T-1</td>
<td>1.0 mcd</td>
<td>90°</td>
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<tr>
<td>5374B*</td>
<td>Yellow</td>
<td>T-1</td>
<td>4.0 mcd</td>
<td>90°</td>
</tr>
<tr>
<td>5774B*</td>
<td>Red</td>
<td>T-1</td>
<td>5.0 mcd</td>
<td>90°</td>
</tr>
<tr>
<td>5152**</td>
<td>Orange</td>
<td>T-1</td>
<td>10.0 mcd</td>
<td>28°</td>
</tr>
<tr>
<td>5252**</td>
<td>Green</td>
<td>T-1</td>
<td>15.0 mcd</td>
<td>28°</td>
</tr>
<tr>
<td>5352**</td>
<td>Yellow</td>
<td>T-1</td>
<td>45.0 mcd</td>
<td>28°</td>
</tr>
<tr>
<td>5752**</td>
<td>Red</td>
<td>T-1</td>
<td>40.0 mcd</td>
<td>28°</td>
</tr>
</tbody>
</table>

*Models are also available with 1" lead lengths, low profile (.138" high) lens, or 180° viewing angle.

**Models are also available with 24° and 65° viewing angles.

It used to be that some sockets demanded filament lamps in spite of their failure and replacement problems. But now you may find all the brightness you need in our long-life LED lamps.

In short, Monsanto LED's can add value to your product. Because of their long life, high reliability, and low power requirements.

To find out more, call your local Monsanto man. Or simply send us the coupon.

Please send me information on your newest LEDs.

Name

Title

Company

Street

City

State

Zip

Mail to Monsanto Electronics Division, Dept. MCD, 3400 Hillview Ave., Palo Alto, CA 94304. Phone (415) 493-3300.

CIRCLE NUMBER 31
The world’s fastest LSI processor family introduces...

- 4 bits wide — fully expandable
- 16 powerful microinstructions
- Control cycle 52 ns
- 4 on-chip subroutine levels
- Instruction or subroutine repeat
- Standard MECL LSI from the ECL leader
- 8 on-chip registers — including expandable 4 X 4 LIFO

Speed alone would place the MC10801 in a microprogram controller class by itself, but with this remarkable MECL LSI building block, speed is just the beginning. Its 16 microinstructions and on-board registers make the MC10801 the most powerful microprogram controller as well as the fastest. Maximum system flexibility is ensured by five data ports. Generation of the next control memory address is possible from any of seven different sources: either I or O bidirectional bus, next address field, incremener, either repeat or instruction register, or LIFO stack.

When the MC10801’s four on-chip subroutine levels are not sufficient, expanding the LIFO stack via the I and O buses accomplishes nesting of more than four levels. And there’s still more. The repeat register permits big savings in control memory, particularly in large multiply or divide routines. Repeat capability for an instruction or subroutine is \( 2^n \), with "n" as the number of 10801s in the system. So with just two, you get 256 repeats. The number 256 points out another MC10801 feature, Page Addressing. Using the status register, multiple pages of 256 words can be addressed.
the world's most powerful microprogram controller.

The MC10801 is the fastest microprogram controller by any measure, but nothing demonstrates that fact better than a system speed calculation like this:

prices. Our introductory MC10801 price (100-up) is just $50.00, and we've already been able to cut our MC10800 price 40%, to $30.00.

Whether your processor application is in disk controllers, radar and guidance, video or speech processing, minicomputers, signal processing, or whether you simply want to emulate your favorite instruction set... the performance of the MECL LSI M10800 Family mandates your consideration, now.

For data, circle the reader service number or write to Motorola Semiconductor Products, Inc., P.O. Box 20912, Phoenix, AZ 85036.

For real action, contact your favorite authorized Motorola distributor or Motorola sales office.
Choose Datel’s DM-350 for your next design . . .
And take a look at these Datel Digital Panel Meters:

<table>
<thead>
<tr>
<th>MODEL</th>
<th>NUMBER OF DIGITS</th>
<th>POWER SUPPLY</th>
<th>FEATURES</th>
<th>PRICE (1-9)</th>
</tr>
</thead>
<tbody>
<tr>
<td>DM-350D1</td>
<td>3-1/2</td>
<td>+5VDC @ .3A</td>
<td>UNIPOLAR, LOW POWER, DISPLAY ONLY</td>
<td>$69 (1-9) $59 (100's)•</td>
</tr>
<tr>
<td>DM-350D2</td>
<td>3-1/2</td>
<td>+5VDC @ .3A</td>
<td>BIPOLAR, LOW POWER, DISPLAY ONLY</td>
<td>$75</td>
</tr>
<tr>
<td>DM-350A1</td>
<td>3-1/2</td>
<td>115/230 VAC</td>
<td>UNIPOLAR, XFMR-ISOLATED, DISPLAY ONLY</td>
<td>$79</td>
</tr>
<tr>
<td>DM-350A2</td>
<td>3-1/2</td>
<td>115/230 VAC</td>
<td>BIPOLAR, XFMR-ISOLATED, DISPLAY ONLY</td>
<td>$89</td>
</tr>
<tr>
<td>DM-4000</td>
<td>4-1/2</td>
<td>+5VDC @ .6A</td>
<td>OPTOISOLATED RATIOMETRIC AUTO ZERO XTAL LINE FILTER</td>
<td>$219 less BCD $239 with BCD</td>
</tr>
<tr>
<td>DM-4300</td>
<td>4-3/4</td>
<td>+5VDC @ .6A</td>
<td>OPTOISOLATED RATIOMETRIC AUTO ZERO XTAL LINE FILTER</td>
<td>$235 less BCD $255 with BCD</td>
</tr>
<tr>
<td>DM-2000AR</td>
<td>3-1/2 DIGITS AUTORANGING OVER 3 DECADES</td>
<td>+5VDC @ .8A</td>
<td>AUTOMATIC RANGING OVER ±200mV. ±2V ±20V FULL SCALE</td>
<td>$169 less optoisolation $218 with optoisolation</td>
</tr>
</tbody>
</table>
Jack and Charlie were having one or two while watching the old-timer drink his lunch. "What do you suppose keeps that guy going?" Jack wondered aloud. "He's at least 80."

"Well," Charlie began, pausing half a second to give the question the cegotiation it deserved, "it's got to be the booze. Look at him. He's just finished his fourth martini, and he's still going strong." Then, getting philosophical, Charlie added that contrary to the advice of people concerned with health—even doctors—alcohol keeps you young. The living proof (80, at least) was lunching (or lurching) at the end of the bar.

"I don’t know," Jack mused. "I think it's the womanizing. Heck, that guy's here every day with a different gorgeous gal. That's got to keep a guy going. It would keep me going."

"No," Charlie asserted. "It's got to be the smoking. I've never seen a guy smoke so much. He burned up half a dozen cigarettes in the last hour, and now he's on his second cigar. I guess tobacco must keep you young."

Before the discussion was allowed to die, Charlie approached the old gentleman. "Excuse me, pop," he said graciously. "To what do you attribute your venerable age?" And when the man muttered, "Well, son, mainly to the fact that I was born so long ago," Charlie chuckled, then tried again. "I mean, old-timer, how old are you?"

"I'm 29," the old man wheezed.

Well, everybody got a large charge out of the story when Bill told it at lunch. But some began to wonder if we don't all make similar mistakes. Too often we spend our time developing plausible theories for facts before the facts are all in. We try to discover why a circuit behaved a certain way before we determine if the circuit behaved that way. We sweat out the solution to a problem only to discover that the problem never existed. So we end up doing penance for sins that haven't been committed. And we offer theories to explain why Joe did something when, in fact, he didn't.

Jumping to conclusions is risky business.

GEORGE ROSTKY
Editor-in-Chief
Want simpler backplane connections?
Come to the source.

Now, a unique Scotchflex brand Socket Connector and Keying Header system lets you interface directly with backplane wire wrap pins and provides for easy, positive polarization and keying. The header design allows for thousands of unduplicated polarizing combinations without loss of backplane pins. The 50-position connector mates with .025" square pins on .100" x .200" grid spacing. Header allows space for and protects two layers of wrap below it. System also provides polarizing keys and strain relief handles.

Need some other ways to simplify wiring and increase circuit density? 3M's Scotchflex line offers you a broad choice of mass terminating socket connectors, plus wire wrap or solder tail headers to suit your specific design problem. Keying capability is also provided.

There are several more things you can get only from 3M. The broadest range of flat cables and complete system components. Best off-the-shelf availability. Proven performance. And the unmatched experience of the people who pioneered this reliable mass termination system.

"Scotchflex" is a registered trademark of 3M Co.

Scotchflex systems from 3M.
The source.
Interested in network variety?
Select from a spectrum of 347 standards.

Allen-Bradley has the popular configurations you need. Pull-ups, Pull-downs. Line Terminators. Networks to complement Core Memory Sense Amplifiers. TTL to ECL Translators. O-Pad Attenuators. All styles available from your Allen-Bradley Electronic Distributor. Call for specs or check your EEM Catalog. If you need specials, contact your local Allen-Bradley district office for fast turn-around. Ask for Publication 5840. A-B is an experienced twin-film manufacturer, i.e. precision thin film and thick film.

User trimmable option
as a special feature.

Solid ceramic body
for mechanical stability.

Color stripe
aids orientation and indicates number of pins. Blue-14 pin; green-16 pin.

Large design area
...room for more resistors, higher power ratings, larger resistance values.

External solder joints
for visual inspection.

Quality in the best tradition.

ALLEN-BRADLEY
Electronics Division
Milwaukee, Wisconsin 53204

CIRCLE NUMBER 191
True, but more buttons do not make a better analyzer. The 80-M Logic Analyzer from Digital Broadcast Systems can do many of the things the more expensive analyzers can do, such as, "snap shot" eight channels of digital logic, store the information in a 1K per channel memory and play it back on your scope or CRT. The 80-M has spike detection, real time and memory operation, eight bit word recognition, 10Mhz operation and much more.

Now that's a lot of analyzer with fewer buttons at a price of only $1,595.

If you are interested in a good analyzer that will fill your needs with easier operation, circle the reader service card number or fill out the coupon and mail to us for faster response.

Digital Broadcast Systems
4306 Governors Drive, Huntsville, Alabama 35805 (205) 837-2183

CIRCLE NUMBER 192

Electronic Design 24, November 22, 1976
POWER FOR LOGIC OR I/O PANELS

Terminal strip fixture-mounted connections are factory wired for various circuit configurations. These modules are available in single, dual, triplex, and multiplex configurations. They mount in 2.5 x 2.5 modules and are available in 10 volt or 5 volt configurations.

POWER FOR YOUR µPROCESSOR

Order multiple output power systems without the wait for rework or troubleshooting. An extensive mechanical library, ready to ship, provides an immediate solution for your µprocessor power needs. Available in a wide range of output configurations, from 3.3 to 15 volts, the Acopian µProcessor module is ideal for any µprocessor system configuration. Guaranteed 3-day delivery.

MATCHED OR DISSIMILAR DUAL OUTPUT

Select the combination of matched or dissimilar power supplies that will best suit your application. Output current ratings from 890 to 1500 watts. Output voltage ratings from 900 to 1500 volts. Acopian has been in your hands, quiting a low-cost, high-quality, single output module, available in 10 volt, 15 volt, or 25 volt configurations. Guaranteed 3-day delivery.

HIGHLY ISOLATED POWER

For applications requiring a power supply with unusually high isolation, such as for power to other sensitive components. Output voltage ratings from 0 to 10 volts. Input source isolation, 10,000 megohms minimum. Guaranteed 3-day delivery.

POWER FOR RELAYS AND DISPLAYS

Drive relay coils, visual indicators and similar loads with the Acopian AC/DC plug-in power modules. These modules are available in single, dual, triplex, and multiplex configurations. They mount in 2.5 x 2.5 modules and are available in 10 volt or 5 volt configurations.

RACK MOUNT POWER...TO 60 AMPS

Designed for mounting in standard 19" wide rack enclosures, these power modules are available in 14 different output ranges from 10 to 50 volts, and from 1 to 60 amps. They are available in single, dual, triplex, and multiplex configurations. They are available in 10 volt or 5 volt configurations.

SOLDER TERMINAL MODULES

For applications where hard wiring is desired, Acopian offers modules with solder terminals. These modules are available in single, dual, triplex, and multiplex configurations. They are available in 10 volt or 5 volt configurations. Guaranteed 3-day delivery.

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ELECTRONIC DESIGN 24, November 22, 1976

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CIRCLE NUMBER 35
Today's instruments are smart, versatile and safe
Smart instruments may have arrived, but they have brought problems with them. One of these is pinning down a definition of what smart means. To some a smart instrument means one that has memory, while to others it means the unit has a calculator chip or a microprocessor in it.

But a “brainy” instrument is not necessarily better than its “dumb” predecessor. Like the 21-transistor radio that used transistors for everything from diodes to resistors, instruments often contain a microprocessor simply for its promotional value.

But some instruments do take advantage of the added power a µP affords. And many of these use the µP to provide an interface between the instrument and the newly adopted IEEE Standard 488 Digital Interface Bus. The combination of microprocessors and the 488 bus is leading to a total system capability far beyond that originally envisioned for the bus. For example, it permits distributed computing systems to be built where processing can be done at the relatively slow rate of 1 Mbyte/s.

Another trend in instrumentation is a move toward synergistic instruments, devices that integrate a variety of different functions into a single unit. Unlike other multifunction instruments that are simply a collection of individual units in one package, the more compact synergistic instruments have a capability that is generally greater than that provided by individual instruments being used together.

But are today’s instruments safe? Manufacturers are going all out now to answer that question. The first thing one notices on new instruments is warning labels everywhere, especially where there is high voltage or even where there might be. Some companies have even gone to the extreme of putting illuminated warning labels on their equipment. These are particularly helpful on instruments being used by someone who is unfamiliar with the equipment.

To really appreciate these instrument changes, just turn to this special section.
Like the scarecrow in the Wizard of Oz, instruments have finally acquired a brain. The newly acquired smartness or intelligence promises no less than to revolutionize the entire test and measuring industry. But what is a smart instrument? What is an intelligent one?

As it turns out, it's just as difficult to define "smart" in equipment as it is in people.

To some, smart means memory. To others, it means an internal µP. Yet some instruments, which boast the use of those ICs, appear to do little more than conventional instruments of their class. The µP seems to be there strictly as a sales gimmick, merely to replace existing logic, with little additional benefits. In other cases, the µP either serves as an interface or does internal control chores.

A more satisfying definition of smartness requires a look beyond form to function. Such probing also helps distinguish between smartness and intelligence. To some, then, a smart instrument recognizes a preprogrammed situation and responds accordingly. Smart, in this case, can be likened to the on-off response of a relay that switches at a predefined level.

An intelligent instrument, on the other hand, goes farther. One viewpoint: An intelligent instrument makes decisions based on previous actions; it can manipulate information, crunch numbers, then choose an action based upon the results.

More than a few instrument designers see programmability as a key aspect of smartness—that is, the equipment can go through a sequence of operations under external control. For example, a user can "keyboard in" numbers and tell the smart equipment to use the values in one of several ways. Or the human operator can be replaced by a minicomputer or some other controller.

The impact of microprocessing

Features like self-diagnosis, automatic calibration, autoranging and automatic zero don't necessarily make a machine

Stanley Runyon
Senior Associate Editor
Slide the calculator-like keyboard out of the front panel, and you'll know immediately that the Dana 9000 is different. The world's first microprocessing timer/counter measures at the push of a button.

smart. These functions were around when µPs weren't. And in spectrum analyzers, at least, arithmetic with standard TTL logic predates the LSI microprocessor concept.

Whatever distinctions are made between smartness and intelligence, two things are immediately clear:

1. Microprocessors have just begun to have an impact on instrumentation.
2. The features and capabilities now possible are more than can be handled reasonably from both an economic and a user's viewpoint—even at this early stage of application.

The advantages of digital processing over analog have been known for some time. But now, with the availability of low-cost computers on a chip, the processing can be moved inside the instrument. Theoretically, at least, whatever a mini can do externally, a µC can do internally.

For the user, the immediate benefits of digital processing include a reduction in physical size, and capabilities and features hitherto impossible or uneconomical. The user also gains more functions and features per dollar, and easier instrument interfacing.

All is not roses for users, however. Although the potential exists in µP-based equipment to clear up front-panel clutter and make an instrument easier to use, just the opposite can occur.

Microprocessor control brings new power to data loggers. With the Fluke 2240A, you can mix voltages, thermocouples and thermocouple types on adjacent channels.

A cursory survey of existing instruments uncovers at least one high-IQ box with nothing up front but a power switch; at the other extreme sits an instrument with 50 pushbuttons and half as many indicators.

Although comparing the two extremes is a bit unfair, the two pieces of equipment do serve to demonstrate the possibilities.

Ease of use isn't easily pinpointed from front-panel design. A blank front panel might signal nothing more than a remotely programmable instrument; 40 pushbuttons might be easier to use than 40 rotaries—but not necessarily. Once a button is punched, in some cases, the user is
Check a $\mu$P-based system with a $\mu$P-based system. The DF1 display formatter boosts the capabilities of the Tektronix 7D01 logic analyzer.

Interactive digital plotting is a new concept brought to realization by the microprocessor. The Tektronix 4662 digitizes and transmits its pen position.

stuck with the entered number. Or the sequence of pushing is crucial—the wrong order brings weird results. Other limitations of smart instruments center around price or speed or reliability.

The price of brain power

Even though costs are dropping, the user must still pay a premium to own a $\mu$P-based instrument, because the cost of development is tacked on. Speeds of smart instruments are still restricted, and until $\mu$Ps get much faster, these restrictions will remain a fact of life.

What about reliability? With brainy instruments at present just babes in swaddling clothes, reliability figures are hard to come by. But, reportedly, complaints aren’t.

Incongruously, a greatly accepted virtue of LSI is the seemingly contradictory promise of greater reliability with increased complexity. That premise may be true. But if the user can’t fully test a chip, how can he be sure of its reliability? If he can’t pin down all possible states at all possible temperatures and voltages, what then? And if the user marries a $\mu$P to a 4-k RAM plus 4 k of ROM or PROM . . . .

Counterpoint to the question of reliability is the increasing use of self-testing and self-diagnosis, brought about by dedicated LSI and $\mu$Ps. If reliability doesn’t increase, then serviceability certainly will.

The designer of smart equipment—once he’s

Graduates from the college of knowledge

Intelligence has touched practically every class of measuring equipment today, and the honor roll gets longer each year. Those with digital processing power include the following:

**Counters:** Dana Laboratories Series 9000 Microprocessing Timer/Counter; Ballantine Laboratories 5500B Universal Counter/Timer.

**Data loggers:** Fluke Summa II Series; Dorian Scientific Digitrend; E: Thermodot DDF-200 (turns a DMM into a smart data acquirer); also units from Acurex and Esterline Angus.

**DMMs and voltmeters:** Systron-Donner 7115 DMM; Hewlett-Packard 3455A; Fluke 8500A; Keithley 6900; Data Precision 7500.

**IC testers:** Offered by Fairchild, Hewlett-Packard, Miroco, Testline and others.

**Impedance bridges:** Boonton Electronic 76A; GenRad 1657; Electro Scientific Industries 296.

**Oscilloscopes:** Nicolet Explorer; Hewlett-Packard 1722A; Norland 2001; Tektronix Digital Processing Oscilloscope.

**Signal sources:** Fluke 6010A Synthesized Signal Generator; Fluke 6011A Signal Generator. Wavetek 172 Programmable Signal Source.

**Others:** Rohde & Schwarz Automatic Radio Test Set; California Instruments CP70 Calculating Processor; GenRad 2230 Component Tester; Moxon Microcomputer Gauging System.
Is this the harbinger of tomorrow’s instrument? In the Fluke 8500A, measurement and control modules sit on a computer-like bus structure.

Two µPs in the Hewlett-Packard smart DMM control measurements, compute correction factors, handle the HP-IB interface and perform mathematics.

passed the learning period—can enjoy a newfound freedom of design flexibility. As software or firmware takes over from hardware, the options to do any single measuring job or internal control function are practically limitless. But there are new headaches, too.

Design decisions now include how to partition the product—that is, what to do in software, what to do in hardware. Which RAM, ROM or PROM to use, and which new memories or µPs will soon appear are questions a designer must continually answer to maintain his product’s competitive edge. And the increased difficulties in evaluating and testing LSI components are a new source of insomnia to already beleaguered engineers.

Marketors of smart instruments must also play a lead role in deciding which of all the possible features are important, what the front-panel should look like, and what performance will appeal to potential customers. In fact, many of the basic design decisions now fall squarely in the marketer’s lap, not the designer’s.

Still, designers are to be envied for several reasons:

1. µP-instruction sets are now powerful enough to produce the most complex algorithms when the sets are combined with ROM-stored programs and data-handling RAMs.

2. One µP can take over all control jobs, from refreshing a display to managing data output to interpreting controls.

3. Discrete operations, in many cases, can replace analog processing, with all its inherent problems.

Analog takes a back seat

One instrument that typifies the advantages of the new technology is the Fluke 8500A DMM. More a measurement system than a DMM, the 8500A is designed around a computer-type bus structure, with individual modules for measurement and control residing on the bus. Even the Fluke unit’s unusual front panel can be considered a limited-use peripheral that occupies one slot of the bus.

Control is handled by an 8080 µP, and the major operating characteristics are defined by software, not hardware.

Filtering noisy signals—ever a problem in measuring equipment—is implemented digitally in the 8500A by averaging many readings taken at a sample rate synchronized with the line frequency. Advantages: less hardware, the ability to program the number of samples per reading and, most important, greater noise rejection at operating speeds faster than analog circuits.

Other analog functions are ripe for simplification or even elimination. Circuits for tweaking or compensation (zero or offset) are candidates for the former category. Comparison, integration and sample-and-hold functions can all be performed digitally—as is done in GenRad’s 1657 Digibridge.

The 1657 is a µP-based automatic bridge that measures R, L, C, D and Q in less than 1/3 s. A sample-and-hold function is achieved in the bridge with software, not hardware, and errors are stored and minimized by digital techniques. The µP also computes and makes decisions—it directs both the instrument and the user to achieve optimum ranging.

Besides speed, the Digibridge user also enjoys maximum resolution, repeatable results and low cost. With component count two-thirds less than conventional circuitry, the 1657 sells for $995. Without the µP, says GenRad, the equivalent bridge would cost about $6000.

Another bridge with the new look is the Electro-Scientific Industries 296. Because of the internal µP, the 296 can be programmed for limit comparison (up to 10 values), can display percentage or absolute deviation and can be con-
Computer power brings a new dimension to everyday optical measurements. Gamma Scientific's CR-1A is an intelligent radiometer with programmable response.

Turn your DMM or DVM into a smart data-acquisition system with the DDF-200 control unit from E2 Thermo-dot, Carpinteria, CA. The unit handles up to 20 inputs, controlled through the IEEE 488 bus.

Still another instrument—the Gamma Scientific CR-1A computing radiometer—further demonstrates the power of internal digital processing.

Checking light with delight

Anyone who has made light measurements knows the problems of making adjustments for drifting zeros and dark currents. With the CR-1A, zero offset, dark current and ambient levels are digitally and automatically subtracted out. With eight keyboard-programmable constants, the user can punch in, update or change correction factors to shape response at various wavelengths. Each of eight registers stores a 3-1/2-digit number, a 1-1/2-digit exponent with sign and selected dimensional units.

The CR-1A takes further advantage of the μP with a self-calibrating algorithm, digital signal averaging and autoranging, among other features. Self-calibration is a growing trend that may soon be a feature of all measuring instruments.

The designers of one smart instrument, Hewlett-Packard's 3455A digital voltmeter, have taken special pains with the "auto cal" feature of the unit. The user unplugs a removable reference, makes four adjustments, then plugs the reference unit in again. The meter then checks its own dc and ohms circuits and corrects for errors.

Controlling the calibration process and computing correction factors in the HP unit is, of course, a μP—one of two in the instrument. The two microprocessors also take care of mathematical computations and controlling both the measurement process and the unit's programmability—that is, the HP-IB, or IEEE 488 interface.

To circumvent the speed limitations of commercial, serially oriented μPs, HP has designed a μP with parallel architecture to control the measurement functions. Such μPs may soon be available commercially from other sources. But one problem designers face with such architecture is the increase in support chips as the μP grows more parallel. Thus, speed may be gained at the expense of cost, size, power consumption and reliability. Somewhere along the line, compromises will have to be made.

A new force in μP testing

Those who design with μPs must also decide how to test the little buggers. To that end, μP or logic analyzers have appeared on the market, some μP-based themselves. One of the μP-based analyzers is HP's 1611A.

In appearance, the keyboard-controlled 1611A resembles a programmable calculator with a CRT display. In operation, the internal 80S0 controls the keyboard, tests for trigger points, keeps hierarchical order and performs other housekeeping chores.

What makes the 1611A smart? Software does much of the work according to HP—counting events, measuring execution time, looking up tables for mnemonic readout, and performing other computations. Thus the 1611A relieves the user from much of the test burden. In effect, the 1611A fights fire with fire: Software checks software; a μP tests a μP.

Other manufacturers recognize the power of the μP as the basis for equipment meant to test other μP-based equipment. Two such tools are the E-I Research Labs 1330 and the Tektronix DF1. In the guts of the Tektronix DF1 display formatter sits a μP, along with four ROMs and nine RAMs, one RAM serving as a scratchpad memory.
The new look in signal generators: Fluke's 6011A stores frequencies and amplitudes and lets the user edit or modify the output from a keyboard.

When used with the company's 7D01 logic analyzer, the DF1 turns any 7000-series scope into a measuring tool that displays timing diagrams, logic maps and state tables in binary, octal or hexadecimal codes.

Using a SC/MP μP, the 1330 offers a wide variety of triggering criteria to perform both logic timing and state analysis.

Not only can smart equipment lift a load from its user, it can even do the same for other smart equipment—a host computer, for instance. Consequently, more and more peripherals are undergoing brain "transplants." Conversely, with μPs combined with the IEEE 488 standard interface, measuring instruments—when connected in a system application—are beginning to look more and more like peripherals.

One "peripheral" is smart enough to speak for itself. The Tektronix 4662 interactive digital plotter—the first with built-in processing, thanks to the MC6800 μP—prints alphanumeric characters as well as draws whatever curve, plot or schematic the host processor dictates.

But give a machine a brain, and what happens? It talks back. The 4662, through use of an X-Y joystick, can send back current pen coordinates and other information.

Thanks again to the μP, the 4662 can work at high speeds, with acceleration, deceleration and vector generation all handled by the 6800. And the plotter can rotate or scale characters, change plot size and self-test its internal buffers.

With this kind of performance now being squeezed out of a design tool (the μP) that's barely five years old, the question arises: What next? New μPs and memories are coming, with on-board complexities and functions that signal even more radical changes in instrument design.

Is the Fluke 8500 voltmeter, with its internal bus structure and functional modularity, the forerunner, the symbol of things to come? Perhaps. But the Fluke design raises more questions than it answers.

Are instrument designs all heading toward a common finale, focusing on a single, universal instrument capable of becoming anything a user would like merely by a change in programming or the dropping in of a few memory chips? One instrument—the RS-432 data and timing generator from Interface Technology, Covina, CA—already permits the user to program the μP section to control the word-generator section.

Or will instrument systems dominate, with clusters of dedicated (perhaps even dumb) equipment chatting away at each other over remote lines, busily measuring, chewing up data, spitting out final results?

Perhaps some other, hitherto unknown, concept will prevail. In the more immediate future, more "conventional" intelligence can be expected to show up in yet untouched or barely influenced equipment—small, low-cost portable DMMs, scopes or spectrum analyzers. Signal generators have just begun to show the effects of the μP. Wavetek's 172 13-MHz synthesizer, for example, uses a μP to simplify programming, to handle formatting and to permit keyboard numeric entry of frequencies. And dynamic RAMs or PROMs in the 172 store programs or subroutines.

Other sources are sure to follow. Whatever happens, it will be exciting to watch.
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Today's battery-powered portable instruments—multimeters (DMMs), counters, chart recorders and waveform generators—are finding an increasingly prominent place on the designer's lab bench. Complex ICs within the instruments ensure high speeds, low power consumption, dense packing and combined functions. And the portable instruments can perform as well as some of the older, line-operated design equipment—at the same cost.

The latest packaging techniques have been combined with efficient, low-cost components to improve the general circuit design and the resultant savings in production costs have been passed on to the user.

The new portables contain the following custom or standard LSI circuits or specialized MSI:

- Entire analog-to-digital converters on one or two MOS chips.
- Complete four-to-eight decade counting circuits in a single package.
- Single-chip instrumentation amplifiers and low-power op amps.
- Specialized control circuits that do all the "internal housekeeping" for the instrument.
- High-efficiency switching regulator circuits.
- Battery-level indicators.

Battery-powered portables are no panacea, however. They often have a limited battery lifetime, a restricted operating temperature range and a high susceptibility to surrounding electrical fields. However, some new battery designs are overcoming these common power limitations.

ICs cut parts, cost & power

MOS LSI circuits, with their high packing densities, have enabled instrument designers to reduce the number of components needed. Custom MOS circuits still predominate in use among instrument manufacturers, although many of the new off-the-shelf circuits (probably last year's custom circuits) are starting to offer designers the functions necessary to build their instruments.

Dave Bursky
Associate Editor
Delivering true rms ac readings in addition to ohms and dc, the 7003 DMM by Systron-Donner can operate for up to six hours from its internal battery pack. Inside the DMM, a single-chip a/d converter takes three readings per second that are displayed on a 3-1/2-digit, 0.4-in.-high light-emitting diode display.

Single and multiple-chip a/d converters in PMOS, CMOS and I-L technology reduce the size and power requirements of DMMs. Converter circuits, such as those developed by Analog Devices, Norwood, MA; General Instrument, Hicksville, NY; Intersil, Cupertino, CA; Motorola, Austin, TX; Siliconix, Santa Clara, CA; and Teledyne Semiconductor, Mountain View, CA, require only 100 to 200 mW. Many of these circuits are designed for single-supply operation, and so eliminate the drain caused by a dc-to-dc converter to get the second supply level. (For more information about a/d converters, see the Focus on data converters" in ED No. 19, September 13, 1976, p. 68, and the special report on monolithic a/d and d/a converters in ED No. 13, June 21, 1976, p. 28).

Almost every DMM manufacturer incorporates one form of these IC a/d converters in his meter —and if he hasn’t found one suitable, he has designed his own. Hewlett-Packard, Palo Alto, CA, for instance, has designed a special conversion circuit and thin-film resistor network for its 3476B DMM. At a cost of $275, with the built-in battery pack, the meter offers V and I on ac or dc and ohms, autoranging, autopolarity and a special range-hold feature.

HP’s special circuit is a hybrid consisting of an NMOS control chip and a tantalum-nitride-on-sapphire resistor network. The control chip contains the counters, buffers, display scanner, 3500 bits of ROM program storage and all analog switches. The resistor chip contains 19 laser-trimmed resistors matched to within 0.02%.

Another DMM, the Danameter from Dana Laboratories, Irvine, CA, has only two ICs—a digital CMOS circuit and a bipolar analog chip. This DMM is one of a few using liquid-crystal displays instead of LEDs or gas-discharge digits. Going this route keeps power requirements to a bare minimum—the Danameter can operate with a 9-V battery for about a year. Weston in Newark, NJ, also offers a DMM with an LCD readout.

Making wide use of CMOS, Logical Technical Services in New York has developed the Model 12T, a combination DMM and thermometer, for $259. The unit fits in the palm of the hand, much like the hand-held DMM developed by Hewlett-Packard several years ago. The 12T uses not only digital-CMOS devices to cut power drain, but also tri-technology products like RCA’s (Somerville, New Jersey).
You can operate this scope and over a dozen other models from almost any voltage because Philips has incorporated a high-efficiency switching supply that eliminates the power transformer.

NJ) CA3130 op amp, which combines MOSFETs, JFETs and bipolar devices. MOSFETs on the op amp’s front end provide high input impedance; the JFETs provide the current source; the bipolar devices in the middle provide gain; and the CMOS output provides up to 20 mA to within several millivolts of the power supply or ground level.

Power consumption is dependent on the number of readings taken per second—a factor often overlooked when portable DMMs are evaluated or designed. The slower the conversion and counting circuits operate, the less power consumed.

When monitoring signals that change at several hertz, DMMs designed for line operation will always have an edge over battery-powered units. For example, most portable DMMs, like the Logical 12T or the Hewlett-Packard 3476B, take only two or three readings per second, while line-operated units often take five or more readings. Slow, periodic fluctuations can easily be missed if the meter's converter is too slow.

Other portable DMMs have been recently introduced: the 8030A and 8040A 3.5 and 4.5-digit DMMs by Fluke, Mountlake Terrace, WA; the Model 248 4.5-digit DMM by Data Precision, Wakefield, MA, and the 172 and 173 30,000-count DMM by Keithley Instruments, Cleveland. In addition to the normal V/I/R functions, Fluke's 8030A has a diode-test capability and can run for eight hours on a single charge. The 8040A has an autoranging capability and does true rms-ac measurements at frequencies up to 20 kHz. Data Precision's Model 248 also has true rms capability. Similar to Data Precision's older 245, the 248 also makes use, internally, of a custom digital circuit originally designed for the company's inexpensive Model 175 DMM to do all the display control.

LSI counting circuits, such as the MK50395 series of six decade counters from Mostek, Carrollton, TX, the ICM 7208 seven-decade unit from Intersil can form the heart of many compact, battery-operated frequency counters. These circuits can replace as many as 15 to 20 MSI devices and draw only about 200 mW.

Several companies are using this approach to make inexpensive, but very compact, frequency counters—but not all. “Non Linear Systems, Del Mar, CA, looked at this approach and decided not to use it,” says Roland Johnson, chief engineer. “We decided we could get even better performance by using low-power Schottky TTL and CMOS to build our FM-7 seven-digit frequency counter.” The FM-7 and its four rechargeable batteries all fit in a 4.5 × 6.5 × 9.6-cm (= 2 × 2.5 × 4 in.) case. The FM-7 can handle input frequencies from 10 Hz to 60 MHz (100 mV rms sine-wave sensitivity) and has an accuracy of ±1 digit ±time-base accuracy.

While most of the portable counters have similar accuracy specs, input sensitivities vary from model to model. Most portables have sensitivities of 10 to 100 mV rms, whereas lab-bench units often have sensitivities down in the microvolt region—direct measurement of rf is commonplace.

Portable instruments with combined functions are on the rise. Both HP and Vu-Data offer portable oscilloscopes with built-in DMMs or frequency counters. Tektronix, Beaverton, OR, goes so far as to use the CRT screen of its Model 213 1-MHz scope to display the reading. The entire combined scope/DMM weighs only 3.7 lb and can operate for 3.5 hours with internal batteries. Inside the 213, Tektronix uses several custom circuits to do the display generation and control all the timing. Very-high-efficiency switching circuits are used to provide the acceleration voltages.

Philips, which has gone to great lengths to make an efficient switching regulator, now in-
With over 150 components crammed into a hand-held DMM/thermometer, Logical Technical Services' Model 12T offers autoranging, autopolarity and 0.1% accuracy (V dc). The 12T provides a 3-1/2-digit answer and measures resistance from 1 Ω to 19.99 MΩ, dc volts from 1 mV to 750 V, ac volts from 200 mV to 750 V and temperature from -55 to 153.5 C. The NiCd batteries permit approximately 3-1/2 hours of use.

includes its regulation circuit in almost every scope it sells. The circuit permits the Philips scopes to be used from almost any ac voltage source ranging from 90 to 270 V at 46 to 440 Hz or any dc source from 100 to 200 V. Power consumption, depending upon model, ranges from 20 to 30 W, and unit weights average about 20 lb.

Function generators demand power

Generating signals in portable packages takes a bit more than simply measuring them. Only a few manufacturers offer any signal source with a self-contained battery pack. With its Model 30, Wavetek, San Diego, CA, is probably the best known. But pressing Wavetek is Exact Electronics, Hillsboro, OR, with its Model 119P.

The Model 30 operates from a single 9-V transistor radio battery and delivers sine, square and triangle waves over a 1-Hz-to-100-kHz range. It can deliver 5-V pk-pk into a 600-Ω load (or about 41 mA, maximum). Of course, delivering that much current will drain the battery pretty quickly, so a $25 rechargeable battery option is available for the $150 instrument.

Although Exact's 119P is larger than the Model 30 and costs about twice as much—$295—it offers more than 10 times the frequency range and twice the output voltage. The 119P spans 0.02 Hz to 2.2 MHz, delivers 10-V pk-pk into a 600-Ω load, and has a variable-time-symmetry adjustment.

While the battery-powered function generators deliver signals, the portable chart recorders can keep signal records. The go-anywhere recorders are available from such companies as Gulton, East Greenwich, RI; Hewlett-Packard in San Diego; Lab Data Control, Riviera Beach, FL, and Esterline-Angus, Speedway City, IN.

The HP 7155B runs from ac (85 to 130 V, 48 to 440 Hz), external dc (10.5 to 36 V) or from

Capable of operating in any position, HP's 7155B chart recorder offers 16-input voltage ranges and 7 chart speeds. It can run for 9 hours off the internal batteries.

Although originally aimed at the hobbyist market, the IM2202 designed by Heathkit has an accuracy of 0.5% on dc and 1% on ac, which makes it suited for many lab-bench applications.
The just announced Model 248 DMM developed by Data Precision offers a 4-1/2-digit LED display and true-rms ac measurement capability.

Internal, rechargeable batteries (up to nine hours on a full charge). There are 16 switch-selectable scale settings for the span (from 0.1 mV/cm to 10 V/cm) and seven chart speeds (from 10 s/cm to 30 min./cm). Scale accuracy is ±0.4% of full scale, and chart speed is controlled to within ±1%. This "Cadillac" of portable recorders goes for a stiff $1400 and $1700 with the internal, rechargeable battery pack.

Portability problems are far from solved

No matter which portable instrument is used, the greatest annoyance is to turn it on and find the batteries either weak or dead. So some manufacturers are incorporating "quick-charge" rechargeable batteries, long-shelf-life lithium cells, push-to-read controls and low-battery indicators. But no vendor has yet come up with an inexpensive way to determine how much operating life is left in a battery.

Since instrument manufacturers apparently are doing all they can to cut power consumption, the only other alternative is to increase battery capacity. To this end, many battery manufacturers have developed the sealed gel-electrolyte units and fast-charge nickel-cadmium cells. For instruments that sit on the shelf for long periods between use, the lithium battery is the answer for improved shelf-life. It has a shelf-life of 5 to 10 years. The lithium batteries are also the same size as carbon-zinc, but offer twice the voltage.

Specially designed circuits and batteries are starting to eliminate some of the guesswork in determining available battery life. Several low-power comparators from Intersil can be externally set to trigger whenever the battery voltage drops below a predetermined level. Once triggered, the circuit can be used to drive a LED indicator.

Battery manufacturers have developed several cells that have abrupt voltage drops when about 70% of their expected life has passed by. The drop is abrupt enough to trigger a circuit that can drive an indicator. Other batteries such as "super-fast"-charge NiCds nearly eliminate the problem. With charge times as short as 15 minutes—and typical NiCd charge times ranging from 4 to 16 hours—these new NiCds appear ideal for portable applications.

Combining both a DMM and a scope into a small, handheld package, Tektronix' Model 213 uses the CRT to display the DMM reading.
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**Complete details on request.
In today's electronics, nothing is more predictable than change. So it's not surprising that some people see the oscilloscope relinquishing its position as the primary test and measurement tool of the electronics industry. They point to the explosive proliferation of LSI chips, so inexpensive that it's sometimes cheaper to replace a faulty circuit board than troubleshoot it.

They say that conventional oscillography is too cumbersome for analysis of digital problems. And, as always, some argue that the oscilloscope has reached its limits in operating parameters and measurement versatility. Though we agree with many of the premises on which such arguments are based, we disagree with many of the conclusions.

Tomorrow's first line oscilloscopes will have good sensitivity and real-time bandwidths in the gigahertz area, as opposed to today's 500 MHz maximum. We are solving many of the CRT writing-rate problems associated with high bandwidths. Our input limitations due to capacitance, loading, and so forth, are being steadily reduced. We are developing better FET probes for impedance translation and we have passive probes that put 450 ohms in front of the scope's 50 ohms.

There has been a lot of progress in semiconductor technology in terms of gain-bandwidth product, impedance transfer function and noise reduction. And when today's 7-7.5 GHz IC processes (which make 1-GHz scopes possible) reach their expected limits at about 10 GHz, we can turn to gallium arsenide, gallium phosphide or other compounds now in development.

Computer-aided design has come along at a fortunate time, too. In the days of discrete circuits, it wasn't too useful because you couldn't put in all the strays.

If you added the strays with CAD, the problem became too complex, and if you didn't your circuit wouldn't work. But with ICs, the strays are smaller and more predictable. And we can work not only with surface

Howard Vollum,
Bill Peek
and Wim Velsink
of Tektronix
Speak on
The Future of
the Scope

George Rostky
Editor-in-Chief
Chatting with a visitor are (l-r) Bill Peek, Wim Velsink and Howard Vollum. In the background are the 511, geometries, but also in the third dimension, designing resistivities along with metal patterns and mask layouts.

Of course higher bandwidths present triggering problems, but we see progress along this line, too. One of the basic departures from the historical approach for greater stability is the use of high-speed ICs, as opposed to tunnel diodes. And faster amplifiers with shorter delays have made it possible to use shorter delay lines with better performance.

Sensitivities in the millivolt region can be anticipated, even at the higher bandwidths. Amplifier noise is the limiting factor here, but semiconductor technology has made great strides in reducing this problem.

Obviously none of these developments would mean much without parallel advances in CRT technology. We've made great progress in this area too. CRTs with bandwidths of 3 to 4 GHz and deflection factors of 1 to 2 V/cm in both vertical and horizontal are a present reality, with photographic writing rates up to 3 cm/ns. You can actually see a single-shot trace with the naked eye. And we haven't reached the limits yet.

Research is pointing away from the mesh scan-expansion CRT toward designs that will give us the nice crisp spot sizes we used to get with instruments like the 547—about 7 mils. And we'll eventually see these new CRTs in wide-bandwidth portables, where finer traces are much in demand.

Looking at the CRT as a display, we see an increased use of alphanumerics. We'll see new kinds of information displayed—information that will help the scope user do his job. It may be an instruction on what to do next, or a coded display—one/zero, hex, maps, signature, etc. A programmed logic analyzer might show you a picture for so many seconds and then ask you what you wanted next. Or a scope might instruct you to hook up this probe at this point and then tell you whether the reading is good or bad.

The storage scope is really coming of age, too. Ideally, we'd like to make every oscilloscope a storage oscilloscope.

Storage almost always works to your advantage. It lets you compare things, eliminates flicker and eases photography tremendously. Because you have a stationary picture of known brightness, there's no hassling—you know you're going to get it. If storage could be incorporated basically into every oscilloscope, even if it cost a little

Tek's first oscilloscope, dating from about 1946, and the 7834, a superspeed storage scope, just introduced.
more, probably everybody would use it.

Of course there were good reasons in the past for not doing this. But today we are getting to the point in storage technology where we can store as fast a signal as we can get on a conventional CRT. The new 7834 is spec'd at 2500 cm/s — fast enough to store a signal at its rated 400 MHz bandwidth. And our future advances in stored writing speed are expected to keep pace with bandwidth advances.

Storage is still the cheapest way to memorize a waveform. In spite of the many cheap A/D converters available, you still need a digital memory to take advantage of them.

**The future of the sampling oscilloscope is less clear. One of the problems is that the sampling scope is useful only with repetitive waveforms, and there just isn't a multiplicity of fast, repetitive waveforms that people want to look at.**

Really fast waveforms are usually single-shot, and the few exceptions can usually be handled by other techniques. Then, too, there has been a race between samplers and real-time scopes for a long time, and though real-time scopes haven't actually won it, in terms of being able to do everything the sampling scope can do, they have covered enough of the applications so that sampling has taken a back seat. And sampling has always had a problem in terms of the operator's confidence that what he sees is what is really there. Sampling scopes aren't easy to use, and there are modes you can get into that give a picture completely different from the real one. False triggering, for instance, and other operator traps. You might say that sampling scopes won the battle but lost the war.

Actually today's sampling scope is easier to use than it was in the past. The computer people, as they get into higher and higher speeds, will be using sampling techniques for some waveform analysis, especially in CPUs and communications links, where the highest speeds are encountered. To do this though, they'll have to program the computer to run in a repetitive mode in most cases.

Sampling techniques will also be used for a good while in time-domain reflectometry instruments like the Tektronix 1502 and 1503 portable TDR cable testers. This application is a natural for sampling. You generate a repetitive pulse and send it down a coax line, then display the reflection to determine the nature of any discontinuity or anomaly. You also measure the elapsed time between pulse and reflection and convert this to distance. With sampling techniques you achieve the gigahertz bandwidth necessary for resolution measured in inches, at a relatively low cost.

The other dimension of sampling lies in its use in A/D converters — rapid acquisition and retention of a bit of information, long enough to convert it to digital information. We'll see a lot of development continuing in that area.

So much for the idea that the oscilloscope has reached its technological limits. Now let's look at the argument that it's becoming obsolete in the
Tektronix. The first product, the Type 511, a 10-MHz, triggered-sweep, calibrated scope using many of the wartime technological advances, was an immediate success.

Today Tektronix occupies more than 500 beautifully landscaped acres in Beaverton and Wilsonville, Oregon, employs more than 13,000 people, and reported over $360 million in sales for fiscal 1976. The oscilloscope still accounts for the largest part of these sales, although Tektronix does a flourishing business in other electronic test and measurement instruments, TV monitors and signal processors, and a growing family of computer peripherals.

Despite his success, Howard remains a soft-spoken, mild-mannered individual, with an active concern for the welfare of his employees and a youthful enthusiasm for progressive ideas. He shuns public attention and attributes the success of Tektronix to the "wonderful, hard-working people" who work with him.

Nevertheless, he has been honored many times by his community, his country, and his peers in the academic and business worlds. He received the Legion of Merit with Oak Leaf Cluster for his contributions to military electronics projects during WW II. He has honorary doctorates in Science, Law and Humane Letters, is an honorary member of the ISA, and received a Medal of Achievement Award from the Western Electronic Manufacturer's Association. He is a Fellow of IEEE and received its Morris Leeds Award in 1973. He has received several distinguished service awards from various colleges, universities and institutes, and is a trustee or board member of three local colleges and one of Portland's largest hospitals.

Howard is married and has five children, ranging in age from 10 to 24 years. In his home, he has installed a full-size pipe organ, which he plays, he says, not nearly as well as his 22-year-old son. His other hobbies include photography and hi-fidelity magnetic recording.

world of the cheap integrated circuit and the smart microprocessor.

There is no doubt that the scope of today is in for some significant changes. But wherever electronics goes, you find the oscilloscope follows.

Remember the old fears that the computer would put everyone out of work? The idea that the oscilloscope will join the unemployed is no more apt to see realization.

As we see it, there will be two main thrusts to future scope development. One is the use of intelligence. It's in this area that the microprocessor will have its greatest impact. What form this will take isn't clear yet. There are plenty of real opportunities here, but also a lot of problems to be solved and decisions to be made.

The other thrust will be toward cost reductions. We expect some severe price competition in segments of our product line. There is strong demand for a multifunction, 50 MHz, 5-mV, dual-channel, delayed-sweep oscilloscope at a lower and lower price. The situation may develop into a repeat of the minicomputer business. Today minis are not getting much faster, but you can get for $2375 what you paid $15 K for when DEC first came out with the PDP-11 series. We haven't seen much of this in the oscilloscope business in the past, but it's probably going to be with us in the next 10 years.

But let's get back to the intelligent scope. Right away we run into a whole chain of considerations. You see, so much depends on how the oscilloscope is to be used.

In the lab, for instance, you don't often know in advance what you want to do with a waveform. You just see what's there, and that leads you to step two and on to step three and so on. It's not a predetermined situation. So, except for very broad mathematical manipulations like FFT, signal averaging, etc., it is difficult to predict in advance what digital processes you are going to need—and you can't build enough of them into a scope to cover every contingency.

On the other hand, there are significant application areas—servicing and production mainly—where the need is well defined. Like measuring rise time, time delay, time between pulses, etc. The scope could be programmed to make these measurements automatically and provide a readout on the CRT. Then if something came out wrong, the same scope could be used to troubleshoot the device.

It's in this area that the microprocessor will have its biggest impact. But we'll still have the problem of deciding what we want the scope to do. This means we'll probably have to provide custom programming software. Or we'll have to make it awfully easy for the customer to do his own programming. Probably we'll do both, in different kinds of instruments.

Some portable scopes may be designed for specific service applications. That is, a computer manufacturer may design a set of computers and
Wim Velsink has been in the front lines of R&D at Tektronix for most of the 16 years he has worked there. After taking his BSEE from Hogere Technische School in 1960, and short stints with Philips and Siemens and Halske in the Netherlands, Wim came to the U.S. He started with Tektronix as a design engineer in the accessories division in 1963, became Project Manager, Advanced Circuitry, in 1965 and Manager, Advanced Project Development, in 1966. One of his more important responsibilities in this position was the development of the 7000 series oscilloscope line. Wim is now Director of Tektronix Laboratories, General Manager, New Ventures Division and Manager, Advanced Display Techniques Development. He became a vice president in 1973.

Wim is a bachelor and an outdoorsman who relishes the many opportunities for skiing, hiking and camping in Oregon.

We'll provide a scope that is identical to last year's model, except that there'll be new cards with PROMs or ROMs and a special service manual for that set of computers and peripherals.

In other scopes we may provide the basic arithmetic functions and a few others that you can operate on a waveform with. You could multiply voltage and current to get instantaneous power, or integrate a current waveform to get charge. These capabilities are useful to a design engineer. And a lot of single-value functions would also be useful—rise time, aberration amplitude, period of aberration ringing, pulse-width, integral under the curve, and many others.

These kinds of functions are valuable in characterizing and documenting circuits, aside from testing them in production or incoming inspection. This kind of a scope would eliminate much of the present drudgery, say, in integrating a waveform. Now the operator must measure the waveform, digitize it point by point, then feed it into a computer, or use his calculator.

But building these functions into a scope isn't as easy as it seems. At first glance, it looks as if you'd only have to sample the waveform at a couple of points, measure the difference digitally, and show the readout on the screen. With this information, plus an examination of the waveform, you'd have a measurement you knew was valid. And this technique wouldn't be complicated or expensive. Actually it's not that easy.

We've found that many times it's just as easy to digitize the whole waveform and store it for viewing as it is to remember the two points and then try to correlate them back to the waveform position. Even the time required to turn the Z-axis on and off creates all sorts of problems in circuit and CRT design.

So let's say we digitize the input signal. By what method? Well, with A/D conversion, if we want to stay within reasonable costs and power requirements we need emitter-coupled logic.

This means a word rate of about 25 MHz or below, which gives us a 10-MHz scope at best. Or we can use scan-conversion techniques, as we did with the 7912. There's virtually no bandwidth limitation here, and you don't need a repetitive signal as you do with sampling. The principal limitation of the scan converter is in the length of the memory. How long a waveform can it remember? You're also limited to one sweep, at least presently, and the cycle between sweeps is relatively long compared to sweep time.

Of course, this limitation applies to all scopes. The only way to get around it is through continuous A/D conversion, and here you run into bandwidth limitations again. Even at a 25-MHz word rate, you fill a memory awfully fast. So you have to let the waveform run through the memory, decide what time slot you're really interested in, and pre- or post-freeze it, depending on the application.

This, incidentally, is one thing you can't do with the scan converter. Of course in the next five years we'll see the word-rate go up by an order of magnitude. We'll also see relatively low-speed scan converters being used as less costly A/D converters. Charge-coupled devices will probably play a big part in this.

One nice thing about scan conversion is the opportunity it affords in the display area. You can get any number of traces on one display in different colors if you have a scan converter in each channel and a color tube. And alphanumeric CRT readout could be color-coded to correspond
Bill Peek came to Tektronix as a design engineer in 1962. A graduate of Oregon State University, he received his master of engineering degree in 1968. In 1975 after holding various managerial positions in circuit- and instrument-design groups, Bill was promoted to the post of General Manager of the Laboratory Instrument Division. This division is responsible for design, production and marketing of Tektronix Laboratory oscilloscopes, the TM 500 line of test and measurement instrumentation and the new family of logic analyzers.

Bill likes to go camping with his wife and two young sons, and also enjoys woodworking, a hobby that came in handy when he built his own home a few years ago.

to the color of the trace it applied to. This would really make a readout a lot easier—reduce operator error and generally make the scope easier to use.

In any event, once A/D conversion becomes a standard item in waveform analysis, a whole spectrum of operations is opened. Relatively, you have all the time in the world to decide what you want to do with the stored waveform—how you want to display it, what kind of information you want to add to it or get from it, etc.

One thing is clear. We’re not going to have a universal scope that’s the equivalent of a hand-held calculator.

There are too many differences in customer needs and too many limitations on digital conversion techniques to make that possible. There is no doubt that new instruments will supplant the oscilloscope as the principal troubleshooting tool in some applications. We’ve recognized this by entering the logic analyzer field. There is a possibility that within the next 10 years, due to the tremendous impact microprocessors will have on all areas of industry, logic-analyzer sales may equal those of oscilloscopes.

Or a new instrument may appear that is even more suitable for the design, test and service of microprocessors. But eventually you still have pulse aberrations and timing relationships to troubleshoot, and power-supply circuits to debug in your microprocessor circuit. You’re going to have a whole array of EEs designing controllers for sewing machines, washing machines, automobile carburetion and braking systems, etc.

Electronics, especially the microprocessor, is penetrating new areas every day—areas previously dominated by mechanics, hydraulics, fluidics, etc. And the oscilloscope will follow, maybe not as the principal, but nevertheless as an indispensable troubleshooting tool. For although a logic analyzer or similar instrument may tell you what is wrong, it takes a scope to find out why it’s wrong.

Incidentally, when it gets down to servicing in these new areas, a few people are skeptical that a car mechanic may be using an oscilloscope to troubleshoot a microprocessor. Well, perhaps he won’t. But the trouble may not be in the microprocessor itself. It may be in the wiring or in the connections, at the inputs and outputs of the device. Probably most of the problems will be of this kind. Diagnosing these problems will require a fair level of sophistication, and this brings up an interesting point.

Some years ago, when radio and television were coming along there was serious consideration given to the proposition that they would never be a success because there wouldn’t be a group of people who could service them. With color television, it was considered impossible. Yet there are now thousands of people who are doing it. And auto mechanics aren’t all that different from other people. Look at the military. They have to maintain all sorts of complex, sophisticated electronic equipment. People rise to a challenge in their profession or vocation. In the future it may be a common sight to see an auto mechanic with a special-purpose oscilloscope, finding out what’s wrong in an electronic device.

In any event, we believe the oscilloscope has a bright future. Its general configuration, operating parameters, and variety of functions will change to meet the needs of our advancing electronics technology. But its primary function as a basic diagnostic tool will remain. Such tools have a way of staying with us. Remember that in spite of the millions of dollars expended each year on sophisticated medical diagnostic equipment, the physician still carries his stethoscope.
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The widespread adoption of the IEEE Standard 488 Digital Interface Bus by programmable instrument manufacturers is getting even wider. Enthusiastic acceptance of the bus by instrument buyers is creating a new generation of test instrumentation, the vast majority of which is designed to be controlled by programmable calculators via this general purpose interface bus (GPIB). Moreover, use of the bus doesn’t end with programmable instruments.

A principal factor in the rising tide of GPIB acceptance has been the proliferation of microprocessors in the last year or so. Increasing use of these microprocessors has permitted the instrument makers to provide, among other things, a low-cost, instrument-to-bus interface.

After a somewhat hesitant start a year and a half ago, the IEEE Standard 488 bus has now been adopted by some 50 instrument manufacturers as a firm option for their product lines. Typical of these manufacturers is the John Fluke Manufacturing Co., Mountlake Terrace, WA.

“As far as product planning,” says John Fluke, Jr., “all of our new products that have a digital output or remote control capability will have an IEEE 488 option. The only possible exception would be in very low-cost portable products. And in these cases, they would have a crude form of data output to drive a simple bus converter.”

The Fluke Model 8500A, a bus-structured, 8080-microprocessor-controlled DVM, is a prime example of the new generation of 488-bus-compatible instruments. “We built the voltmeter very much like a computer system,” Fluke explains, “where each function to be performed by the voltmeter has a corresponding module that plugs into an internal bus. The digital interface to the outside world plugs into slots provided for that purpose.”

Three interface cards are available for the instrument: an RS-232-C serial module, a duplex-parallel interface designed for interfacing directly to minicomputers, and the IEEE 488 interface.
Microprocessors and the 488 busses are being combined in instrumentation to provide a total system capability far beyond that originally envisioned for the bus, according to Pete Silvernail, group engineer at Wavetek, San Diego. Distributed processing or networking makes use of the intelligence scattered throughout the system in each instrument interconnected by the bus, Silvernail explains.

The original intention for the 488 bus developed by Hewlett-Packard was that it enable the user to assemble a group of bench-top measuring instruments and signal sources into systems that could be easily assembled or reconfigured. But now the bus is finding a home in military radar systems, process-control systems, interfacing with the IEEE Standard 583 Standard Modular Instrumentation and Digital Interface System, usually called Camac (Computer-automated measurement and control), as well as in large-scale automatic test equipment systems.

**Bus gives distributed processing capability**

The distributed processing capability of a system configured around the 488 bus provides a powerful tool for the instrumentation-system user, which means, according to Silvernail, that processing is shared by the calculator and the various microprocessors throughout the system. Thus, processing done at the relatively slow 1-Mb/s maximum speed of the 488 bus is substantially higher.

So Silvernail doesn't see any significant need for superspeed on the GPIB bus. But what he does see is a great need for the ability to tell instruments exactly what to do and for the instruments to respond by telling what they're doing.

These “command structures” have been incorporated into the Wavetek Model 172 Programmable Signal Source, according to Silvernail. The 172 is a combination oscillator, waveform generator, pulse generator and synthesizer, all of which are manually or remotely programmable. The instrument can generate sine, square, triangle, pulse, ramp, haversine, havertriangle and dc-level waveforms on command.

The 172 has the widest frequency range of any programmable function generator today, says Silvernail, and operates from 0.0001 Hz to 13 MHz, with the synthesizer portion operating from 10 Hz to 13 MHz.

In the 172's command structure, the instrument receives and stores a set of instructions from the calculator (or controller) during slack or initialization time. Only then is it necessary to use a hand-wave signal that essentially says: “Now do this or that.” This type of distributed operation reduces traffic on the bus significantly.

**The 172 talks back**

The 172 is the first machine to have an alphanumeric display that states what is happening within the instrument in English, French or German. For example, upon entering either a front-panel or remote frequency, the display reads: “Frequency is XX kHz,” in one of the three languages.

On the other hand, if the range is exceeded, the display states: “Frequency range exceeded,” and the excess is not indicated by the usual blinking LED, as with other instruments.
This automatic test set for transceiver measurements, by Rohde & Schwarz, is controlled through the IEEE bus by a programmable calculator. Card readers can also be used for system control.

While the 488-bus interface has been implemented initially in measuring and signal-generating instruments, Silvernail foresees the bus being adopted by display and storage systems as well.

"Within five years, every printer and plotter will be interfaced with the GPIB," he predicts. "I also say that many magnetic tapes and floppy discs will have that interface."

The move is to larger systems

In addition to being incorporated into programmable instruments, the 488 interface is being incorporated into computer-operated systems, according to Don Loughry, a Hewlett-Packard corporate interface engineer. Several other manufacturers are now providing bus-port interfaces, he adds.

A computer-controlled test system in Fairchild's new Logic System VII that uses multiprocessor techniques employs the 488 bus to simplify the addition of programmable instrumentation. And the latest disc-based Logic-Circuit Test System from GenRad, Concord, MA—the 1795—has an optional 488 instrumentation port.

The 488 bus's distributed-processing capability that links a group of microprocessors has been adapted to an application for which it was not originally conceived—an aircraft search system under development at MIT's Lincoln Laboratory. The bus's ability to connect several components of the radar system has simplified the system by eliminating the central computer needed in previous systems.

"While we've already used the bus on a small airborne radar, we have five or six other radar projects that we're going to use it on," says C. Ed Muhe, leader of the radar-techniques group at the Lincoln Laboratory.

Bus is central system element

"With the usual digital system, the first thing you think about is the central computer," Muhe notes. "But with the bus, we do just the opposite, we think of the bus as the central element of the system. And all the functional modules tie onto the bus.

"The basic idea is to functionally divide the system into parts that require the minimum amount of communication between them. We put enough microprocessor intelligence into each part so that communication on the bus is fairly small."

"As an example, the digital display has to be refreshed about 30 times a second, and the refresh function is put into the display with a local microprocessor. The display is updated only when there are changes in it, and this update is easily handled by the bus using rates of about 0.5 Mbytes per second."

Slow or fast µPs are used, depending on the requirements, Muhe points out, and the 8080 and 2901 are Lincoln Laboratory's favorite choices.

The bus saves substantial design time—a major advantage, according to Muhe. Using the 488 with standard building blocks to construct the radar systems means, for example, that a display can be connected with its µP into another radar. With the standard interface, it's necessary only to plug it into the bus.

"While I know the bus offers a tremendous advantage in designing several systems using the same functional units, I think that the bus means less design work even for one system," Muhe concludes.

Programming is still a problem

Eugene Fisher, design engineer at the University of California's Lawrence Livermore Laboratory, Livermore, CA, is enthusiastic about using the 488 for interfacing instruments to minicomputers at the laboratory. With the proper bus interface, Fisher points out, he can acquire an
A microprocessor-based digital plotter, the Tektronix 4662, is a leader in the trend to provide plotters with the IEEE 488 general purpose interface as standard.

instrument for a particular instrumentation setup and simply plug it in.

"All I have to do then," he notes, "is learn how to program it," notes Fisher, adding: "This is a continuing problem with each new instrument because each instrument manufacturer is interpreting the bus specification slightly differently."

Programming individual instruments has been a problem for some time because it has not been spelled out in the original specs.

"Work is continuing in the standards area relative to software," says Don Loughry. "I prefer to call software 'codes and formats,'" Draft documents are being generated and will be reviewed this month at the International Level in Europe in the parent committee of Technical Committee 66."

Historically, the interface of early programmable instruments has been the parallel, four-bit BCD bus, which is still available in standard form in the majority of today's instruments. But the demand for it is falling while the demand for the 488 interface rises.

As a result, instruments already on the market, but still reliable and highly useful, are now being retrofitted with IEEE 488 interface cards or modules. The Model 605-145 ASCII interface developed for Exact Electronics Models 605 and 606 Programmable Waveform Generators is a good example. Only an inch and a half high, the new 488 interface module of the Hillsboro, OR, firm sits on top of the 3-1/2-in. rack package of the 605 and 606. The total package is only 5-1/4-in. high and fits into a 19-in. rack.

Keithley's new portable 4-1/2-digit, 30,000-count DMMs, Models 172 and 173, are being provided with a 6800 µP-based IEEE 488 interface module (available in January, 1977).

Because these instruments are small, the interface module of the Cleveland manufacturer is a separate unit, not a plug-in card.

Three DVMs from Dana Laboratories—the 5000, 5900 and the 6900—are designed with integral BCD outputs. A piggyback package of the Irvine, CA, firm, the 55, designed with a microprocessor-controlled interface, is used for interfacing between the BCD outputs and the IEEE 488 bus.

For the Dana 9000 Counter-Timer, which uses
A complete automatic measuring system for production or incoming inspection is provided by this Electro Scientific Industries LCR bridge. It has a 6800 µP.

an Intel 4004, the interface is incorporated within the box.

The number just gets bigger

Microprocessor interfaces are found in a number of other instruments. For example, the Model 296 wide-range LCR bridge from Electro Scientific Industries, Hillsboro, OR, incorporates a 6800 µP to provide calculating power in the instrument as well as provide the 488 interface. The 2961 is not yet supplied with the standard BCD outputs.

"The instrument can be programmed remotely, including sequencing a mixture of tests,” according to Jim Currier, instrument product manager. "For example, a capacitor can be measured, followed by a resistor. Or it can be controlled to provide multiple-component, high-speed testing.

"A 10-limit sorting capability is available, using a plug-in option card,” Currier continues. "So, with one instrument you have a complete measuring system for production or incoming inspection."

A special feature incorporated in the digital bridge is the ability to do either percentage deviation or absolute deviation. Instruments have traditionally come with either deviation measurement.

The instrument program can be changed easily by simply substituting another program ROM in the µP, notes Currier.

The SMPU Test Assembly by Rohde & Schwarz, Fairfield, NJ, is a microprocessor-controlled, IEEE-bus compatible automatic test set for transceiver measurements. The system, whose deliveries have just begun, contains multiple instruments required to test both transmitters and receivers automatically.

Control comes from a card reader or through the Tektronix TEK 31 programmable calculator. Where more elaborate programming facilities are required, the Tektronix 4501 Graphic Computer system is used.

The SMPU is connected to the calculator through the IEEE bus.

The microprocessor is used for setting up and maintaining subroutines and for preventing erroneous and potentially destructive measurements. For example, if the transmitter test is selected by pushing the “transmitter” button, no type of receiver test can be called up, because the system will refuse it.

Not all microprocessors used in instruments function as a part of the bus interface. For example, the 4004 µP in the Systron-Donner 7115 DMM provides intelligence for internal data calculations, self-calibration and troubleshooting.

In the 7115—and in three other of the Concord, CA, manufacturer’s instruments that interface with the 488 bus—the DPS 50 Power Supply, the 1600-series Microwave Synthesizers and the 6054B Microwave Counter are normally supplied with the BCD and the 488 interfaces as plug-in card options.

Camac systems take the 488 bus

The influence of the GPIB is spreading to the process-control field. Users of the Camac systems (IEEE 583) are providing the 488 bus with interfaces so that instruments that are physically incompatible with the Camac modular system of hardware—programmable attenuators, DVMs, and displays, among others—may be added.

Use of the Camac system is pretty much divided between nuclear instrumentation and process-control instrumentation.
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Many major instrument manufacturers are now integrating a variety of different test functions into a single unit. The goal? A synergistic instrument with features that go beyond the result of simply putting together two single-function instruments.

The resulting instrument is usually more compact (less bench space needed), easier to use (not only in the lab but also in the field), and often considerably cheaper than if each component instrument had been purchased separately.

One element of the combined device can often be used to check another. In a combined oscilloscope-frequency meter, for example the frequency-counting element can provide a digital readout of the scope unit’s sweep rate. This capability thus establishes a separate verification of the accuracy of the scope’s sweep-speed dial setting.

All but the kitchen sink

The digital multimeter-counter-miniscope, Model PS 915A/975A ($1295) by Vu-Data Corp., San Diego, CA, is an example of this new breed of test instrument. Small despite its lengthy title, this test instrument is the first to combine a digital multimeter (DMM), a frequency counter and an oscilloscope in one package.

Each of these measurement functions possesses its own dedicated display, and each may be used independently or simultaneously, or to complement each other.

The PS 915A/975A provides synergistic convenience by connecting all three component units internally. Only a single probe (to the item tested) is needed to permit test measurements. This arrangement eliminates the often cumbersome external wiring interconnections required among the three instruments when used separately or even together.

Performing a conventional set of measurements on a power-supply circuit provides a good example of the convenience offered by such a combined instrument. The DMM portion can

Samuel Derman
Associate Editor

ELECTRONIC DESIGN 24, November 22, 1976
Measuring time intervals (to 1% accuracy), voltage, resistance, and even temperature (all digitally) is possible with the Tektronix DM 44 scope option.

measure and display the dc level, while the ac-ripple amplitude is displayed on the scope’s CRT. At the same time, the ripple frequency is monitored and displayed digitally by the counter.

The Vu-Data PS 915A/975A is basically three instruments in one:
- An autoranging DMM, with its readings displayed on a 3-1/2-digit LED panel, measures ac and dc voltage as well as resistance.
- The scope, which carries its own model number, PS 915, provides vertical sensitivity of 10 mV per division at a 20-MHz bandwidth. Fastest sweep rate is 100 ns per division with the possibility of an increase to 20 ns per division by a five-times magnifier.
- The frequency counter, which is activated by the scope’s trigger pulses, digitally presents the frequency of the signal displayed on the scope’s CRT.

An “external-trigger” scope mode is also available, so that the frequency of the externally applied signal can be measured, whether this signal is displayed on the scope or not. A full four-digit LED display supplies the frequency readout.

In the “ac volts” mode, the device’s DMM will give the RMS value of a sine wave appearing on the scope, so “eyeball” measurements of the peak-to-peak voltage amplitude, followed by the usual calculation to reduce this measurement to RMS value, are unnecessary.

Compact capability

A serious competitor in the combined-instrument race is the Versatester by Systron-Donner Corp., Concord, CA. Designed not only for R&D work but also as a production and service test instrument, Versatester combines a multimeter, a signal generator and a frequency counter in a compact package. A single four-digit LED display with automatic decimal point supplies the readout for all component instruments.

Versatester offers a useful variety of devices and functions:
- 20-MHz frequency counter with autoranging.
- 20-MHz pulse generator.
Systron-Donner's Versatester generates pulse, square and sine waves from 20 Hz to 20 MHz. It also functions as a dc power supply and as a 4-digit multimeter.

Lab-All, manufactured by UFAD Corp., uses a precise filter to perform a wide variety of signal phase, spectrum and distortion analyses.

- 20-MHz square-wave generator.
- 20-MHz sine-wave generator.
- Dc-power supply (available voltages are +5 V, ±15 V and ±30 V).
- Multimeter (ac, dc and ohms) with a four-digit readout. In ac-voltage mode, voltages can be measured whose frequency is as high as 20 MHz.

Versatester's instruments all run continuously. For example, a sine-wave output is available simultaneously with pulse or square-wave output. Also, the multimeter modes can operate at the same time any one of the signal-generating modes is used.

The Versatester's synergesty results in cost effectiveness, convenience, and portability. The cost is appreciably less than the sum of the costs of Versatester's individual components, says Norm Whitla, Systron-Donner's product manager. There are hidden savings too, Whitla adds. Fewer spare parts need be stocked, and only the one, basic instrument must be calibrated.

Pint-sized test package

Joining the race is a digital multimeter (DMM) and oscilloscope ($1200) from Tektronix, Beaverton, OR.

Weighing in at 3.7 lb and occupying a space 3.0 x 5.2 x 8.9 inches, the Model 213 is small enough to be held in a hand, or carried in a briefcase or tool kit.

Unlike the Systron-Donner Versatester and the Vu-Data PS 915A/975A, which use LEDs for the digital display, the 213's numeric figures are projected directly on the CRT face (in 3-1/2-digit format). Although this arrangement does not permit the operator to view the waveform and read the voltage simultaneously, a single pushbutton switch permits instant changeover from one type of display to the other.

The DMM can measure voltage (dc and RMS ac), ohms and current. Measurable dc voltages range from 0.1 V to 1000 V, and measurable current from 0.1 mA to 1 A full-scale. Resolution of the DMM is specified as 100 µV for voltage measurements and 100 nA for current readings. Frequency range of the 213's scope is from dc to 1 MHz. The scope can also display current waveforms, unlike most field scopes of this type.

A second multifunction test device from Tektronix, the DM 44, is not a complete piece of test gear, but an attachable module for the Tektronix 464, 465, 466, 475 and 475A portable oscilloscopes. This optional feature provides:

- 3-1/2-digit LED readout.
- Direct numerical readout (with 1% accuracy) of the time interval between two signals presented on the scope's CRT.
- Delta-delayed sweep for very fast time measurements (i.e., pulse width, rise time).
- Dc-voltage measurements with 0.1% accuracy.
- Resistance measurements with 0.25% accuracy.
- Temperature measurement from -55 C to +150 C.

Linking the DM 44 module to an oscilloscope produces a highly versatile piece of test equipment—one that can make precise timing measurements (1% accuracy) and can perform gen-
eral circuit troubleshooting. The DM 44 option adds $410 to the price of the selected oscilloscope. The temperature probe can be omitted if not required, however, and the price drops to $335.

**A DMM you can count on**

For applications that require a frequency counter combined with the capabilities of a DMM, Valhalla Scientific Inc., San Diego, CA, has a 4-1/2-digit multimeter counter Model 4440.

For $299 (plus an extra $50 for the counter option), the purchaser gets several capabilities: dc and ac (RMS) voltage measurements from 200 mV to 1000 V, input impedance of 1000 megohms on the 200-mV and 2-V ranges and 10 megohms on all other ranges, current measurement (dc and ac) from 200 µA to 2000 mA, resistance measurements from 200 Ω to 20 kΩ, and frequency counting from 2 kHz to 20 MHz, with accuracy of 0.01% ±0.005% of full scale.

The frequency counter is actually usable 7 MHz beyond its 20 MHz limit for measuring citizens band (CB) signals, says Harold Clark, Valhalla's president. Above 20 MHz, the counter indicates "overflow," and the first significant digit of the readout is missing. However, since CB frequencies all fall into the 26 and 27-MHz range, the value “2” for the first digit is understood.

A variety of available options extends the capability of the Model 4440.

For data-communications measurements, the user can determine the time duration of the tone burst signal—a low frequency sine wave burst sent over telephone lines to indicate that a remote operator wishes to communicate with a computer. The duration of such signals must be precisely controlled, and in cases where dozens, even hundreds of telephone lines link up to a central computer, checking out these time intervals can be exceptionally tedious. The 4440's data-communication option speeds up this testing process.

Temperatures can be measured via an optional probe that generates a dc voltage of 1 mV/°C. When the user switches the digital multimeter to the 200-mV range, the meter becomes a direct reading thermometer up to a maximum of 150 °C. Temperature resolution is specified as 0.01 °C, but over-all temperature accuracy is limited to 2 °C.

A pulse generator/pulse supply package, the Logiklab 151 ($79.50) from Integral Electronics Corp., Commack, NY, is designed to be both a lab-testing device and a teaching tool.

The power supply is highly regulated, short-circuit proof and capable of delivering 1 A at 5 V dc. The signal source in the astable mode simultaneously provides true and complementary TTL-compatible square waves and pulses ranging from 10 Hz to 100 kHz.

In the monostable mode, single pulses whose widths vary continuously from 5 µs to 50 ms are produced by either a manual or remote trigger.

**Multimeter race is on**

A tendency within the combined-instrument trend is to add temperature-measuring capability to the gamut of multimeter functions. Harold Clark, president of Valhalla Scientific, explains:

"Let's say a design engineer—one who typically uses a multimeter—has designed something that uses a power transistor. The power transistor gets hot, and the engineer needs to know just what the temperature rise is. That's a pretty universal need.

"Now he's not willing to go out and spend $1000 on a temperature-measuring digital meter. So if you (the manufacturer) have a low-cost temperature-measuring option on your multimeter, the engineer will buy your product."

Philips Test and Measuring Instruments, Woodbury, NY, and Logical Technical Services (LTS) Corp., New York City are just two of a growing number of firms that currently offer a multimeter that can measure temperature.

Philips has two models available, the PM2513 and the PM2527. Using an LSI circuit, the 2513 multimeter functions with 26 ranges and a temperature-measuring option (−50 to 200 °C)—all
within its 3-lb package. A 3-1/2-digit LED read-out provides the display.

Higher accuracy, autoranging, extended dc-voltage range, 4-1/2-digit display, and wide bandwidth on ac measurements (30 Hz to 100 kHz) come with Model 2527. This version not only can read surface temperatures between -60 and +200°C, but also can measure the surface temperature to 99% of final value within 10 seconds (See ED No. 11, May 24, 1976, p. 137).

A small hand-held DMM from LTS uses a semiconductor junction tip to provide temperature-measuring capability. Autoranging and autopolarity also come with this Model 12T, which supplies readings via a 3-1/2-digit LED display. Accuracy for dc-voltage measurements is specified as 0.1%, and temperature-measurement range is -55 to +153.5°C.

Four AA-sized rechargeable NiCd batteries provide power for the 12T, which also has an ac adaptor/charger. (See “Portable Instruments: The Specs Are Fine, but Their Batteries Are Still Short-Lived,” p. 60.)

![Philips Model PM 2513 DMM](image)

Philips Model PM 2513 DMM is also equipped to measure temperatures. Temperature range is -50°C to +200°C, with resolution to 0.1°C and accuracy of ±1 degree.

A new phase in measurements

A single low-cost ($2495) instrument from UF AD Corp., Grand Rapids, MI, simultaneously measures phase shift, voltage gain, and network distortion.

Known as Lab-All, the device uses a filter to select a precise band of frequencies. The exact bandwidth can be set to customer’s specifications anywhere from 0.01 to 3000 Hz.

Determining the frequency components of a complex signal is just one of the many functions this filter can perform. Not only can the filter’s center frequency be positioned manually anywhere in the band from 30 Hz to 100 kHz with a front-panel control, but the filter can also be caused to sweep through a range of frequencies—in the manner of a spectrum analyzer—by injecting an external sawtooth voltage.

Lab-All comes with the following:

- Tracking bandpass filter (constant area filter). Shape of bandpass is such that at 60 dB down, bandwidth is only twenty times the 3 dB bandwidth.
- Quadrature outputs. At the selected frequency, dc voltages proportional to both the sine and cosine components of the signal are available as separate outputs.
- Tracking notch filter.
- Sweep filter.
- Wave analyzer.
- Spectrum analyzer.
- Distortion analyzer. (The rejected frequencies are available as a separate output.)

In addition to its wide variety of general applications, the Lab-All has been used in many special situations, according to Tony Heibel, UF AD’s vice president:

- “Nondestructive testing” of humans to determine the degree of hardening of the arteries. A broadband noise signal was applied to a portion of a human limb in an experiment conducted at Michigan State University. After the signal had passed through the subject’s body, Lab-All examined its frequency spectrum. The researchers discovered, interestingly enough, that the blood flowing through arteries coated with fatty deposits affected the transmitted signal so that its frequency spectrum differed measurably from a similar signal passing through subjects with lower arterial deposits.

Lab-All was used because its precise narrow-band capabilities could pick out the frequency differences.

- Balancing rotating machinery, such as crankshafts. Lab-All can accurately determine the amount of unbalance by measuring frequency variations.
- Tracking signals buried in noise or measuring signal phase with the aid of a scope. Lab-All is such a precise tracker, Heibel points out, that it can track a signal as low (relatively) as the 101st harmonic of a square wave.
- Other applications include measurements of noise and doppler frequency shifts and speaker and microphone testing.
- A scope CRT overlay, calibrated in both amplitude and phase is provided. By varying Lab-All’s frequency, a Nyquist plot is generated on the scope screen. ■
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For measurement convenience, the 1741A has a selectable 50Ω input in addition to the standard 1 MΩ input. A 5X magnifier permits two channel measurements as low as 1 mV/div. to 30 MHz, without cascading. The 1741A is priced at $3,950*.

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American engineers and their European counterparts are both engaged in the same thing: designing. But they go at it in very different ways.

The American engineer has a way of cost-thinking that the European doesn't. He has a better feeling for how much money he should put into the design of a new instrument.

I know of one European company whose product planning meetings always started at the wrong end: They began with the customer's needs when they should have begun with his money. How much was the customer prepared to spend? How much performance and reliability could he get for this amount? How much resolution? How many functions?

The American engineer is a master of compromise and of doing things inexpensively. The color television set, for example, is a remarkably complicated machine that is produced very inexpensively.

Europeans haven't really learned compromise yet: they look first at performance. They get a block diagram and say, "let's design this instrument." Only later, after it is produced, do Europeans try to see how to make it cheaper.

The American engineer is much more adjusted to reality than the European. The European engineer wants to design the best in the world. The American engineer wants to design the most marketable.

European pride in design is overvalued and runs up the cost. Not only does this pride cause more performance to be designed into an instrument than the customer needs or wants to pay for, but it even stifles teamwork.

I recall once when two groups of engineers were designing synthesizers—each group was building "the best synthesizer in the world." Eventually, they became so competitive they wouldn't speak to each other. No one wanted to give any tips away to the opposing team. So
Ulrich L. Rohde, whose father is co-founder of Rohde & Schwarz, Munich, not only markets company products in the United States, but also designs instrumentation to be built in the United States.

they ended up with two excellent synthesizers—both so expensive no one would ever be able to afford them. So they had to be redesigned.

In America, the two groups would have talked with each other—possibly at lunch or while playing baseball—and they would have turned out one synthesizer in half the time and at a much lower cost.

European engineers—and the Japanese, apparently—are brought up to think that to earn money, they have to spend years and years designing something that’s never been equalled before. But by the time it is finished, the product is no longer needed or new. European engineers should settle on some in-between point of view that’s less theoretical and more practical.

Another reason Europeans design instruments with high performance specs is that most European governments require them.

This “excellence” works to the Europeans’ disadvantage when they try to sell in America. Americans say, “You have a fantastic machine, but it does too much; we don’t want to pay for what we’re not going to use.” For example, Rohde & Schwarz has an excellent signal generator used for blocking tests as required in Germany, but such stringent tests and specifications are not required here. Hewlett-Packard has a similar machine that does only what the FCC now requires and costs less than Rohde & Schwarz’s. So how do we convince an American to pay more for something he doesn’t need?

European manufacturers will probably adopt American practicality in the next five years or so, anyway, because of the increasing availability of information. Not only are the American journals like ELECTRONIC DESIGN well read in Europe, because so many European engineers learn English in school, but now there’s more personal contact with Americans. With the devaluation of the dollar, Europeans can now afford to travel to the United States to attend symposia and trade fairs,
and visit U.S. government agencies and industries. The dollar was devalued in 1968. So, actually Europeans have only had eight years of this personal exposure to American ideas.

One thing I don’t understand is how American engineers can buy an instrument that not only barely does the job, but becomes obsolete in a couple of years.

Europeans like to have instruments that go far beyond their needs. But I suppose the American engineer can’t be blamed completely; it’s the management point of view that prevails.

The difference between the European and the American engineer begins in school. The American’s education is more practical, the European’s more theoretical.

I’m sure the German engineer, fresh out of school, typically knows more mathematics than the American. He goes more deeply into things. I’d also bet that the European engineer in general knows much more, mathematically, about the circuit he designs, and why he did it that way, than the American.

I have talked with people who admire me for some particular detail I happen to know. But, actually, the detail has very little meaning; I just learned it in school because I had to. Anyone can memorize a lot of formulas and equations—and later forget them or not even need them.

The Japanese have a similar in-depth background. Look at any copy of Proceedings of the IEEE and you’ll find that most of those articles that contain those almost unreadable mathematical descriptions are authored by Japanese.

After the first two years in a German engineering school, every student must take on a special project—usually a mathematical problem—that he must finish successfully in order to get his diploma. Here in America, the special project would be to build a product, not solve a mathematical problem. The result is that the American is much better prepared for his job than the European; indeed, he’s about two years ahead of a German engineer. If a German engineer is hired right out of school, it usually takes about a year before he can be used.

Another way the American engineer and the European differ is in their motivation. The American wants excitement and glamour. He likes to move from one job to the other. And he wants to work where he can play golf or swim or whatever it is he likes.

The American is more extroverted than the German. He dresses better, and—this is a metaphor for his whole point of view—his house and car are more flamboyant. He’s more caught up in status than the German.

The European in general is more interested in job security, fringe benefits and retirement plans. He also wants to excel at his work and be recognized for his engineering skills and achievements.

American engineers differ radically from their European counterparts in their willingness to exchange information.

Americans like to talk about what they’re doing, while in Europe everything is a big secret.

I have seen things at Hewlett-Packard, for example, that I would never see at a German company as a visitor.

Maybe Americans are more open because of pride—they like to show people what they’ve achieved. More likely, however, Americans realize—whereas Europeans don’t—that most proprietary secrets don’t mean very much. If Rohde & Schwarz, for example, learned all of American Company X’s techniques for making better oscilloscopes, Company X would still make better oscilloscopes. It would probably have its own IC department, make its own CRTs, and would have evolved its own manufacturing procedures. However, I’m sure that Company X wouldn’t find it so easy to produce military communications to compete with Rohde & Schwarz in Europe.

Communication is important because people are like wolves. They occasionally like to be by themselves, but they do best when they’re together. If someone is isolated, he’s either sick or in
trouble. Once when I was a development manager, I instituted weekly meetings where engineers could tell their colleagues what they were doing.

Are Americans good salesmen?

I used to meet American salesmen who had come to Germany to sell semiconductors or instruments. And I admired them tremendously. They had the courage to come to a foreign country where they couldn't speak the language. They had to rely on finding enough German engineers who spoke English to be able to function.

If these men didn't make a sale, however, it was usually because their company didn't back them up. The company couldn't assure its salesman that the component he was trying to sell would still be in production by the time the European customer needed it in large quantities. It has also happened that by the time the European company has finished a design, the desired component was no longer being produced, and we had to start over again.

American salesmen are even good in America, considering the red tape everyone must go through to sell to an American firm.

In Germany, a department head often needs about five internal signatures to buy instrumentation for his company. Here in the United States, I've seen companies that require 10 or 12. Any salesman who can get through all this red tape has to be admired.

European engineers also differ from Americans in their approach to writing specs; the Europeans are more conservative than aggressive. European engineers promise the very minimum a product can achieve so the customer who gets the one product out of a hundred that falls to that level won't be disappointed.

Americans, on the other hand, pride themselves on their "specsman ship." A clever sales force can put an instrument's best spec forward, so to speak. Or specs can be written in a way that's hard to interpret for all cases. Europeans haven't done this yet.

How do Europeans sell to the American market? That's what I'm here to find out.

Back in 1967, before the dollar was devalued, American instruments were expensive in Europe and European products were cheap in America. Rohde & Schwarz sold easily in America, but Europeans found it difficult to buy American products. I remember the HP spectrum analyzer—it was practically the only one being made, and it was unbelievably expensive.

Then the dollar went down, and American products were in great demand in Europe. They hadn't suddenly become better, just cheaper.

European-made products are more expensive to produce than American-made products because, first of all, European labor is expensive—there are so many fringe benefits that Americans don't have. For one thing, it's almost impossible to fire a German engineer. Germany is probably the only country I know that has a strong engineer's union.

Also, some European products contain American-made high-technology components, which means the factory in Europe has had to wait to receive the shipment from the United States; it's no doubt had to hassle with customs, and it has had to deal with, and pay, distributors.

The solution is to produce a reliable product that's in demand and that's economically competitive, which rules out digital voltmeters and counters right away. I'd like to know how many people got burned making these devices. The

Who is Ulrich Rohde?

Ulrich L. Rohde is winding up his second year as president of Rohde & Schwarz Co., (USA), which has offices in Fairfield, NJ, and a territory that covers the entire United States including Puerto Rico.

Besides marketing products manufactured by Rohde & Schwarz, Munich (Rohde's father, Dr. Lothar A. Rohde, is one of the company's founders), Rohde himself is also designing products for manufacture here in the United States.

Born in 1940, Rohde studied communications engineering at the technical universities of Munich and Darmstadt, and after working for other companies became head of the Research and Development Div. for Military Communications Equipment of AEG-Telefunken in Ulm, West Germany.

A Senior Member of the IEEE, Rohde has published more than 40 articles in the field of communication engineering. While still in school, he wrote a book on the behavior of transistors at very high and ultra-high frequencies.

"My father had always said that if you wanted to become an expert in a subject, write about it. I did and it was a great success; it sold 20,000 copies, which is a lot for a book published in German. But it didn't win me any friends at school. People thought I was presumptuous, I suppose, writing a technical book while still an undergraduate.

"How did I get from Munich to Fairfield, NJ? I'm here to learn how to sell European products in America, what changes in design and in philosophy you need to be successful here. Because once you are successful in America, you're successful worldwide."
number of them being offered is unbelievable.

Rohde & Schwarz’s latest really successful instrument is not an inexpensive, bread-and-butter product; it is the SMPU, a fully automatic, radio-telephone test set assembly.

Rohde & Schwarz is selling the SMPU for less than HP’s comparable Bigfoot. Our SMPU is about $45,000. We’ve sold to RCA and General Electric, which use them in the production of their communication equipment.

How did we do it? It was very simple. We used a lot of things we already had available, and we put them all into one box, using only as much of a device as we needed and no more.

We took the most significant assemblies of a digital voltmeter, an audio-distortion analyzer, a power meter—only those portions that we needed—and automatically, the SMPU became cheaper. Basically, we ended up with a computer-controlled magazine full of PC boards and one μP. The main cost was for the software.

Learning to produce more for less is the only way to compete. And we’re learning. We have several more instruments in the works that we also feel will be successful.

Why did I go with the competition? I didn’t go with my father’s company for several good reasons.

I wanted to be on my own. I didn’t want people to think that I was qualified by heritage alone. I knew I was a good design engineer, and I wanted to prove it. At Rohde & Schwarz, I knew I’d be handicapped in my day-to-day work by being the president’s son. If you were my boss, for example, you’d feel a little funny knowing that my father was president. Also, I knew if you and I should reach a roadblock on a technical issue, and we went to my father, he’d side with you.

I thought it was better to gain experience by working in a company other than Rohde & Schwarz, Munich, which my father and Dr. Schwarz started in 1933.

My first contact with an outside company, however, would never have turned out well if I hadn’t been able to deliver the goods—if I hadn’t been a good designer at 19, when I was still in school.

One day, one of Telefunken’s top engineers, Prof. Werner Nestel, came to our house for lunch and, noting my studied silence, asked me afterwards what was wrong. So I told him. After school, I had built an amateur radio receiver in the cellar of the house, and it had worked like a charm. But when my father came down to see it, he unfortunately grasped an uninsulated wire.

To teach me a lesson for my negligence, he locked the cellar door when we left, and I couldn’t get back in.

Don’t worry, the professor told me. He would do something. What? Get the key? No, he couldn’t do that. But a few days later, I received a handful of transistors—the very first vhf/uhf transistors ever built in Germany. And with them I built an FM radio, probably one of the first in Germany. I sent it, and my thanks, to the professor, who in turn sent me his thanks and a check for the design. Telefunken then produced the radio.

After finishing my education and working for several small companies I was hired by Prof. Nestel at Telefunken as a design engineer and division manager.

Here in New Jersey, I’m a salesman. But I spend quite a few week-ends here in the office building synthesizers. One was for a microwave project. I have already sold the first piece.

Now I couldn’t have done this at Rohde & Schwarz in Munich or at Telefunken. They’re both too big. I’d have ended up with difficulties. And that’s normal. There must be rules. Everyone can’t go around doing whatever he likes. But I’m the boss here in this sales office and I can do what I like—on week-ends.

Do you know what I always wanted to do? I had good experience in Europe with big companies and I would really have liked to see how a big American company works from the inside. I’d like to have worked as vice-president of engineering for something like Hughes Aircraft, or another big company, where I could work with radio communications designers.

But now I enjoy promoting Rohde & Schwarz and other companies in the United States and have even organized some manufacturing here.

America spoils me. If I had the choice of going back or staying here, I think I’d be in trouble. I like it here, my wife does. We have a 15-month old daughter who has an American passport. I have a house here I couldn’t have near Munich—there’s not that much space near Munich. No one there has a one-acre lot.

I am able to keep in touch with my friends in Germany. I get up every morning at six and talk to them by my short-wave radio at home. It’s their lunch time then. And would you believe that just outside of Fairfield, here in the woods of New Jersey, there’s a very good little German restaurant? Good German beer, wurst, sauerbraten—whatever you like. Let’s go! And when we come back, I’ll give you some Leberkäse to take home; there’s a good German butcher not far from here. •••
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The demand for ever greater precision in the laboratory, on the bench and on the production line continues in the face of the tightening budgets that design engineers must face. Competition is forcing engineers not only to squeeze more information capability onto ever narrower frequency bands and more bits into conversions, but also to interface with more powerful computers.

These competitive advances require improved standards and measuring equipment, and, fortunately, many basic standards can now be specified to greater accuracies than ever before. The basic standards for voltage and capacitance, and from these, standards for resistance and current, are now very precise. Frequency and its reciprocal, time, the most precise parameters, are increasingly available in standalone hardware and in a variety of existing broadcast or planned orbiting satellite distribution systems.

NBS—keeper of the keys

The U.S. legal standards, maintained by the National Bureau of Standards (NBS), approximate the accepted international (MKS system) definitions of electrical measuring units. Volt, farad, ohm and ampere standards are set by the Electricity Division of NBS in Gaithersburg, MD; the nation's master clock is the responsibility of the Time and Frequency Division in Boulder, CO. The standards are stringent: for electricity, NBS measures accuracy down to parts per million; for the master clock, accuracy is a matter of picoseconds.

NBS makes every effort to disseminate these extremely accurate values to industry; conversely, secondary (industrial) standards sent to NBS by its industrial customers are calibrated against its primary standards. Measurement Assurance Programs (MAPs) ensure that industrial total measurement processes are reliable. Time and frequency are distributed via VLF radio transmission and satellites.
Repeatable color performance from monitors is obtained with Tektronix' J16 photometer. Any number of monitors corrected to a color temperature of 6500 K can be matched for color even at separate locations.

But how accurate are the values of the basic standards themselves? The entire measurement process depends on the precision of the NBS standard. Fortunately, some of the basic standards have recently been made extremely precise.

The volt is now more precise

Increased precision for the standard volt has been achieved by using the ac Josephson effect to calibrate the average value of the voltage standard itself, a bank of Weston cells. The ac Josephson junction is the most accurate voltage source ever, and its voltage, a series of steps, is known to a few parts in $10^{-8}$.

The Josephson junction is a frequency-to-voltage converter in which, the tunnel junction of two superconductors—separated by a thin insulator, properly biased with dc current and irradiated with microwaves—produces a series of voltage steps proportional to the microwave frequency. Its proportionality constant depends on the values of the electron's charge and Plank's constant, and is known to better than one part in $10^{-8}$.

As a standard, the Josephson reference has three advantages:

- The junction itself is readily reproduced.
- The thin films are permanent structures that require no mechanical adjustments before calibration.
- The junction requires no cleaning or reconditioning.

There are drawbacks, however. The superconducting junction requires nearly absolute zero temperature; output voltage is only 5 mV per junction; and the process is time-consuming. NBS uses two junctions in series for 10-mV output, but the circuitry needed to scale the output up to the 1-V level at cryogenic temperatures is a source of error. Because calibration with the Josephson effect takes so long, even the NBS doesn't calibrate its standard cell bank more than once a month.

Capacitance is the most precise electrical unit

Currently, the most attainable electrical standard is the unit of capacitance, the farad. With the Thompson-Lampard capacitor as the basis for calibration, the U.S. legal farad standard is calibrated to 0.02 parts per million of the international definition.

The Thompson-Lampard is a variable-cross-type capacitor, with a grounded conductor rod passing through its center. Moving the rod between its extremes results in a 1/2-pF change in capacitance. This value is precisely calculable to less uncertainty than two parts in $10^{-8}$, in terms of only one variable—the distance the rod is
moved. This distance is measured on a stabilized laser interferometer built into the device.

The U.S. legal farad standard consists of a bank of five fused-silica dielectric capacitors, each with a value of 10 pF.

Resistance is calibrated to the capacitance standard. The equipment used to perform this calibration is so accurate that the U.S. legal ohm is less than 0.06 parts per million from the internationally defined ohm—despite the numerous calibration steps involved.

The precision to which the ohm and volt standards are known have limited the fluctuation in yet another standard—the ampere. An absolute determination of the ampere is carried out at NBS only once every ten years or so because the procedure is so cumbersome and inexact. A balance measures the force produced by current flowing in two conductors. But this method has as much as 15 parts-per-million error. The volt and ohm standards can be used to produce the ampere to an accuracy of 0.07 parts per million.

**Frequency is the most precise standard**

The most accurate standard available, frequency, is derived from the hydrogen maser. The hydrogen maser is capable of stabilities of 1 part in $10^{-14}$ for 100-s averaging and 2 parts in $10^{-15}$ for 1000-s averaging.

While they are ultra-precise, hydrogen masers are also expensive, large, heavy and sensitive to shock and vibration. But precision hydrogen masers have been made that have a diameter of only 19 in., a height of 30 in. and a weight of 80 lb. These have been applied in airborne-relativity experiments.

Since, for most applications, the maser's ultimate precision is superfluous anyway, the less precise atomic-frequency standards, cesium and rubidium, are widely used in industry. Also, quartz-crystal standards are now available that offer surprising stability and spectral purity. The frequency stability is usually of the order $10^{-11}$ for rubidium standards and either $10^{-12}$ or $10^{-13}$ for cesium standards. On the other hand, quartz-crystal oscillations boast stabilities of $10^{-10}$ and even better.

In addition to atomic and crystal standards, precise frequency is available through WWVB, a VLF standard broadcast station run by NBS.

An alternative to WWVB for obtaining precise frequency is the use of a TV color sync-burst comparison. All four major TV networks (ABC, NBC, CBS and PBS) have extremely stable carrier frequencies. The frequency in their color bursts (3.58 MHz) is synchronized with atomic clocks.

The TV-color-sync-burst technique is accurate to 1 part in $10^{-11}$. TV network time is offset from the rest of the world's agreed time (UTC time) by 3000 parts in $10^{-11}$. Normal TV-network-broadcast signals are the NBS signal minus 3000 parts in $10^{-11}$.

Two NBS stationary Geophysical Orbiting Earth Satellites (GOES) now broadcast to the earth and cover the North American continent.

**Industrial low-frequency standards**

Today, low-frequency electrical instrumentation offers the variety of a flea market. Streamlined and softly colored five-and-six-digit meters stand alongside the walnut and black of the older, more staid analog devices, while stable components, using new materials and processes re-
Accurate rms measurements at zero dBm and zero dB levels are provided by W & G's EPM-1 milliwatt test set. Probe circuitry prevents thermocouple burn-out.

Place prosaic wire wound resistors. In the precision-instrument bazaar, a new generation of automatic equipment vies with the older, manual hardware. Nearly ultimate accuracy and lower, but cheaper, precision come in almost every instrument.

A reference that can maintain a unit of voltage with a 1-ppm precision at the one-volt level is now available from Superconducting Technology, Mountain View, CA. It consists of a Josephson junction with low-temperature Dewar, microwave and dc-bias junction sources, and a potentiometer.

In addition to its line of impedance standards and precision bridges, GenRad of Concord, MA, has introduced an inexpensive capacitance standard with 0.25% accuracy over seven range selections, from 1 µF to 1 F. The GR 1417 costs $775 and can be used as a standard for dissipation factor (D).

A fine-line process at Hewlett-Packard, Palo Alto, laser trims resistors on a sapphire substrate to ratios of 0.01%. The fine-line process was first used in HP's 3465 multimeter. Now, every DVM on the HP drawing boards uses the stable fine-line processed resistors whose values range from 5 Ω to 10 MΩ.

Automated standards are the trend at Ballantine Laboratories, Boonton, NJ. Ballantine's Model 1500A auto-balance ac-to-dc transfer standard, for measuring true rms-ac voltage, brings the precision of the standards lab to the calibration and manufacturing areas. Featuring 0.005% precision and calibration from 2 Hz to 30 MHz, this remotely programmable instrument reportedly can be used even beyond 100 MHz.

The feeling at Electro Scientific Instruments, Portland OR, about measuring dc resistance in the ppm range is that the measuring instrument's long term stability is degraded when its size is reduced and its speed increased. Consequently, the calibration cycle must be shortened.

Architected systems for test and calibration are a major involvement at Julie Research Labs in New York. Its Locost line of automated precision test and calibration systems are controlled by master programs on cassettes. The software asks the operator a series of questions to which he replies via keyboard entries.
The world's most accurate voltage standard, the Josephson junction (left) is mounted in a microstrip enclosure for microwave irradiation while held at -77 K or less. Capacitance is a distance function in the Thompson-Lampard variable cross capacitor (right).

Time bases for counters and local oscillators (LOs) for communication systems require precise frequency. Frequency counter time bases require frequency stability, while modulated-carrier communications devices are concerned primarily with having a phase noise (spectral purity) of low spectral density, especially near the carrier. This is especially true of digital systems where channels are spaced only 10 to 15 kHz apart; obviously, phase noise near the carrier is a crucial consideration when information is phase-modulated onto a carrier. And in the upcoming area of gigahertz timing, both phase noise and stability are important.

Frequency hardware is available

Fortunately, industrial frequency sources abound. New component quartz-crystal oscillators from Austron of Austin, TX claim a phase noise of -110 dB at 1-Hz deviation, -155 dB at 10 Hz and -180 dB at and beyond 1 kHz.

For Austron's 2010B Disciplined Frequency Standard, stability of a few parts in 10^13 per day is maintained for several months by the instrument's third-order servo loop. The unit's quartz oscillator is corrected from an input, say a cesium-beam standard or a Loran-C signal. The device then "learns" its frequency offset and aging rate and constantly corrects itself.

Hewlett-Packard's quartz oscillators emphasize long-term stability rather than spectral purity. HP's 10544A instrument is intended for use in communications systems as a counter's time base rather than a LO. The unit has a long term stability of 5 parts in 10^10 per day. However, the 10544A has pretty respectable phase noise characteristics—83 dB at 1 Hz to -145 dB at 1 kHz.

The -145 dB noise floor is partly the fault of the unit's switching regulator. At the beginning of 1977, HP's 10544B quartz oscillator will be available. This new instrument will have its internal dc generated by a linear regulator, and the noise floor for the unit will be lowered to -150 dB at and beyond 1 kHz from the carrier.

Arbiter Systems of Goleta CA, markets a Model 1011B frequency comparator for under $3000, which compares a unit under test to the standard TV broadcast color burst. The comparator requires eight cycles of the 3.58-MHz color burst to phase-lock. No warm-ups or adjustments are needed, and like any phase locked system, the uncertainty (error) is reduced by increasing the sampling time (averaging). However, averaging times with this system are in seconds rather than days, as with VLF systems. For example: a frequency may be tested to an accuracy (±1/2 LSB) of 10^-9 in 1 s or up to 10^-13 in 1000 s. ••

ELECTRONIC DESIGN 24, November 22, 1976
a new generation oscilloscope
HAVE YOU EVER NEEDED STORAGE 'SCOPe RESOLUTION THAT JUST WASN'T THERE?

In a storage 'scope you need better, not lower resolution, because what you capture will be all you'll ever see if the signal occurs just once.

Nicolet’s general purpose storage oscilloscope provides 20 times better resolution than the next best storage 'scope. And you don’t need binoculars or a microscope. You can electronically zoom in on any detail of interest. Quickly and easily, whether the signal is stored or live.
Hide a Waveform???

Some storage oscilloscopes can hold a trace, without fading, for so long a time that the instrument specifications merely say "holds until erased".

This is true of Nicolet's storage oscilloscope, EXPLORER. And a fine additional feature is that you can cause the stored information to be hidden away, out of sight, until you want to see it again. This means that you can use the EXPLORER for normal operations in the meantime. It isn't tied up by the holding process. You can tuck away several waveforms, out of sight. And can recall any of these, or all of them at once superimposed, for examination and comparisons. A minute, an hour, days, or weeks later.

Write-through Storage!

If you want to see the effects of small changes while they are occurring in a circuit system, it's great to be able to store the original waveform and continue to see live, ongoing signal waveforms superimposed on the original waveform.

Especially in the case of the EXPLORER, which allows up to 64X expansion of corresponding regions of both the stored and live waveforms. Changes of as little as 0.02% can be clearly seen and there's no limit to the length of time this can be continued. The stored signal doesn't degrade in the least.

What's Automatic Persistence?

Variable persistence storage oscilloscopes are useful for observing signals that don't occur often. The persistence time can be adjusted so that the trace fades by the time the next signal is expected.

Automatic persistence is better. The trace remains, without fading, right up to the time the next signal occurs. It doesn't matter how long or short the interval between signals, and no adjustments are needed. Nicolet's EXPLORER oscilloscope has automatic persistence.
Simple Signal Capture!

To capture a signal with the EXPLORER just press a "hold" button. To return to live action, press the "live" button.

There's no mode switching, no enhancement, no beam adjustment, no erase step and no sweep arming. The EXPLORER is much quicker and much easier to use.

To speed up reaction time, use a remote sensor to choose the interesting signal. It can decide before, during or after. That's important because sometimes neither you nor the sensor know that the signal should be held until the signal has started or ended.

Store a Week-Long Signal!

Storage oscilloscopes are handy for observing very slow signals. Sweep times as long as a minute, in a non-storage scope, result in a display that's not much more than a slowly moving dot. But a storage scope generates a clear trace representing the signal waveform, which is much better.

For longer sweep times you'd better borrow a pen recorder. Or use Nicolet's storage oscilloscope which has sweep times that range from microseconds to days.

Even if very slow signals are not your immediate interest, it's handy (fun, in fact) to record overnight or over-weekend changes in such variables as temperature or line voltage. With high accuracy and better resolution than a high precision pen recorder.

These are half a dozen significant new capabilities of the EXPLORER. There are half a dozen more, and a few more of less importance.

Hundreds of pleased EXPLORER users find them easy and natural to operate. In the words of one, "Anyone who has ever actually used an EXPLORER in his work will never want to go back (to the older 'scopes) again." Evaluated by one of the nation's largest laboratories, "An excellent oscilloscope — providing significant advantages."

EXPLORER is a low frequency, general purpose oscilloscope.

Bandwidth, 1, 2 or 5 MHz depending on plug-in.

The EXPLORER is pictured here with the Model 96A plug-in for two-input, 1 MHz applications.

To discuss details, order a brochure, or arrange a demonstration please contact Applications Engineer John Gericke.
New! Bi-polarity Silicon Transient Suppressors!

Can be supplied as JAN, JANTX or JANTXV to MIL-S-19500/516 (EL)

This new series of silicon bi-polarity transient suppressors is unique in that a single device will provide voltage transient protection symmetrically (i.e., provide protection for A.C. signals in addition to D.C.). This new series of devices has peak pulse power ratings of 500 to 1500 watts for 1 millisecond and its response time is effectively instantaneous (less than $1 \times 10^{-12}$ sec.). Therefore, these versatile devices have many protection applications where large voltage transients can permanently damage voltage-sensitive components. The devices are encased in Semtech’s Metoxilite, fused directly to the high temperature metallurgically bonded assembly. For use in commercial, industrial, military and space programs.

500 Watt
Peak Pulse Power

- Types: IN6102 through IN6137
- Breakdown Voltage (VBR): From 6.8 to 200 Vdc ± 10%
- Peak Surge Voltage (Vsm): 11.0 to 286.0V
- Peak Surge Current (Ism): 45.4 to 1.7A
- Temperature Coefficient of (VBR): 05 to .11%/°C
- Case Size (Max.): .140” D x .165” L

1500 Watt
Peak Pulse Power

- Types: IN6138 through IN6173
- Breakdown Voltage (VBR): From 6.8 to 200 Vdc ± 10%
- Peak Surge Voltage (Vsm): 11.0 to 286.0V
- Peak Surge Current (Ism): 136.4 to 5.2A
- Temperature Coefficient of (VBR): 05 to .11%/°C
- Case Size (Max.): .180” D x .165” L

4-LAYER DIODE IN METOXILITE!
Reduce circuit costs and increase reliability!

Semtech’s 4 Layer Diode (PNPN) is a silicon switch that is controlled by the amount of voltage applied. The application of this diode to a circuit often reduces the number of associated components which in turn, leads to cost reduction and increased reliability. Now available in Semtech’s proven Metoxilite construction as two terminal, fast-switching devices specifically designed for low voltage applications such as logic circuits, pulse generators, memory and relay drivers, relay replacements, alarm circuits, multivibrators, ring counters, and telephone switching circuits.

- Types: 1N5779 thru 93, 1N5158 thru 60
- Switching Voltage: 10 to 15V
- Switching Speeds: f(on) = 75ns, f(off) = 250ns
- Junction Capacitance: 150pF
- Case Size (Max.): .070” D x .165” L

1975 NATIONAL SBA SUBCONTRACTOR OF THE YEAR
An interesting horror story making the rounds of the instrument manufacturers deals with the manufacturer's responsibility for both safe use and safe misuse of his product. The story goes something like this:

A man buys a power lawnmower and has no difficulty mowing his lawn. After a while, he notices that his hedge needs trimming, so feeling, quite logically, that he already owns a power-driven, leaf-cutting tool, he starts up the mower and lifts it to do the hedge. But before he can cut the hedge, he cuts off a couple of his fingers. So the man sues the lawnmower manufacturer for not placing a warning label on the mower indicating that the grass-cutting blade is to be used to cut grass alone and is hazardous to fingers.

Now comes the horror part of the story: The man wins his suit.

Danger: high voltage

Warning labels are a step toward safe instrumentation that most companies are taking. Labels are being placed on high-voltage probes to warn the user about putting his hands in certain areas—for example, too close to the tip of the probe. Labels are also being attached on outside covers of high-voltage instruments, and internal cages that cordon off the specific high-voltage sections.

A red lightning-bolt design is becoming standard on front panels of instruments with high-voltage connectors. Some companies are even using the lightning bolt where lethal voltages may appear—for example, on voltmeter-input connectors. Here, the instrument doesn't generate high voltage on its input, but the input terminals become "hot" when high voltages are measured.

Liberal warnings can now be found within the text of specific measurement or calibration procedures outlined in instruction manuals. To make their point, these warnings are often printed or outlined in red and set off from the rest of the text.

Some companies have even
A lighted warning label that tells the user to be careful of high voltages is a new safety feature that is starting to appear on instruments such as this precision power amplifier from Fluke.

gone to the extreme of putting lighted warning labels on their equipment. For example, an automated test system developed by John Fluke, Mountlake Terrace, WA, is capable of performing preprogrammed tests on many pieces of equipment. A good number of these tests have potentially lethal voltages crossing between the automatic tester and the tested device. The interface between them is a transition panel with a lightning-bolt label that lights up when the programmed test involves dangerous voltages.

Illuminated warning labels are especially useful when an instrument is meant to be used by someone unfamiliar with high voltage and its effects. But what about those who are supposedly familiar with high voltage—the engineers and technicians who deal with it every working day? Has anyone not been zapped by a "familiar" piece of equipment at one time or another?

Familiar with the moral of the story of the man and his lawnmower, most instrument manufacturers provide safety interlocks on their equipment that are designed to protect the user. Many even go to the extent of incorporating double interlocking switches in situations where lethal high voltage exists.

**Double interlocks maintain integrity**

Double interlocks are used to guard against the failure of any single interlock switch to maintain the integrity of the protective interlock system.

Clear plexiglas shields are commonly employed with the interlocks over internal portions of the instrument where high voltages may be present. Besides permitting the area to be inspected and the curiosity of the purchasing engineer to be satisfied, the shield prevents access to the high-voltage area.

The exacting requirements of the medical electronics industry have led to the production of clear plastic, ac-line-cord plugs. The visibility of all connections from the insulated line cord to the
metal prongs of the plug helps ensure that the cord wires are connected to the proper prongs.

The instrument manufacturer's concern for safety has expanded to include his own safety devices. Fuses, which are included in equipment design for safety, are now being analyzed themselves by cautious instrument manufacturers. Fuse holders are being incorporated into equipment as an integrated fuse-hold-and-line-cord-receptacle combination that sometimes includes a cover-interlock switch for the instrument. This combined fuse holder and line-cord receptacle is outfitted with its own fuse cover, which prevents contact with the fuses while the equipment is plugged in. The cover slides over the receptacle in which the fuse is located. This ensures that the power is physically disconnected from the instrument.

Since the fuse cover is generally clear plastic, the fuses may be observed while the equipment is in operation to check for any burn-outs.

Similarly, when an old-style, black-bakelite, panel-mounted fuse holder is used in an instrument, the power (hot) line of the fused circuit is generally connected to the rear (tail) of the fuse rather than the front (head). So the fuse clamp ed into the holder by its head can be removed by unscrewing the front of the fuse holder and avoiding any directly exposed line voltage. The hot line is deep inside a hole in the fuseholder and can only be reached by touching the bottom of this hole with a probe whose diameter is limited to a quarter of an inch.

Proper grounding a must

Properly grounding all exposed metal parts on the outside of an instrument is essential to the safety of operating personnel. Standard practice requires that a solid connection be established between all exposed metal parts and the ground wire in a three-wire ac line cord. In fact, one proposed international specification requires that all exposed metal parts on an instrument measure not more than one ohm to the ground pin on the ac line plug.

Instrument power-line switches are also being scrutinized by safety engineers. Double-pole-single-throw switches that break both the hot and neutral sides of the power line are replacing the old single-pole-single-throw ac line switches to assure complete isolation from the power line when the equipment is switched off. Only the ground connection is left intact. The neutral side of the power line is not at ground potential in many cases, and allowing “power-off” adjustment of switched-off equipment with a portion of the instrument’s circuitry at other than ground is a risk many instrument manufacturers are choosing not to take.

Volt-ohmmeter goes boom

Volt-ohmmeters are particularly suited to misuse and potential failure. Since they generally have multiple ranges and sensitivities, they can be easily connected to large voltages even while set improperly. This usually happens while attempting to measure voltages with the meter set to measure either resistance or current.

Traditionally, ohmmeter manufacturers have protected their products by building them to withstand up to 30 V on the input when inadvertently connected to a live circuit, then have relied on a fuse to save the meter above 30 V. Now ohmmeters are equipped with semiconductor protection circuits that enable them to withstand a guaranteed 250-V application, on the theory that the meters should not be harmed when connected to the ac power line accidentally.

However, as illustrated by the case of a man measuring voltages with a volt-ohmmeter held between his knees, meter manufacturers have more to worry about than protecting their own products. The man had the range switch set for current, and as he probed a power line, the volt-ohmmeter exploded. Fortunately, the man was not injured, and the volt-ohmmeter manufacturer learned the same lesson as the lawnmower manufacturer, but at a much cheaper cost.

But attempts to solve safety problems must be considered for their own safety value. The ac-
With a line of minis and micros like ours, we don’t have to push any one of them.

With other companies, you might set out to buy a microprocessor chip and end up with the whole chassis. Or get a box when all you need is a board.

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dent just described caused one volt-ohmmeter manufacturer to install a 250-V rated protective fuse in one probe of his meter. But this in turn caused other problems. In one instance, a maintenance man was probing a 480-V busbar with his volt-ohmmeter accidentally set on current instead of voltage. The fused probe blew up in the man’s hand, although the meter was apparently saved from damage.

Placing a guard chassis within the main cabinet of the instrument is a technique well suited to making measurements float with respect to ground. Typical proposed breakdown specifications for this application are 1000 V rms plus twice the maximum voltage expected between the guard chassis and ground. Since standard operating procedure in the United States is to use input-power transformers with 1.5-kV dielectric breakdown voltages, the guard’s chassis-to-ground potential is limited for the immediate future to a ratable 250 V.

Floating exposes trouble

Currently, there are few instruments in the 3-to-5-kV, common-mode-input rating range, but many more will be available within the next two years, as safety standards become more common. But now the standard laboratory technique for floating measuring instruments from ground, disconnecting the ground pin of the equipment’s ac power-line cord, is coming under fire from the safety engineers. When this floating takes place, every exposed metal part of an oscilloscope, for example, rises to the common-mode voltage of the measured signal and presents a great opportunity for electrical shock. Because of this shock hazard, safety engineers are talking of redesigning the BNC connector to eliminate its exposed metal.

The alternative is to redesign the inputs to the oscilloscope and make all measurements differentially. This alternative, however, would raise the price of the oscilloscope from a few hundred to a few thousand dollars and reduce the bandwidth from a few hundred megahertz to a few megahertz.

To permit floating at virtually any potential, many companies are going to battery operation. But one specification is extremely important for the safe use of battery-powered instruments: leakage. If a battery-operated voltmeter, for example, is being used to measure voltage between the legs of a three-phase powerline, every part of the meter is above ground potential. If there is any leakage current flowing through the instrument’s case, it may end up flowing through the person making the measurement.

Safety specifications for this type of test equipment are not easily generated. For example, capacitors must be tested to see if they withstand a certain voltage. And, if they are of the oil-filled variety, the dielectric may become polarized during the testing process. When discharged, these capacitors will present a safety hazard in themselves after—as well as during—the measurements. The reason: the oil-filled recharge without connection to external circuitry.

Binding posts are hazardous too

Even the lowly binding post is due for a redesign, because its exposed metal parts allow all too easy contact between an instrument user and hazardous voltages. Hazardous voltages are currently defined by safety engineers as 30-V rms for sinusoidal signals and 60 V for dc, with variations for nonsinusoidal waveforms.

Today’s thinking is that ordinary five-way binding posts are unsafe for use with these voltages, and that something without exposed metal must be designed to take their place. But so far no one has designed anything that can connect to wires and banana plugs as efficiently as the standard five-way binding post.

Providing banana jacks recessed from the mounting panel so that only the mating banana plug can make contact with the jack has been reasonably successful. This method solves the problem at one end of the cable, but the other end of the cable needs to make contact, too. Thus either the other end of the cable has banana plugs with unsafe voltage on them, or some other connector is devised.

Binding posts are a safety problem whether they are located on sources of power or on the inputs to measuring instruments that never act as a source. Once the connection is made between the source and measuring circuit, all of the binding posts in the completed path are live.

Sinking sources save

Two notable ways to prevent instruments from damaging one another by misconnection are making sources capable of sinking current as well as sourcing it, and alternatively, disconnecting themselves from devices under test if required to sink current.

An ac calibrator from John Fluke has a transient detector that shuts down the calibrator and equipment under test before a destructive arc can occur. The calibrator does this by detecting the corona discharge that precedes an arc discharge.
Protection that adds value . . .

You came to the right place.

Because a Heinemann circuit breaker just might solve that design or procurement problem you’re wrestling with right now. You’d be surprised at how many things we can do so well in the general area of circuit protection, on/off switching, remote actuation, and even limit control.

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HEINEMANN CIRCLE NUMBER 59
Borrow my coffee cup... but never my C-Meter.

The C-Meter opens up a new route to efficient designing. It's so handy that you'll find yourself measuring capacitors as a matter of course. Why? Because its pushbutton speed, high accuracy (.1%), small size and versatility (.1pf to .2 farads), make capacitors easier to measure than resistors.

With the C-Meter, you'll waste no time twiddling, and nulling, and you'll cut the need for expensive tight-tolerance capacitors or tweak pots in your circuits. You'll be a much more efficient engineer. And popular too, because people just can't keep their hands off the C-Meter.

You owe it to yourself to try one. Our reps are stocking them at $289.
Industry asked us for hundreds of variations of these switches. Evidently we're pushing the right buttons.

And we intend to keep pushing them.

So that every time one of your new ideas creates a design problem, MICRO SWITCH will be ready with the miniature manual switch that solves it.

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The Series 8 lineup of miniature manuals includes toggles, pushbuttons, paddles and lighted or unlighted rockers. They're UL listed at 6 amps, 125 VAC. And every one is available in a low energy version as well.

Choose terminal variations ranging from solder to quick-connect to PC board or wire wrap. There's also a choice of panel and bushing-sealed pushbuttons and toggles. And non-threaded bushings on PC mounted toggles. Even colored sleeves and integral colored tips for the toggles.

And of course, you'll find one feature you won't find anywhere else—the quality you've come to expect from MICRO SWITCH. Series 8 switches are inspected to a 1% Acceptable Quality Level (AQL).

That's quality you can put your finger on.

For your immediate product needs, see your nearest MICRO SWITCH Authorized Distributor. If you have other requirements, contact a MICRO SWITCH Branch Office or call 815/235-6600.

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Tell us about that special enclosure you need -- basic specifications or a brief description, even a rough sketch will do -- and we'll make something out of it. Something special.

It's your brainstorm.
You did it: designed a new instrument or system. Now you need a special enclosure to house it. One designed, built and priced right. Get it -- get it all. From Bud.

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A local "metal bender" could bang out your enclosures. Trouble is, his business isn't enclosures. Why risk amateurism? You have too much riding on that new instrument or system. Get what you want -- professionalism. From Bud.

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CIRCLE NUMBER 63
Get on the IEC bus. Soon to be an international standard for interfacing instruments, the bus brings many benefits—and a few problems too.

Think international when you interconnect test equipment. An interface for measuring instruments will soon be a world standard of the International Electrotechnical Commission (IEC). The Standard has been adopted by the IEEE (Std. 488-1975), with a change in the connector proposed by the IEC.

Many benefits accrue from the standard. With it, you can connect up to 15 different instruments, spaced up to a total of 65 cable feet (20 meters). The instruments can come from practically any vendor—only minor software adjustments are sometimes necessary (Fig. 1).

The proposed IEC standard uses a byte-serial, bit-parallel format, with bidirectional lines for both data flow and addressing. Alterations to accommodate special needs can be made with simple and inexpensive reprogramming. And since the system is modular in concept, you can start small and work up as necessary.

Other advantages of an international standard include the following:

- No engineering costs are tied up in developing special interfaces.
- Instrument manufacturers can concentrate on producing instruments, not interface systems.
- Specialized modules can be easily produced; for example, power-supply makers can concentrate on power supplies and not worry about designing a system for the supplies to fit into.
- Instruments can be optimized internally to satisfy the international standard.

Details of the IEC standard

Maximum speed of the standard is 1 Mbyte/s with three-state drivers and 250 kbyte/s with open-collector drivers, speeds high enough for most applications. Transfer of one 8-digit word (8 characters) takes about 32 µs.

The specified cable has both male and female connectors, so that plugs can be stacked piggyback fashion, thus saving space on instrument back panels (Fig. 2). This makes expansion of the system very simple.

In general, any communications link requires three active devices: a listener, a talker and a controller. The controller decides the role each device plays at any time; any device not addressed remains inactive. Of course a device can perform more than one role at different times.

The proposed IEC bus system carries all mes-

Manfred Richter, Interface Engineer, Philips Electronic Industries GmbH, Hamburg, Germany.
Why an international interface standard?

The basis of the IEC standard is a set of objectives that define the bus but leave designers free to select the necessary interface capability. The objectives are:

- To provide cost-effective capability for simple bench systems.
- To be compatible with simple controllers. However, a system limited to just two devices must be able to use the link without controllers.
- To serve the needs of a wide variety of products—such as controllers, processors and instrumentation.

- To be compatible with the ISO, a 7-bit code for address and command data that’s easy to generate, display and read.
- To provide for flexible data rates and communication paths with a minimum of timing restrictions.
- To provide capability to accommodate multiple listeners and direct communication paths—without buffering in the controllers.
- To permit a mode for transfer of basic data with unrestricted codes.
- To minimize the number of wires.

2. Space is saved and system expansion is easy with connectors that allow piggy-back stacking.

3. What the various bus wires do: 16 lines take care of data flow, data transfer and general housekeeping chores.
listeners—the DAV line is set to high (data not valid), the NRFD set to low (no listener ready for data) and NDAC to low (no listener has accepted data).

2. The talker checks the line conditions, then puts a data byte on the lines.

3. Listeners are ready to accept data, so the NRFD line goes high—this cannot happen before all listeners are ready.

4. When a talker senses that NRFD is high, it sets DAV low to indicate that the data are valid.

5. The first listener sets NRFD to low to indicate that it is no longer ready and starts to accept data. The other listeners follow at their own pace.

6. First listener to finish sets NDAC to high to indicate it has accepted the data.

7. When the final listener has indicated that it has accepted the data, NDAC goes high.

8. The talker senses NDAC high and sets DAV high to indicate that the data are no longer valid.

9. Talker removes the data from the line.

10. The listeners, sensing DAV is high, set NDAC low in preparation for the next cycle.

11. All three lines are now in the initial states.

A typical example of how the IEC data bus can be used is demonstrated by a system for the analysis of the stresses in prototype railway cars and passenger carriages. (Fig. 5).

A practical example of the bus

Upwards of 300 strain gauges are connected to the vehicle under test. Bridges and voltmeters process and read the transducer outputs.

A manually controlled test system requires setting each bridge value, selecting the relevant transducer, measuring the output, then performing a further calculation to establish the load at each point. One way to avoid the tedium of these time-consuming chores: Design a computer-controlled, automatic system to collect and process the data and produce a printout.

Even trying to connect the series of necessary instruments in a star system—scanner, scanner control, bridge, digital voltmeter, computer, teletypewriter—involves serious wiring problems. Since a computer is necessary anyway, it's no problem to use it to control a data bus.

Operation is simple. The computer, as a controller, addresses the scanner—the listener—and requests data from a selected-strain transducer. The bridge—also a listener—is addressed to set up the relevant bridge components to take the information from the scanner. So the bridge can present the analog signal to the DVM.

The voltmeter is instructed to act first as a listener, second as a talker to pass the information to the computer. The computer processes the information and commands the printer to listen

4. Timing of the three-line handshake process, in which data bytes are transferred across the interface. Only one data line is shown.

5. A practical use of the bus involves stress analysis of railroad cars. Strain gauges collect the raw data, a bridge forms the analog outputs, and a DVM reads and converts the signals. A computer controls the entire system automatically.
and do its job. Of course, if the information is wanted only for external processing, the printer can control the system and produce a series of output-voltage readings for later use.

The operation of the strain-gauge test system conforms to the following sequence:

1. The computer—as a controller—uses the IFC (Interface Clear Line) to start the system.
2. The controller sends a DCL (Device Clear) message to set all devices to an initial state.
3. The controller sends the listen address of the scanner control, followed by data, to select a particular strain gauge.
4. The controller sends an “unlisten” command, then the listen address of the bridge, followed by data for matching a selected strain gauge.
5. The controller again sends an “unlisten” command, then the listen address of the DVM, then data to read the output of the bridge on the analog line.
6. The controller sends an unlisten command, sets itself to listen, then sends the talk address of the DVM.
7. When the DVM has the measurement information, it sends the data to the computer.
8. When the computer has processed the information, it again clears the interface and sends the listen address of the printer, followed by the required output information.
9. When the printer has typed all information, the controller can restart the sequence.

Sometimes, output information is needed in several forms—say, in a tape memory as well as a printout. If so, bear in mind that a tape drive is obviously much faster than a printer and can supply a data-accepted signal as soon as it is finished. But a controller will not react until all devices receiving information have sent data-accepted signals, that is, the controller must wait until the NDAC line goes high.

Unresolved problems

For distances longer than 20 m, the problem becomes more complicated. The present IEC system can be applied up to 330 ft (100 m) with some upgrading of hardware. For much longer distances, from 2000 up to 3000 m (2 to 3 km), it is necessary to go to full serialized busses with only one or two wires.

Much more work is necessary before all the interconnection problems are solved. But the IEC bus is the most practical step yet taken. Its success depends on people making an effort to understand and use the bus.

Further work is also underway in the field of “software,” for example, data formats. The problem here is to decide where to stop. If the description is taken too far, individual designers can be unnecessarily restricted. ●●

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CIRCLE NUMBER 64

127
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Electronic Design 24, November 22, 1976
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CIRCLE NUMBER 66
Measuring capacitor loss: Are S-parameters any good? They’re not, but other methods—like the use of Q-bridges or resonant coaxial lines—are acceptable.

In determining the losses of microwave capacitors, the Q values calculated from measured S parameters are worthless. Perhaps this is the reason that articles endorsing S parameters for capacitors emphasize the importance of low series resistance, but seldom give measured values of \( r \) or \( Q \). In the few instances when such data can be found, no hint is given of the origin of the values.

Valid techniques do exist, however, those using Q-bridges or resonant transmission lines, for example.

The two S parameters usually published to describe microwave capacitors are \( S_{11} \)—the input reflection coefficient of a series capacitor and a termination, \( Z_n \), and \( S_{21} \)—the forward insertion loss of the same combination. The Q of the capacitor relates to these parameters through the expression:

\[
Q = \frac{2|S_{11}| |S_{21}|}{1 - |S_{11}|^2 - |S_{21}|^2}.
\]

A recent treatment of the subject states that the Q of a capacitor can be found from \( S_{11} \) alone, giving:

\[
Q_r = \frac{\sin \theta}{\cos \theta - |S_{11}|},
\]

where \( \theta \) is the phase angle of \( S_{11} \).

Although Q is acknowledged as a key parameter, no values are given. Instead, the “insertion loss” is tabulated for several capacitors over a wide range of frequencies. The loss is correctly defined as the sum of the reflective and dissipative losses, but the insertion loss is based on the expression for the reflection loss only.

For capacitors of high, or even modest Q values, it is true that the dissipated power is extremely small compared to the reflected power, but the correct relationship includes both and is given by:

\[
\text{Insertion loss} = 10 \log_{10} \left( \frac{1 - |S_{11}|^2}{1 - |S_{21}|^2} \right),
\]

or Insertion loss \( = 10 \log_{10} |S_{21}|^2 \).

You may well wonder why insertion loss for capacitors is emphasized. For small values of capacitance, at frequencies in the order of a few hundred megahertz, the insertion loss is naturally high. The loss drops as either the capacitance or frequency increases, and it is almost entirely a function of the reactance.

Is insertion loss of any value?

To attribute a low Q factor to a high insertion loss would be folly. The only redeeming value of insertion loss, other than characterizing reactance as a function of frequency, is to discover resonances in the capacitor or the test fixture.

The equations already given by \( Q_r \) are correct. Then where does the problem lie? The limitation is in the measuring system. Most equipment cannot resolve the small values of resistance and the resulting small differences of phase. Remember, the capacitor loss must be detected in the

---

R. E. Lafferty, Vice President and Engineering Manager, Boonton Electronics Corp., Route 287 at Smith Road, Parsippany, NJ 07054.
presence of a total resistance equal to twice the characteristic impedance of the system (100 Ω).

What little effect the series resistance has on both $S_{11}$ and $S_{21}$ is lost in the uncertainty of S-parameter measurements.

Example: A 22-pF capacitor with a Q of 200 at 300 MHz has calculated values of 0.234160 for $S_{11}$ and 0.971028 for $S_{21}$. If the series loss could be reduced to zero, calculated values would be 0.234424 and 0.972134, respectively, a change of only 0.11%, or approximately 0.01 dB. In a measuring system with two-digit resolution, there would be no detectable differences in the S values.

The failure of S parameters to provide significant values of Q is clearly illustrated in a table of calculated Q values for several capacitors. Measured values of $S_{11}$ and $S_{21}$ have been taken from published data, and the results of both equations (1) and (2) are listed. The absurd values of Q obtained with either equation are a convincing argument against using S parameters to measure capacitor loss.

**Is there a better way?**

How can the high-frequency loss of a capacitor be measured? A Q-bridge is a good means of directly measuring Qs up to 10,000 for capacitors from 20 to 1000 pF at frequencies of 0.1 to 50 MHz.

For frequencies above 50 MHz, the only suitable method known to the author requires a resonant coaxial transmission line. A quarter-wave coaxial line is coupled loosely to a stable signal generator. The outer-to-center conductor spacing of the line should be compatible with the terminal spacing of the capacitor to be measured, provided the Q of the line can be held to a high value. The generator should have a digital display of the output frequency; if it doesn’t, a counter must be used.

An rf millivoltmeter, lightly coupled to the open end of the line, detects the voltage at the resonant frequency, $f_r$, and on each side of resonance (Fig. 1).

The Q of the line at $f_r$ may be calculated from:

$$Q_o = \left(\frac{f_r}{\Delta f}\right) \sqrt{\frac{D_1 D_2/3}{1 - (\pi/4Q_o)^2 f_1 f_2 D_3}},$$

(4)

where $Q_o$ denotes the measured Q of the unloaded quarter-wave line, $m$ equals the ratio of resonant to off-resonant voltage, and $\Delta f$ equals the total bandwidth between the off-resonant voltage points. If the half-voltage points are used, Eq. 4 reduces to:

$$Q_o = \sqrt{\frac{3}{\pi}} \left(\frac{f_o}{\Delta f}\right)$$

(5)

**Measuring $Q_c$.**

Connect the capacitor to be tested across the open end of the line. Resonance will now occur at a lower frequency, $f_1$, where the reactance of the line equals the reactance of the capacitor. The generator frequency is again adjusted above and below resonance where the coupled voltage falls to half of its resonant value. Q can now be calculated using the following equation:

$$Q_c = \frac{\cos \beta f_1}{\sqrt{D_1 D_2/3 - (\pi/4Q_o)^2 f_1 f_2 D_3}},$$

(6)

where $D_1 = \cos \beta f_1 - \frac{\sin \beta f_1}{\tan \beta f_1} \left[\frac{f_1}{f_2}\right]$, $D_2 = \sin \beta f_1 - \frac{\cos \beta f_1}{\tan \beta f_1}$, and $D_3 = \sin \beta f_1 + \frac{\cos \beta f_1}{\tan \beta f_1}$, and $\beta_1$, $\beta_2$, and $\beta_3$ are the electrical lengths of the line at frequencies $f_1$, $f_2$, and $f_3$, respectively.

$$\beta_1 = \left(f_1/f_2\right) 90^\circ$$

(7)

$$\beta_2 = \left(f_2/f_3\right) 90^\circ$$

(8)

$$\beta_3 = \left(f_3/f_1\right) 90^\circ$$

(9)

Example: With a 6-ft copper line having an I.D. of 4 in. and an O.D. of 1.125 in., the natural resonant frequency is 41 MHz, and $Q_o = 2190$. When a 22-pF capacitor is connected across the open end, the resonant frequency drops to approximately 31.76 MHz. The measured frequencies at which the voltage falls to half of the resonant voltage are:

$f_2 = 31.7766$ MHz and $f_3 = 31.7448$ MHz.

Therefore $f_1 = (f_2 + f_3)/2$, which equals 31.7607 MHz.

With the aid of a calculator the following terms can be found:

$$\beta_1 = (31.7607/41) 90^\circ = 69.718610^\circ$$

$$\beta_2 = (31.7766/41) 90^\circ = 69.753512^\circ$$

$$\beta_3 = (31.7448/41) 90^\circ = 69.718610^\circ$$
Through a connector to couple the probe tip to the lines, a threaded bushing can be soldered to the center conductor of the line.

Outer wall, with some form of insulated feedthrough connector to couple the probe tip to the center conductor of the line.

Both the full-scale and half-scale of the line; and both the full-scale and half-scale meter: a high-impedance probe is important; it should be coupled loosely to the open, or test end of the line. A terminating resistor in series with the line should be sufficient to excite the line and give a good reading on a loosely coupled rf millivoltmeter without introducing noticeable loss in the line. A terminating resistor in series with the loop will reduce the SWR on the connecting cable.

Whether or not the induced voltage is a function of frequency is of little consequence because of the rigorous interrelationship of the measuring frequency, the capacitance and the length of the line, an unfortunate constraint is imposed with this method. For a given line, you may select capacitance or frequency, but not both. The parameters are related as follows:

\[
C = \frac{1}{\omega L_0 \tan (1.91 \times 10^{-10} \omega L t_{mn})}
\]

It is convenient to draw a graph of capacitance vs frequency for each line.

Sources of error

For the signal source, the major requirement is frequency stability. Accurate measurements can't be made with a generator that drifts. Residual AM or FM will not affect the measurement.

A small loop inserted at the shorted end of the line should be sufficient to excite the line and give a good reading on a loosely coupled rf millivoltmeter without introducing noticeable loss in the line. A terminating resistor in series with the loop will reduce the SWR on the connecting cable. Whether or not the induced voltage is a function of frequency is of little consequence because of the small deviation needed for the measurement.

There are a few requisites for the rf millivoltmeter: a high-impedance probe is important; it should be coupled loosely to the open, or test end of the line; and both the full-scale and half-scale readings on the ranges to be used (probably 1, 3, and 10 mV) should be calibrated.

For large-diameter lines, you can thread the probe directly through the outer wall. For smaller lines, a threaded bushing can be soldered to the outer wall, with some form of insulated feedthrough connector to couple the probe tip to the center conductor of the line.

Probe loading with loose coupling does not influence the measured Q. This is proven by coupling the millivoltmeter at both the open end and as far down as a sixteenth of a wavelength. There is no measurable difference in the results. Calculations made with the measured capacitance between the probe and the line, and with the input resistance of the probe, also confirm a negligible contribution by the probe to line loading.

Errors of a few percent in the millivoltmeter calibration will cause similar errors in the measured Q and, with calibration, errors should remain less than 2%.

Eq. 6 assumes that the entire line loss is from series resistance and that this resistance, and hence the attenuation constant, is proportional to \(\sqrt{f}\). To satisfy this requirement, the line material must be uniform throughout and should not be plated. If insulated screws are needed to support the center conductor, the number should obviously be minimized.

Repeatability and accuracy

Measurements of the unloaded Q of several coaxial lines, taken over a period of 18 months, repeat within 2%. Loaded Q measurements are less repeatable but with regular cleaning of the terminals, measurements usually agree within 10%. At frequencies below 50 MHz, the correlation between coaxial line and Q-bridge measurements (not to be confused with a Q-meter) are usually within 15% for Q values under 2000.

For Q values less than 2500, and assuming the Q of the line is greater than that of the test capacitor, the accuracy of this method may be within 15 to 30%. All factors considered, it is not now prudent to place a better figure of uncertainty on the outlined measuring technique. Regardless of the absolute accuracy, the measurement provides reasonable Q data—S-parameter measurements do not.

A plot of Q vs frequency for a few ceramic capacitors approximates the expected slope of \(1/f\) at high frequencies for capacitors of low dielectric loss and with effective plate thickness less than the skin depth (constant \(r_0\)). Such a plot is given in Fig. 2.

Users of Q-meters who have experienced difficulty in measuring the loss of capacitors may be concerned that the transmission line measurement suffers from the same deficiencies. Two important differences between the two techniques yield a significant improvement in accuracy for the transmission line.

First, when you connect a capacitor to a line, the attendant lowering of the resonant frequency is accompanied by a predictable change in line loss (within a few percent). But when you connect a capacitor to the Q-meter, the internal variable capacitor is reduced to restore resonance.
Tabulated Q values calculated from published data for $S_{11}$ and $S_{21}$

<table>
<thead>
<tr>
<th>C (pF)</th>
<th>f (MHz)</th>
<th>$S_{11}$ (Re)</th>
<th>$S_{11}$ (Im)</th>
<th>$S_{21}$ (Re)</th>
<th>$S_{21}$ (Im)</th>
<th>$Q_c$ (from $S_{11}$)</th>
<th>$Q_c$ (from $S_{21}$)</th>
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<td>10</td>
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<td>0.99</td>
<td>-0.03</td>
<td>7.9</td>
<td>-0.16</td>
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</table>

The change in the capacitance affects the loss of the internal capacitor, but the extent of the change is difficult to determine, and the repeatability is suspect. As a result, it is usually ignored, and the measured Q is generally higher than the correct value—and it may even be negative!

Second, the intrinsic Q values of transmission lines are substantially higher than those of the work coils used with a Q-meter. Consequently, capacitors of moderately high Q have a pronounced influence on the effective loss of a coaxial line. The same capacitor on a Q-meter may barely change the reading. ■

References
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Measure the characteristic impedance
of almost any line with this two-load technique,
and avoid many of the limitations of traditional methods.

Here's a two-load method for determining the characteristic impedance, $Z_0$, of almost any audio or rf transmission line of any length without having to assume a no-loss condition. The new method avoids most of the disadvantages of traditional approaches.

Traditional methods of determining $Z_0$ of uniform transmission lines (Fig. 1) include:
- Calculating from the geometry or distributed constants of the line.
- Measuring open and short-circuited line impedances.
- Measuring a shorted eighth-wavelength line section.

Traditional methods have practical disadvantages

All three approaches have practical disadvantages that limit accuracy, convenience or both.\cite{1,2,3}

In the first method, the constants must be found over the frequency range of interest—not an easy task, since distributed resistance, capacitance and inductance are all frequency sensitive to some degree. Also, calculating the impedance from line-material properties and cable geometry is tedious, unless simplifying assumptions are made.

The open and short-circuit method is the most widely used, but is accurate only for short lengths of low-loss sections. Furthermore, it’s unusable for lengths near quarter-wave multiples, because the extreme impedance values obtained lead to poor accuracy. And when lengths are very near the critical quarter-wave multiples, the high impedance values are usually outside the measurement range of most commercial bridges.

Finally, only the magnitude of $Z_0$ is measured directly with the shorted eighth-wavelength method. And not only is the eighth-wavelength method limited to very low-loss lines, but also the length must be determined precisely.

Except for the calculation method, these traditional methods assume low-loss lines. However, a

---

**Traditional ways of determining $Z_0$**

Calculations from line geometry

<table>
<thead>
<tr>
<th>LINE GEOMETRY</th>
<th>CHARACTERISTIC IMPEDANCE</th>
</tr>
</thead>
<tbody>
<tr>
<td>OPEN TWO-WIRE LINE IN AIR</td>
<td>$Z_0 = 120 \cosh\frac{d}{\lambda}$</td>
</tr>
<tr>
<td>$\approx 276 \log_{10} \frac{2D}{d}$</td>
<td></td>
</tr>
<tr>
<td>SINGLE COAXIAL LINE</td>
<td>$Z_0 = \frac{138}{\sqrt{\epsilon}} \log_{10} \frac{D}{d}$</td>
</tr>
<tr>
<td>$\epsilon = \text{dielectric constant}$</td>
<td></td>
</tr>
<tr>
<td>$= 1 \text{ in air}$</td>
<td></td>
</tr>
<tr>
<td>BALANCED SHIELDED LINE</td>
<td>$Z_0 = \frac{276}{\sqrt{\epsilon}} \log_{10} \left[ \frac{2u - i\sigma^2}{i + \sigma^2} \right]$</td>
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<tr>
<td>$u = \frac{h}{d}$</td>
<td></td>
</tr>
<tr>
<td>$\sigma = \frac{\pi}{\epsilon}$</td>
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<tr>
<td>ECCENTRIC LINE</td>
<td>$Z_0 = \frac{138}{\sqrt{\epsilon}} \log_{10} \left[ 1 - \left( \frac{2\epsilon}{\lambda} \right)^2 \right]$</td>
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<tr>
<td>$\sigma$</td>
<td></td>
</tr>
<tr>
<td>$= \text{dielectric constant}$</td>
<td></td>
</tr>
<tr>
<td>$= 1 \text{ in air}$</td>
<td></td>
</tr>
<tr>
<td>OPEN AND SHORT-CIRCUIT METHOD</td>
<td>$Z_0 = \sqrt{Z_{SC}Z_{OC}}$</td>
</tr>
<tr>
<td>MAKE TWO MEASUREMENTS — $Z_1$ when $Z_r = 0$</td>
<td></td>
</tr>
<tr>
<td>AND $Z_1 = Z_{SC}$ when $Z_r = \infty$</td>
<td></td>
</tr>
<tr>
<td>$Z_0 = \sqrt{Z_{SC}Z_{OC}}$</td>
<td></td>
</tr>
<tr>
<td>$Z_{OC}$ (open circuit) = $Z_0 \coth \gamma \lambda$</td>
<td></td>
</tr>
<tr>
<td>$Z_{SC}$ (short circuit) = $Z_0 \tanh \gamma \lambda$</td>
<td></td>
</tr>
</tbody>
</table>

| SHORTED 1/8-WAVELENGTH LINE | |
| $|Z_1| = |Z_0|$ |
| $\lambda = \lambda/8$ |

1. Traditional methods of determining a line’s characteristic impedance usually require assumptions not always true in practice, especially for long lossy lines operating at audio frequencies.

James E. McKay, Project Engineer, WSB Radio, 1601 W. Peachtree St. NE, Atlanta, GA 30309.
Using two known load impedances, \( R_1 \) and \( R_2 \), to produce easily measured line input impedances, overcomes most of the shortcomings of the traditional methods for determining the \( Z_0 \) of a line.

Low-loss condition can't be assumed for low frequencies as in many telephone voice and data lines.

Several special techniques are also used, including the use of slotted lines to compare \( Z_0 \) with a standard, time-domain reflectometry and the complicated Chipman method of resonance-curve plotting. These methods are generally limited to microwave frequencies and require that line losses be negligible.

New method needs two measurements

Using two different known load impedances avoids many of the previously mentioned limitations. The new method applies to both audio and rf lines of any length, and no assumption of negligible loss is required. The method uses the general-transmission line equation,

\[
Z = Z_0 + R \tanh \gamma \ell = Z_0 + R \tanh \gamma \ell ,
\]

where

- \( Z_0 = \) characteristic impedance
- \( R = \) load impedance
- \( \gamma = \) propagation constant
- \( \ell = \) line length
- \( Z = \) impedance at a distance \( \ell \) from the load

Solving Eq. 1 for \( \tanh \gamma \ell \) yields

\[
\tanh \gamma \ell = \frac{Z_0 (Z - R)}{Z_0^2 - RZ} .
\]

Two measurements are made at the frequency of interest. The first is a measurement of the line impedance, \( Z_1 \), with a known terminating impedance, \( R_1 \). The second measures an impedance, \( Z_2 \), with another known load impedance, \( R_2 \). Impedances or, preferably, resistances \( R_1 \) and \( R_2 \) are chosen to yield readily measurable values of \( Z_1 \) and \( Z_2 \); otherwise, they are arbitrary.

Note that \( \gamma \) depends entirely on the line constants, \( \ell \) is a fixed length, hence \( \tanh \gamma \ell \) is the same for both measurements. Writing Eq. 2 for each measurement and equating them results in

\[
\tanh \gamma \ell \left[ \frac{Z_0 (Z_1 - R_1)}{Z_0^2 - R_1 Z_1} \right] = \frac{Z_0 (Z_2 - R_2)}{Z_0^2 - R_2 Z_2} .
\]

Solving for \( Z_0 \) yields

\[
Z_0 = \left[ \frac{(Z_1 - R_1) R_1 Z_2 - (Z_2 - R_2) R_1 Z_1}{Z_1 - Z_2 - R_1 + R_2} \right]^{1/2} .
\]

The \( R_1 \) and \( R_2 \) quantities on the right side of Eq. 4 are selected for easy measurement. Note that \( Z_0 \) is independent of line length or losses. The error sources in Eq. 4 involve the normal measurement tolerances, not theory or assumptions.

If terminating impedances \( R_1 \) and \( R_2 \) are chosen to be pure resistances, the measured impedances \( Z_1 \) and \( Z_2 \) are, respectively, complex; therefore, Eq. 4 can yield complex values for \( Z_0 \). This result is expected for some lossy lines, and all practical lines at low frequencies.

In the special cases of half-wave, low-loss lines or extremely short sections, be particularly careful when selecting the load impedances, \( R_1 \) and \( R_2 \). They should be selected to best resolve the differences, \( (Z_1 - R_1) \) and \( (Z_2 - R_2) \), between the measured and load impedances.

References

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For random-pulse rates, the statistical accuracy—and for regular pulse rates, the absolute accuracy—depends on how long you are willing to wait for the result. The circuit works in the same way for random and regular signals.

Gated counters determine the ratio

In the simplified arrangement of Fig. 1, the input-pulse rates, \( f_1 \) and \( f_2 \), enter the two NOR gates, IC₁₁ and IC₁₂, respectively. A J-K flip-flop latch circuit, IC₂₁, controls the state of these gates.

Pulses passed by IC₁₁ accumulate in a four-decade register, \( N_1 \), formed by counter circuits IC₃ through IC₆; pulses passed by IC₁₂ accumulate in another four-decade register, \( N_2 \), formed by counter circuits IC₇ through IC₁₀. Register \( N_2 \) has a \( 1 \times 10^4 \) overflow circuit consisting of flip-flop IC₂₂, transistor Q₁, and a LED. A four-decade, numerical readout displays the contents of \( N_2 \).

The counting time, \( t_1 \), of the two registers is the amount of time register \( N_1 \) needs to accumulate a count selected with switch \( S₁₁ \). When \( N_1 \) accumulates the selected count, latch IC₂₁ operates and closes gates IC₁₁ and IC₁₂. The circuit then holds and displays the contents of \( N_2 \) until the circuit is manually reset with \( S₂ \).

Clearly the ratio of the pulse rates \( f_1 \) and \( f_2 \) are related to the counts, \( n_1\) and \( n_2\), accumulated in the corresponding registers, \( N_1 \) and \( N_2 \), by the following equation:

\[
\frac{f_2}{f_1} = \frac{n_2}{n_1}
\]

The \( n_1 \) counts are the powers of ten—\( 10^1 \) or \( 10^2 \)—for easy interpretation of the displayed ratio. A switch section, \( S₁₂ \), automatically illuminates the proper decimal point corresponding to the \( n_1 \) count selected. As explained later, additional \( N_1 \) stages can be added for increased accuracy.

For example, if

\[
f_1 = 580 \text{ Hz}, \quad f_2 = 45 \text{ Hz}, \quad \text{and} \quad n_1 = 10^4,
\]

then

\[
\frac{f_2}{f_1} = \frac{n_2}{n_1} = \frac{77}{10^4} = 0.077
\]

with the second from left decimal point illuminated on the four-decade display.

However, since the true ratio of \( f_2/f_1 \) is 0.0775862, this answer has a measurement error of about 0.75%. On the other hand, if \( S₁₁ \) is set to count \( 10^4 \), \( n_2 \) would equal 775, and the displayed ratio would show .0775—an error of only 0.11%. But the reading time for this greater accuracy is 17.24 s vs 1.724 s for the first example. If \( n_1 \) could be greater than \( 10^4 \), then even greater accuracy could be attained, but, of course, at an even longer reading time.

Clearly, the circuit also can handle ratios greater than one. But with \( f_2 \) greater than \( f_1 \), \( N_2 \) might overflow before \( N_1 \) has accumulated the selected number. To indicate such a condition, a LED overflow lamp, controlled by transistor Q₁, turns ON. The overflow latch circuit, flip-flop IC₂₂, actuates when the \( N_2 \) count exceeds \( 1 \times 10^4 \). The overflow LED remains ON until the circuit is manually reset by \( S₂ \).

Determining errors of random-pulse ratios

When the input pulse rates are random and have a Gaussian distribution, the ratio-measuring procedure—whether \( f_1 \) is greater or less than \( f_2 \)—is the same as for the regularly spaced pulse inputs just described. However, now the accuracy of the measured ratios becomes a statistical quantity.

The standard deviation, \( \sigma \), of the measured ratio of random inputs is given by the expression:

\[
\pm \sigma = \frac{n_2}{n_1} \left( \frac{1}{n_1} + \frac{1}{n_2} \right)^{1/2}
\]

1. The decimal point of the four-place readout for the rate-ratio circuit (a) is automatically established by the setting of switch $S_1$. Counter-to-indicator connections (b) for each counter in the $N_i$ chain are identical.

2. For random pulse-rate signals, the count of chain $N_i$, as set by switch $S_1$, determines the expected precision of the ratio measured in terms of a percentage relative standard deviation, $\sigma\%$. 
The standard deviation can be expressed as a percentage deviation from the true mean ratio of the two inputs. This form of the deviation is called a percentage relative standard deviation, \( \sigma\% \):

\[
\pm \sigma\% = 100 \left( \frac{1}{n_1} + \frac{1}{n_2} \right)^{1/2}
\]  

(2)

Eq. 2 allows you to determine the number of counts that must be accumulated in register \( N_1 \) to achieve a specified accuracy.

As an example, consider this mean random-pulse-rate ratio:

\[
f_2/f_1 = n_2/n_1 = 0.2
\]

and a required \( \sigma\% \) of \( \pm 1\% \). Substitute 0.2 \( n_1 \) for \( n_2 \) and the value 1% for \( \sigma\% \), then

\[
\pm \sigma\% = 100 \left( \frac{1}{n_1} + \frac{1}{0.2 n_1} \right)^{1/2}
\]

and \( n_1 = 6 \times 10^4 \).

Similarly, for the same pulse-rate ratio, but for \( \sigma\% = 5\% \),

\[
n_1 = 2.4 \times 10^4.
\]

**Percentage deviation independent of large \( n_2 \).**

Fig. 2 is a plot of the \( n_2 \) counts required for given percentage relative standard deviations, \( \sigma\% \), over a range of random input ratios from \( 10^{-2} \) to \( 10^4 \). It is interesting to note that in Eq. 2, when \( n_2 >> n_1 \), the expression approaches \( 100 / \sqrt{n_1} \), which is independent of the value of \( n_2 \).

For random-signal rates, as in the case of steady-signal rates, large \( n_2 \) counts provide improved accuracy, but only with increased measuring time. Thus, with unknown inputs, if you start with a quick, low \( n_1 \) to help find your “bearings,” then you can trade time for the accuracy you want.

To illustrate the use of the curves in Fig. 2, assume you desire a \( \pm 2\% \) value for \( \sigma\% \), and \( f_2/f_1 = 3 \). Then an \( n_1 \) of 3200 is required. If switch \( S_{-1} \) is set to \( n_1 = 10^4 \), the accuracy is somewhat over 1%—better than specified. On the other hand, if \( n_1 \) is made to equal 10^4, the counting time will be reduced to one-tenth that at \( n_1 = 10^4 \), but the value of \( \sigma\% \) will be about 4%.

Note that Fig. 2 shows the minimum measurable ratios for 10, 5 and 2% values of \( \sigma\% : 0.01, 0.043 \) and 0.35, respectively. Also, \( \pm 1\% \) values can’t be obtained for any ratio attainable with the counters in Fig. 1; \( n_1 \) must be greater than \( 10^4 \). To improve measurement accuracy, additional counter stages can be added to both the \( N_1 \) and \( N_2 \) counter chains.

**References**

3. Hewlett-Packard Application Note 934 (5082-7300 series), Palo Alto, CA.
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SID52501, priced under $1000 is available with 30-day delivery. Or get Big SID in our TC1160 camera for less than $2000.

Hi-speed IR emitters for fiber-optic communications.

The speeds are right: 100 MHz min. analog bandwidth (C30119) or 40 MHz min. (C30123). And so is the size: A 6-mil edge emitter in an OP-18 package with removable cap that assures good collection efficiency with single fibers or bundles. (Also available in hermetically sealed package.) These IR emitters are rated at up to 200 mA forward current for continuous operation and 1.5 A peak forward current for pulse operation. Competitively priced, they're available from stock.
Don't sweat with thermocouple thermometers.
CMOS analog and digital devices make it easy to design an inexpensive thermometer.

Thermocouples (TCs) are reliable and low-cost temperature transducers, but they have two major disadvantages:
- Low output (millivolts).
- Reference-junction drift.

The problems can be avoided by using inexpensive linear-CMOS-chips as low-level signal conditioners, and a bucking voltage for reference-junction compensation. The complex electronics and temperature control of past designs are not needed. Thus TCs are now attractive transducers, even for temperatures as low as 0 to 100°C (see Fig. 1).

Thermocouple probes, as we know, are made by simply welding together the ends of two dissimilar-metal wires. As shown schematically in Fig. 2, however, not one but at least two junctions are formed when a TC is used. In other words, the measurement is differential and affected by reference-junction temperature. Therefore we introduce a voltage that automatically cancels the potential generated at the reference junction.

Compensate for the reference junction

We use a bridge (Fig. 3) containing a temperature-sensitive resistor to generate a compensation voltage. Since only a small output voltage is required, a copper wire with a resistivity tempco of 0.00393 °C is sufficient. For accurate tracking, the copper-wire resistor and the reference TC must be at the same temperature; also, the bridge's output (in terms of µV/°C) must match the reference TC.

Proper layout yields good temperature tracking (i.e., the reference TC is placed near the copper-wire resistor, and both are thermally insulated from the ambient.) The temperature sensitivity of the bridge is then matched to the reference TC by \( R_{adj}(T) \) (Fig. 3), which controls the current through the bridge. Finally, offsets are adjusted using \( R_{offset} \).

Design a compensation circuit

Let's analyze the circuit for automatic reference TC compensation (Fig. 3). For illustration, we will use a Chromel/Alumel couple. The TC's sensitivity at room temperature \( (S_{TC}) \) is 39 µV/°C. This must be matched by the voltage variation across the copper-wire resistor \( (R_{cu}) \) as a function of temperature. If a 15-Ω copper-wire resistor is selected, the current through it \( (I_{cu}) \) is

---

Dr. S. Ben-Yaakov, Head, and Y. Sanandagi, R & D Technician, Institute of Electronics, Ben-Gurion University of the Negev, Beer-Sheva, Israel.
2. Thermocouple temperature measuring involves a measuring-junction M, and a reference-junction R. If the junctions with the copper wire are kept at the same temperature, their potentials cancel.

3. The bridge, using a copper-wire resistor \((R_{cu})\), produces a temperature dependent output voltage for reference-junction compensation. The voltage is made equal and of opposite polarity to the reference junction.

\[
I_{cu} = \frac{S_{TC}}{R_{cu} \times S_{cu}},
\]

where \(S_{cu}\) is the temperature coefficient of resistivity of copper, which is equal to 0.00393 /°C. The required current is

\[
I_{cu} = \frac{40 \times 10^{-4}}{3.93 \times 10^{-9} \times 15} = 0.678 \text{ mA}
\]

Assuming a symmetrical bridge, the current through \(R_{adj}\) \((I_{adj})\) should be

\[
I_{adj} = 2 \times I_{cu} = 1.36 \text{ mA}
\]

and the expression for \(R_{adj}\):

\[
R_{adj} = \frac{V_{ref} - I_{cu} (R_1 + R_{cu})}{I_{adj}}.
\]

4. Automatic-offset-correcting dc amplifier's output is proportional to the difference of \(V_1\) and \(V_2\). The analog switches conduct when their control line is high.

Selecting \(R_1\) to be 5 kΩ and assuming a reference voltage \((V_{ref})\) of 5 V,

\[
R_{adj} = \frac{5 - 0.678 \times 10^{-3} \times 5.015 \times 10^{-3}}{1.36 \times 10^{-3}} = 1.18 \text{ kΩ}
\]

Eliminate dc-amplifier offset

A major problem in the design of TC thermometers stems from the extremely low dc levels involved. Offsets in dc amps tend to mask the signal. We overcome this problem, while using standard CMOS op amps, with an automatic offset-correction circuit. The major components of the circuit are shown in block form (Fig. 4). Operational amplifiers, analog switches and series capacitors are used.

The switches are driven by a square-wave (see Fig. 4). The switches conduct when the drive is high. During the offset-adjustment period, switches A, C, and D conduct. C1 charges to \(V_1\), and \(C_2\) charges to the offset-dc error at the output of \(A_1\). The charge on \(C_1\) and \(C_2\) is maintained during the temperature-measuring half-cycle. The output voltage of \(A_2\) is therefore proportional to
5. Thermocouple thermometer uses all CMOS chips for both analog and digital functions.

V₁ - V₂ and is free of the offset voltage at A₁, which is subtracted out by the voltage across C₂.

Use CMOS circuits throughout

The design principles presented here are applied in the all-CMOS circuit of Fig. 5. It includes an RC oscillator, analog gates and op amps. The op amps’ CMOS input-and-output stages have two useful features:
- **Very low input bias current.** A value of 10 pA is typical. Hence, capacitor discharge (the droop) is negligible during the 5-ms temperature measuring cycle.
- **Ability to operate from a single supply.** The op amps’ input-and-output terminals are permitted to reach ground potential. This simplifies the power supply, an important feature in battery-operated instruments.

With the values shown in Fig. 5, the amplifier has an over-all gain of about 1000 and an offset-voltage drift of less than 0.3 µV/°C. Assuming a duty cycle of 50%, the over-all gain to the filtered output is 500. Use of a Chromel/Alumel TC produces a full scale of 400 mV for a 0-to-100-C temperature span. With a proper series resistor, the signal conditioner can drive a 100-µA moving-coil meter.

Two additional features are:
- Expanded-scale capability.
- Variable bucking voltage.

Using these features together, you can buck out a reading, then expand the scale to measure small superimposed temperature fluctuations with a sensitivity greater than 0.1 C. This procedure produces a resolution less than 4 µV.
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Then there's our Model 275 Industrial Grade Isolation Amplifier, $79 (1-9), that is gain programmable over a range of 1 to 100 by a single resistor with nonlinearity to less than 0.05%. And our Model 285 is like the 275 but features a low impedance op amp output. And our Models 279, 282 and 283 for multichannel applications.

We could go on and on about this line. But our free Analog Devices Isolation Amplifier Handbook says it all. Ask for a copy along with the data sheets on our new Isolation Amplifiers. Write Analog Devices, the real company in isolation amplifiers.

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Low-cost data-acquisition systems need not transmit analog signals. Two-chip integrating a/d converters need only two wires for data handling.

Putting together a low-cost data-acquisition system is getting easier all the time, especially when it's based on a microprocessor. By placing the analog half of a two-chip integrating analog-to-digital converter at each monitoring point, you can get the benefits of all-digital communications and still maintain good accuracy.

Potential advantages of a system based on a two-chip a/d converter include:
- Accuracy to better than 0.1%.
- Communication and control with only two digital signals.
- Noise immunity of digital signals.
- Multiple remotes can be easily multiplexed.
- Convert-command capability with no extra leads.
- Simple interface to monitors or a processor.
- Small hardware commitment at the remote sites.

Previously, all the analog sensor outputs had to be routed to one central point, multiplexed and sequentially converted to digital form (Fig. 1). Unfortunately, the analog variables are often widely dispersed—and must be transmitted over long cable runs where signal losses and noise pickup can occur.

By using an a/d converter at each point and then transmitting the words to a multiplexer you
2. The 1405 analog-converter subsystem permits you to remotely locate a small part of the total data collection system, yet still retain complete control of conversion.

solve the transmission problem, but increase the costs.

A two-chip a/d converter system—the MC-1405/14435, for example—can provide an intermediate solution when up to 3-1/2 digit resolution is needed (Fig. 2). The 1405 analog subsystem and the 14435 digital subsystem communicate through only two digital signal lines—a ramp control and a comparator output. As a result, the analog subsystem can be remotely located from the digital half.

To multiplex the different 1405 subsystems to a single 14435, a central controller must be able to start and stop the conversion process of each 1405 at any time. This is easy enough to do: just bring the ramp control line HIGH and the 1405 comparator output will be LOW. However, in this idle state there are two stringent requirements for the integrating capacitors.

1. The capacitor, during idle conditions, will see reverse dc voltages and so must be nonpolar. The required capacitance is a function of supply voltage, clock frequency and maximum allowed input, and can be calculated from:

\[ C_1 = \frac{(V_{IN\text{MAX}}/2.7\,\text{kΩ}) (1000/|f (V_{CC} - 3.3)|)}{2}. \]

The system clock should be high enough in frequency to allow a convenient value of \( C_1 \). (Frequencies between 100 kHz and 1 MHz are possible.) At a \( V_{IN} \) of 1 V, a \( V_{CC} \) of 12 V and an \( f = 500 \text{ kHz} \), \( C_1 \) is 0.15 \( \mu F \).

2. The dielectric absorption of the capacitor must be low if the first conversion after restart is to be accurate. If 0.1% accuracy for the first conversion is required, an expensive polycarbonate capacitor with a value in tenths of a microfarad must be used. You can get away with a lower cost Mylar capacitor if two conversions at each remote site are permitted. At a 500-kHz frequency, each conversion requires about 15 ms.

A typical remote a/d converter station using the 1405 can operate from a single supply, use the MC3403 quad op amp as an input buffer, have true differential inputs and have a common-mode input range to zero (Fig. 3).

Multiplexing the 1405 is easy

The circuit shown in Fig. 4 can be used to multiplex four remote stations with a 14435 digital subsystem. By extending the counter chains and multiplexing gates, you can expand the system to 32 channels and provide three updates per second for each channel. The ramp control signal drives half of the 14520 dual binary counter. Outputs \( Q_2 \) and \( Q_3 \) from the 14520 provide the station scan addresses and commit the 14435 to the station for each conversion.

During the first conversion of each channel the strobe line remains LOW (controlled by \( Q_1 \) of the 14520), thus keeping the incorrect 14435 output from reaching a display or processor. The second conversion result gets strobed out since the \( Q_3 \) output goes LOW.

When the comparator signal from the remote 1405 goes LOW, it inhibits the 14435 clock. Data get strobed into the 14435 latches and the counters and ramp control are reset. The ramp control change also advances the address counter, which...
Basic operation of the 1405/14435 a/d converter

The MC1405 and 14435 ICs form a dual-slope a/d converter that delivers a 3-1/2 digit BCD output (max. count 1999). The digital subsystem chip (14435) controls the direction of integration in the analog subsystem (1405) through its ramp control output. A logic ZERO initiates a ramp-up operation and a ONE starts the ramp-down function. A comparator output of the 1405 controls the clock of the 14435.

At the start of a conversion cycle, the ramp control and comparator lines are at ZERO. The integrator then ramps upward through the internal comparator threshold, changing the comparator output to ONE, and thus starting the clock in the 14435. The integrator in the 1405 continues to ramp upward until the internal counter of the 14435 reaches a count of 1000, at which point the ramp control line of the 14435 goes HIGH. Now, the integrator starts ramping down, with a slope determined by an internal reference.

The comparator output remains HIGH until the down-going ramp voltage crosses the comparator threshold. During the downward ramp the 14435 counts pulses from a stable oscillator and latches the count when the comparator output goes LOW. The counters and other internal control circuitry are also reset and the ramp control line returns to ZERO, thus initiating the next conversion.
in turn opens the first channel's MC14529 transmission gate. With the transmission gate held open, the 10 kΩ resistor keeps the ramp control line HIGH and the 1405 integrator voltage ramps to zero and stays there.

As the first channel's ramp voltage crosses the comparator threshold, the next channel gets a ramp-up command from the 14435 and the process repeats. The MC14028 binary-to-one-of-eight decoder monitors the address scanner and delivers a display-select output that is held HIGH during each conversion so that the display shows the results of any channel that is selected.

The half of the 14530 that hasn't been used yet can provide a data-update strobe signal that goes HIGH with the ramp-up command and returns to the LOW state after the third clock pulse of the conversion cycle. Thus, you can use it to enable and disable the redundant digit-select pulses available from the NOR gates in Fig. 4.

Interfacing the output data from the 14435 can be done in several different ways. The circuit of

5. Simple control and drive circuitry can decode the multiplexed BCD data and display it on a 3-1/2-digit liquid-crystal display.

6. A complete 16-channel system using a binary-output digital subsystem can feed all data into a microprocessor-based controller under software command. The 6820 PIA generates the software interrupt.
7. For short-distance signal transmission, the MC696 dual line-driver/receiver can operate at distances up to 25 ft (a). For longer distances, a floating data bus can be used over a two-wire twisted pair (b). Cable runs of 100 ft and more can be used with the floating bus and only a twisted-wire pair is necessary.

8. Optically isolated data transmission can be used in areas where ground potentials present damaging levels to the circuits. For long cable runs emitter followers provide the drive capability.

Fig. 5 uses three 4-bit data latch decoders (MC14543) and the MLC400 liquid-crystal 3-1/2 digit display. A triple 3-input AND gate (MC14073) controls the update of the display; the clock circuit, consisting of two inverters and one-half of an MC14013 D flip-flop, controls the LCD phasing frequency.

The output lines can also feed data into a µP based system (Fig. 6). An end-of-conversion signal generated by the comparator interrupts the processor when the new data word is ready.

Interfaces for the 14435 are simple

For µP-based data-acquisition networks, a parallel-binary format is preferable. The circuit of Fig. 6 uses a 12-bit binary equivalent of the 14435 to interface with an M6820 peripheral interface adapter in a 6800-based system.

Data from any of the 16 channels come once every two conversions. The comparator's output generates a software interrupt signal that feeds into the CA1 line of the 6820. It causes the 6800 to store the 16-bit word output of the binary subsystem. Lines PA0 and PA3 of the 6820 provide a 4-bit channel label and lines PA4 to PB7 provide the 12 data bits.

The ramp control output of the binary subsystem advances the MC14024 counter, thus incrementing the scan address. If either the 14435 or
the binary subsystem is used, the processor can provide channel addresses under software control.

Digital CMOS signals are not ideal for long-distance transmission. Requirements will vary, of course, depending upon your application, but let's look at several line driving schemes using the MC696 dual line driver/receiver.

Do the signal transmission with line drivers

For distances of 25 ft or less the 696 can be used directly as a single-ended line driver (Fig. 7a). If capacitive decoupling of power supplies for the circuits is not possible at remote locations, you can use an MC7812 regulator to power the 696 circuit. Over short distances the cost of a four-wire cable is probably less than the cost of a remote supply.

When distances increase to more than 25 ft, a single twisted-wire pair can be used to transmit the digital data (Fig. 7b). This method parallels the output of one driver with the input of another and can send data over distances of more than 100 ft.

This “floating bus” method uses the real-time nature of the control signals. Conversion information is contained in the time between ramp control transitions and comparator signals, and the nature of these signals guarantees that the two will always alternate. Any voltage caused by the transmission-line delay can be calibrated out by the 1405’s zero adjust.

The voltage between points A and B on the schematic of Fig. 7b can be positive, negative or zero depending on the outputs of IC1A and IC2A. The diode-resistor networks on each output modify the signals to form sink and source nodes.

You are still able to decode the information since the alternating-edge constraint keeps everything in sync. Also, one of the signals is locally generated and the other must be received and decoded at the sensor. IC1B generates the ramp-control signal simply by using its internal hysteresis. The comparator signal at IC2B is derived from the switching of the receiver threshold each time the ramp control line changes state. A 500-pF capacitor connected to IC2B slightly delays the ramp control signal to ensure that the line driver cannot detect the edge that switches the threshold.

In many instrumentation systems, large ground-potential differences can create interconnect problems to a central collection point. Optoisolators can be used on the outputs or inputs of the 696s to provide isolation of up to 2500 V (Fig. 8). Back-to-back LEDs from two 4N25 couplers operate at about 8 mA and provide bidirectional signal handling. If extremely long lines are used, emitter followers can increase the line-driving capability.
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### MAJOR PARAMETER LIMITS

<table>
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<th>Type</th>
<th>hFE @ 25A</th>
<th>hFE @ 10A</th>
<th>VCEO (ss)</th>
<th>VCEO (sat)</th>
<th>ICEO @ 20A</th>
<th>ICEO @ 600V</th>
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#### TYPICAL SWITCHING

- DTS-4066
- DTS-4067
- DTS-4074
- DTS-4075

<table>
<thead>
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<th>Parameter</th>
<th>Typical Values</th>
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<tr>
<td>t\text{g}</td>
<td>5.0\mu s</td>
</tr>
<tr>
<td>t\text{f}</td>
<td>4.5\mu s</td>
</tr>
</tbody>
</table>

NPN triple diffused silicon Darlingtons are packaged in solid copper cases conforming to JEDEC TO-3 outline dimensions.

with parallel Darlingtons. A speed-up diode is built into the DTS-4074 and DTS-4075 permitting data sheet t, typicals of 1.0 \mu s. Drive circuit techniques involving I_	ext{g2} \geq 2 A and a Baker clamp produce t, typicals in the 0.4-0.6 \mu s range for the DTS-4066, DTS-4067, DTS-4074, and DTS-4075.

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These Darlingtons are already in high volume production and are available on distributor shelves. Prices, applications literature, and data sheets from your nearest Delco sales office or Delco distributor can complete the story on these new Darlingtons.

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<td>PHOENIX</td>
<td>Sterling Electronics, Inc.</td>
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<td>SUNNYVALE</td>
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<tr>
<td>COLORADO</td>
<td>DENVER</td>
<td>Kierulf Electronics, Inc.</td>
<td>(303) 371-6500</td>
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<td>NORWALK</td>
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<tr>
<td>Montreal</td>
<td>(514) 730-5361</td>
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<td>700 E. Fitzmor, Kokomo, Ind. 46901</td>
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**Electronic Design**

| 24, November 22, 1976 |
| CIRCLE NUMBER 81 |

**Delco Electronics**

| Division of General Motors |
| Kokomo, Indiana |
Consider v/f converters for data-acquisition systems. They offer high resolution and accuracy when used as analog-to-digital converters.

Examine the performance specifications of voltage-to-frequency converters before you pick an analog-to-digital converter for your application. Three relatively inexpensive (under $100) methods—the successive-approximation, dual-slope and voltage-to-frequency conversion schemes—can deliver equal accuracy, but each is used best in a different application (Table 1).

Look at the key converter specifications (Table 2) to evaluate the performance of v/f converters compared to the two other methods. Some of the most commonly specified parameters are resolution, linearity, conversion time, temperature stability and monotonicity (no missing codes).

V/f conversion: an alternative a/d method

Seldom used until a few years ago, v/f conversion techniques are rapidly becoming popular as an alternative to successive-approximation or dual-slope techniques. There are several ways to build a v/f conversion circuit, but the charge-balancing method (Fig. 1a) is the most popular.

If \( V_{in} \) is positive, the integrator output ramps down until its output voltage \( V_o \) crosses the comparator's threshold (ground, in this case) and causes the comparator to change state. The transition, in turn, triggers a precision timing circuit that delivers a constant-width pulse. The pulse gets fed to two places: a buffer circuit that then feeds the output; and the integrator, where the pulse causes the integrator output to rapidly ramp up (Fig. 1b).

The timing circuit is, in effect, a precision one-shot multivibrator that is stable with both time and temperature. The reference current, \( I_{ref} \), must also be stable, and a precision regulator with a voltage reference source is included for that purpose.

Since the reference current is pulled from the integrator summing junction for a fixed amount of time, and at intervals determined by the input voltage, the positive-input current feeding the integrator balances the current pulses being pulled out. The integrator can be made extremely linear and, when combined with the charge-balancing feedback loop, can achieve nonlinearities as low as 0.005%.

To form an a/d converter with the v/f technique, the output of the v/f circuit must feed a counter that is gated for the desired maximum count (for a converter with a 10-kHz output, a four-digit BCD counter or a four-stage binary counter can be used).

Nail down the definitions first

Before you start comparing specifications, make sure the specs are defined. Resolution tells you the smallest quantity the converter can distinguish. Even though the quantity is usually an analog voltage the resolution is given in terms of bits: 8, 10, 12 or more.

The usable resolution of a converter can be less than the stated resolution. However, because it's a function of linearity and stability, the usable resolution can often change with time and temperature.

In the v/f form of an a/d converter, the resolution is determined by the full-scale frequency, the time base and the capacity of the counter used (Fig. 2). If a 10-kHz v/f converter is used with a time base of 1 second and four decade counters, its resolution is one part in 10,000, or four binary-coded decimal (BCD) digits. Successive-approximation or dual-slope converters with straight binary coding would have to deliver a digital output of at least 13 bits to come close (13 bits = 1 part in 8192). A v/f-based a/d converter can also deliver straight binary. To make a 12-bit unit, use three 4-bit binary counters and set the time base equal to 0.4096 seconds.

In dual-slope converters, resolution is also a function of integration time, clock frequency and counter capacity. Successive-approximation units use weighted current sources, and the number of sources determines the resolution. The higher the number of bits, the harder it becomes to maintain the linearity of the weighted sources.

Eugene Zuch, Senior Engineer, Datel Systems, 1020 Turnpike St., Canton, MA 02021.
Table 1. Typical converter applications

<table>
<thead>
<tr>
<th>A/d converter type</th>
<th>Common applications</th>
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<tbody>
<tr>
<td>High-speed data-acquisition systems</td>
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<tr>
<td>Pulse-code-modulation systems</td>
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<tr>
<td>Waveform sampling &amp; digitizing</td>
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<tr>
<td>Automatic test systems</td>
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<td>Digital process control systems</td>
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<tr>
<td>Digital multimeters</td>
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<tr>
<td>Digital panel meters</td>
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<tr>
<td>Laboratory measurements</td>
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<tr>
<td>Slow-speed data-acquisition systems</td>
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<tr>
<td>Monitoring systems</td>
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<tr>
<td>Ratiometric measurements</td>
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<tr>
<td>Measurements in high-noise environments</td>
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<tr>
<td>Dual slope</td>
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</tr>
<tr>
<td>Digital multimeters</td>
<td></td>
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<tr>
<td>Digital panel meters</td>
<td></td>
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<tr>
<td>Remote data transmission</td>
<td></td>
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<tr>
<td>Totalizing measurements</td>
<td></td>
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<tr>
<td>Measurements in high-noise environments</td>
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<tr>
<td>High-voltage isolation measurements</td>
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<tr>
<td>Ratiometric measurements</td>
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<tr>
<td>Voltage to frequency</td>
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<tr>
<td>Digital multimeters</td>
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<td>Digital panel meters</td>
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<td>High-voltage isolation measurements</td>
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<tr>
<td>Ratiometric measurements</td>
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</tbody>
</table>

Table 2. Comparison of a/d converter types

<table>
<thead>
<tr>
<th>Specification</th>
<th>Successive approximation</th>
<th>Dual slope</th>
<th>Voltage to frequency</th>
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<tbody>
<tr>
<td>Resolution</td>
<td>12 bits</td>
<td>12 bits</td>
<td>12 bits</td>
</tr>
<tr>
<td>Missing codes</td>
<td>none by careful design</td>
<td>none, inherent</td>
<td>none, inherent</td>
</tr>
<tr>
<td>Nonlinearity</td>
<td>±0.012% max.</td>
<td>±0.05 to 0.01% max.</td>
<td>±0.005% max.</td>
</tr>
<tr>
<td>Diff. nonlinearity</td>
<td>±1/2 LSB</td>
<td>≈ 0</td>
<td>≈ 0</td>
</tr>
<tr>
<td>Tempco</td>
<td>10 to 50 ppm/°C</td>
<td>10 to 50 ppm/°C</td>
<td>10 to 50 ppm/°C</td>
</tr>
<tr>
<td>Conversion time</td>
<td>2 to 50 μs</td>
<td>5 to 77 ms</td>
<td>0.041 to 0.41 s</td>
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<tr>
<td>Noise rejection, 60 Hz</td>
<td>None</td>
<td>40 to 60 dB</td>
<td>33.8 dB*</td>
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</table>

*For 0.41-s conversion time.

Linearity is the acid test of any a/d converter specification since resolution can be unusable if linearity error doesn’t hold to less than ±0.5 LSB (1 LSB at the worst). At a fixed temperature, linearity is the only error that remains after offset and gain errors have been adjusted out.

The linearity error of a converter is the maximum deviation of the output values from a straight line drawn from zero to the maximum output. For 12-bit a/d converters a “good-quality,” successive-approximation unit has a non-linearity of about ±0.012%. A dual-slope unit about ±0.05 to ±0.01% and a v/f converter about ±0.01 to ±0.005%.

The nonlinearity characteristic of successive-approximation converters differs fundamentally from that of the dual-slope or v/f. Typical non-linearity curves are shown (slightly exaggerated) in Fig. 3.

Both the v/f and dual-slope converter linearity characteristics tend to have a bow that is caused by the operational integrators used in the con-
1. The basic charge balancing v/f converter (a) uses an operational integrator with a precision timing circuit connected in a feedback loop. The output pulse width (b) is proportional to the charge stored in the capacitor.

2. By using a v/f converter and a precision timer, you can build an a/d converter that delivers a BCD output.

3. Nonlinearities of v/f and dual-slope a/d converters appear as a slight bow in the curve. However, successive-approximation nonlinearities make the curve jagged.

Don't let the converter slow you down

The v/f converter takes the longest to do a complete conversion. The time base used in Fig. 1 is 1 second for a single conversion—rather slow for most applications. Dual-slope converters are faster, with conversion times ranging from 5 ms to 100 ms.

Successive-approximation converters are the fastest of the three, with conversion times as short as 2 µs for 12-bits. Most successive-approximation converters have conversion times between 3.5 and 50 µs.

However, if time isn’t a problem, you can increase the time base to 10 seconds, add another decade counter and, voila: a converter with a resolution of one part in 100,000. Such a long conversion time could cause difficulty in many applications. And, the linearity of the 10 kHz unit would not be commensurate (±0.012% for a 12-bit converter).
Successive approximation and dual slope conversion methods

The successive-approximation approach is the most widely used (Fig. A) of the three most popular conversion schemes. It compares the output of an internal d/a converter against the input signal, one bit at a time. Therefore, N fixed time periods are needed to deliver an output N bits long, but the total time needed is independent of input-voltage value.

The first step after the start pulse in a successive-approximation conversion cycle is turning on the MSB, which sets the d/a converter's output at half-scale (Fig. B). This analog signal is then fed back to the comparator. The MSB is left on if the d/a converter's output is smaller than the analog input, and turned off if the output is larger.

Next, the second bit is turned on, and the quarter-scale value added to the d/a converter output and the comparator again does its job. This process continues until the LSB has been tested and the final comparison made. When the process is complete, the converter signals this by changing the state of its end-of-conversion (status) output. The final digital output can then be read from the output of the successive-approximation register of the converter.

Successive-approximation converters can achieve conversion speeds of 100 ns/bit in medium-priced ($250 to $350) 8 and 10-bit units. Converters with 12-bit outputs are typically available with conversion times ranging from 2 to 50 µs.

Dual-slope units slow the pace

The dual-slope converter uses a simple counter to indirectly measure the input signal after an operational integrator converts a voltage into a time period (Fig. C). This scheme is the second most commonly employed method and is used, almost exclusively, in such instruments as digital multimeters and panel meters.

The conversion cycle begins when the analog-input signal is switched to the input of the operational integrator. The voltage is integrated (Fig. D) for a fixed time period determined by the clock frequency and the counter size. At the end of the period, the integrator input is switched to an internal reference whose polarity is opposite that of the original analog input. The reference is then integrated until the output reaches zero and triggers the comparator.

During the second integration, the clock is gated into a counter chain that accumulates the count until the comparator inhibits the clock. When the clock signal stops, the conversion is complete.
high levels of input noise.

For these two integrating converters, the longer the signal is integrated, the better the noise attenuation. When the integration period equals a multiple of the inverse of the line frequency (for dual-slope units), the noise rejection becomes infinite at integral values $T_n$, where $T$ is the integration period and $f_n$ is the noise frequency (Fig. 4). V/f converters don't, in general, use a period that is a multiple of any periodic noise, and so the asymptote of the noise-rejection curve is used to determine the rejection at a given $T_n$.

The v/f converter's noise-rejection asymptote rises by 20 dB per decade, and, for a 60-Hz power line and a 0.41-s conversion time, the rejection can be computed at 33.8 dB. Dual-slope converters have rejection ratios as high as 60 dB when conversion is synchronized with the noise frequency.

Successive-approximation converters have no noise-rejection capability whatsoever. Input noise at any time during the conversion process can cause significant conversion errors. (Noise feeds directly to the comparator and can change the decision point.) The only way to minimize noise is to add an input noise filter to the converter.

**Temperature coefficients change converter specs**

Operation at different temperatures can tremendously alter converter performance, no matter which converter type you select. These changes affect offset and gain, two important converter parameters. Even though offset and gain are adjusted during calibration, they can change significantly with temperature.

Offset is a function of current-source leakage, comparator bias current and comparator input voltage offset. Gain (sometimes called scale factor) is a function of the voltage reference, resistor tracking and semiconductor-junction matching—and is usually the most difficult parameter to control. Absolute accuracy is affected by offset and gain changes, so if these change during operation, output errors will occur.

And, if the linearity degrades, a converter can actually skip output codes (become nonmonotonic). (An a/d converter is said to have no missing codes when, as the analog input of the converter increases from zero to full scale or vice versa, the digital output passes through all of its possible states.) Both the dual-slope and v/f converters are inherently monotonic because of their integration techniques and the use of counting circuits to deliver the digital output.

The successive-approximation a/d converter, on the other hand, is more prone to missing codes. The code jumps occur when the analog transitions between adjacent output codes become greater than 1 LSB. Because the jumps can be greater than 1 LSB, another spec. differential nonlinearity, becomes very important. Differential nonlinearity is defined as the maximum deviation of the size of any adjacent code transitions from their ideal value of 1 LSB.

A specified differential nonlinearity of $\pm 0.5$ LSB tells you that the magnitude of every code transition is 1 LSB $\pm 0.5$ LSB, maximum. The differential nonlinearity can reach a maximum of $\pm 1$ LSB before converter performance is in doubt.

Picking the right converter for your application is no easy matter. For example, digital multimeters typically use a dual-slope converter since high speed isn't necessary but high noise rejec-
6. V/f converters can be used in simple, remote data-gathering applications since only a twisted pair of wires is needed to transmit the signals (a). Differential line drivers can be added if long transmission distances are required (b), or an opto-isolator can be used to eliminate large, common-mode voltage problems (c).

7. A microprocessor or computer-based controller can be used to make a multiple-channel data-collection system with a v/f converter at each point (a). If manual switches are used instead of a timer, you can turn a v/f-based a/d converter into an "infinite" integrator (b).

8. The integration process in a v/f converter can be defined in terms of millivolt-seconds for each pulse delivered. To get the total area, simply multiply the total count by 0.001.

9. If you use two v/f converters, you can make a high-accuracy, ratiometric a/d converter. Because of the wide frequency span covered, the dynamic range of the converter can reach 10,000:1.
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Drift-free integration is only one bonus

Unlike analog integrators that must use "super high quality" components when the integration period extends past several minutes, the \(v/f\) integrator uses inexpensive components and can even hold its value indefinitely.

A 10-kHz \(v/f\) converter delivers a pulse every 0.1 ms if the input is 10 V, or a pulse every 1 ms if the input drops to 1 V. You can manipulate these facts and say that the converter generates an output pulse for every millivolt-second of input signal. The output-pulse count then represents a piece-by-piece addition of input voltage/time area (Fig. 8). The integral of the signal with time is the total count multiplied by 0.001 volt-seconds.

You can put together a ratiometric a/d converter (Fig. 9) by combining two \(v/f\) converters and a divide chain. Input \(V_1\) acts as the numerator and \(V_2\) as the denominator, while the divide chain acts as a scale factor.

\[
\text{Count} = 2N V_1 / V_2
\]

If you use 10-kHz \(v/f\) converters, the time base period is no longer than 1 second for ratios of up to 1000 to 1. Unlike other ratio-measurement methods that have rather limited dynamic ranges, using two \(v/f\) converters permits a possible dynamic range of 10,000 to 1.
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Inverter circuit handles bidirectional signal flow without latching up

This unusual two-terminal circuit not only inverts logic pulses or levels, but also each of its terminals can serve as either an input or an output. Positive input signals to its terminal 1 are inverted to negative outputs at terminal 2. Conversely, negative-input signals must enter terminal 2 to provide positive outputs at terminal 1. This bidirectional circuit can be used in low-power applications such as CMOS circuits, because it draws current only when a signal level is being inverted.

The problem of latch-up that results if such a circuit is built with the usual logic modules is solved with one inhibit circuit, Q3 or Q4, for each inverter. As a result, only one inverter, Q1 or Q2, respectively, functions at a time.

Diodes D1 and D2 discriminate between incoming and outgoing logic levels at their respective terminals; therefore, corresponding inverters turn ON only when an input terminal has a signal.

For example, with a positive pulse applied to terminal 1, D1 becomes reversed-biased, and Q1 remains cut off, but inverter Q2 turns ON to bring terminal 2 near ground. Thus, the positive signal at terminal 1 is inverted. Transistor Q3 also turns ON and keeps inverter Q2 OFF, which prevents Q1 from latching Q2 ON.

Similarly, a negative signal into terminal 2 reverse biases D2 to keep Q2 OFF and also turns Q1 ON. Transistor Q3 turns Q4 ON, which then holds Q4 OFF to prevent Q1 from latching. Terminal 1, therefore, is now the output and provides a negative signal.

Component values for the circuit are not critical. They can be chosen to conform to individual power-supply and logic-drive requirements. Diodes D1 and D2 can be general-purpose germanium switching diodes when used with low-threshold logic, such as TTL.

Larry Acker, Engineering Associate, Steiner-Parker Co., 356 S. 900 East C, Salt Lake City, UT 84102.
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CIRCLE NUMBER 280 FOR INFORMATION
CIRCLE NUMBER 281 FOR FREE DEMONSTRATION
A simple technique accurately generates symmetrical triangular and square waveforms whose frequency is directly proportional to an external control voltage.

The circuit (Fig. 1) uses a voltage-controlled current generator (VCCG) that is connected across a full-wave diode bridge (D₁ through D₄) to charge and discharge an integrating capacitor, C. The charge and discharge paths for C have identical linearity, because they pass through the same unidirectional current generator. A Schmitt-trigger dual-comparator circuit and an SPDT analog switch completes the free-running circuit.

With the capacitor, C, initially discharged and the flip-flop, F, in the set state, the X output of the flip-flop is HIGH and the S₁, “contact” of S₁A is closed; S₂ is open. A constant current then flows through the bridge from the +10-V supply along the path MLKN to capacitor C.

The magnitude of this constant current, I, is controlled by the controlling voltage, Vᵣ, and by the emitter resistor, Rₑ, of transistor Q₁. The controlled constant-current linearly charges C until the voltage passes the upper-trip-point voltage, V₉, of the comparator, CO₁. When CO₁ trips, it resets the flip-flop, which turns S₁ OFF and S₂ ON.

At this point, the −10-V supply rail connects to the bridge discharging C at the same rate as it was charged, but over path NLKM. Current I is the same as when C was charging.

When the discharging voltage at node N crosses the lower trip-point voltage, V₁, CO₂ provides a signal that sets the flip-flop back to the initial condition. A free-running symmetrical triangular waveform appears at node N. The output terminal of the flip-flop provides a TTL-compatible square waveform.

A CA 3098 dual-level detector with memory can be used to replace the Schmitt and analog switch and thus reduce the number of required components.

Not only is the triangular wave linear, but also the control of the frequency is linear with respect to variations in the control-voltage, Vᵣ.

1. A triangular and square-waveform generator is linearly voltage controlled by a constant-current generator. A diode bridge allows the use of the same current generator for both charging and discharging the timing capacitor—and thus produces symmetrical waves.
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CIRCLE NUMBER 85
components. Also, the CA 3098 has a large driving capability, so its output square waveform can swing almost fully from +V to −V and thereby eliminate the requirement for an analog switch.

The charging time, \( T_1 \), of the capacitor \( C \) is

\[
T_1 = \frac{(V_U - V_L)C}{V_C/R_E} = V\cdotC\cdotRE/V_c
\]

where, \( V = (V_U - V_L) \) = peak-to-peak amplitude of the triangular waveform. Similarly, the discharging time, \( T_2 \), of the capacitor is

\[
T_2 = V\cdotC\cdotR_E/V_c
\]

The frequency of oscillation is then

\[
f = \frac{1}{T} = \frac{1}{(T_1 + T_2)} = V_c/2\cdotC\cdotR_E\cdotV = k\cdotV_c
\]

Fig. 2 shows the linear f-vs.-Vc output that the circuit can deliver.

Rana Dattagupta, Dipak K. Basu, and Pradip K. Das Computer Centre, Jadavpur University, Calcutta, India 700032. CIRCLE NO. 312

---

**Control the data rate of a µP system with software instructions**

You can control the data rate of a microprocessor system with software by the use of three or four ICs (Fig. 1). It's possible that your system already contains a bit-rate generator, such as the MC14411, and a 3-to-8 line demultiplexer—a 74LS138. The 74LS138 generates 1-k-byte boundary chip-select signals. In Fig. 1, the last eight 1-k steps of the addressing range provide chip-select signals for ROM, RAM and other devices.

One of these bytes, \( Y_i \), when inverted and NANDed with an inverted read/write (R/W) signal, provides a new write signal to a 74LS75 four-bit latch. The 74LS75 need not be used to its full capability, since eight of the 16 frequencies generated by the MC14411 with a 1.84-MHz crystal are more than adequate to cover most data-communications requirements. Thus the fourth bit could be used in conjunction with a LED to provide diagnostics or status indications.

Three data bits select the 1-of-8 frequencies available from the MC14411 with a 74LS151.

The MC14411 has four time bases—64, 16, 8 or 1—selectable by its terminals, RSa and RSb. In this application base 16 is programmed so that the bit rates sent to the transmitting device are 16 times the data rate. Output Q of the 74LS75 could be connected to RSa of the MC14411 to provide bases 16 or 64.

During power-on procedures, firmware should address E400H and write 000 on the data bus; thus the circuit selects 110 baud for starting purposes. The control can then be transferred to an operator to make a new data-rate selection via a keyboard entry.

Garret Spears, Senior Engineer, Chem-Nuclear Systems, Inc., P.O. Box 1866, Bellevue, WA 98009. CIRCLE NO. 313

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Go with the Pros and you can't go wrong.
Use TTY or CRT interchangeably on μP system

The 6800 microprocessor family contains an Asynchronous Communication Interface Adapter (ACIA). The ACIA provides data formatting and control to interface to the microprocessor such serial I/O devices as TTYs, CRTs, and thermal printers.

A problem arises when the ACIA is used in a system in which a TTY or CRT terminal may be interchanged. A TTY requires 11 bits of serial data (2 stop bits) at 110 baud, while most other serial I/O devices—such as CRTs or thermal printers—require 10 bits of serial data (1 stop bit) at rates above 300 baud.

Although the baud rate can be readily varied manually with a switch, the 10 or 11-bit (1 or 2 stop bits) format must be programmed into the ACIA by the microprocessor. Since there are no external inputs to the ACIA for identifying whether 10 or 11 bits are required by the I/O device, a simple method was devised to inform the microprocessor how to program the ACIA.

The method uses the image locations created by “don’t cares” in the address decoding. A typical addressing technique for ACIAs is shown in Table 1. Other images—8014-8017, 8024-8027, . . . —may be eliminated by decoding address bits A14 through A4, as required.

Locations 8004 through 8007 are used as examples only; this technique may be used at any address. By not decoding address bit A1, locations 8004 and 8006 respond identically and are images of the Control and Status registers. Locations 8005 and 8007 are images of the Input/Output registers.

If the register-select (RS) pin of that ACIA is tied to A1 rather than A0, then locations 8004 and 8005 are images of the Status and Control register while 8006 and 8007 become images of the Input/Output register.

During initialization, the MPU compares locations 8004 and 8006 (Table 2). If they are equal, the ACIA is programmed for 11 bits, otherwise the ACIA is programmed for 10 bits. Locations 8004 and 8007 are always used as Control/Status and Input/Output, respectively.

Fig. 1 is a block diagram of a typical ACIA implementation. The advantages of this method are:

- No address decoding, other than switch S1, is required.
Switch S1 does not load address lines.
Switch S1 may be incorporated with the baud rate switch, S2, at the 110-baud position.
No tests need be made on locations 8005 or 8006 after initialization, since 8004 is always Status and Control and 8007 is always I/O.
The method allows software to remain the same when hardware changes.


CIRCLE NO. 314

1. The TTY/CRT bit-section switch, S1, can be incorporated into the baud-rate switch, S2.

TABLE 1. ACIA ADDRESSING TECHNIQUE

<table>
<thead>
<tr>
<th>CS0</th>
<th>CS2</th>
<th>CS1</th>
<th>DON'T CARE</th>
<th>RS</th>
<th>LOCATIONS</th>
</tr>
</thead>
<tbody>
<tr>
<td>A15-VMA</td>
<td>A3</td>
<td>A2</td>
<td>AI</td>
<td>AO</td>
<td>8004-8006</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>8005-8007</td>
</tr>
<tr>
<td>A15-VMA</td>
<td>A3</td>
<td>A2</td>
<td>AO</td>
<td>A1</td>
<td>8004-8005</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>8006-8007</td>
</tr>
</tbody>
</table>

TABLE 2. ACIA INITIALIZATION ROUTINE

<table>
<thead>
<tr>
<th>n+0</th>
<th>CE</th>
<th>LDX I</th>
<th>SETS INDEX REGISTER ON ACIA</th>
</tr>
</thead>
<tbody>
<tr>
<td>n+1</td>
<td>80</td>
<td></td>
<td></td>
</tr>
<tr>
<td>n+2</td>
<td>04</td>
<td></td>
<td></td>
</tr>
<tr>
<td>n+3</td>
<td>86</td>
<td>LDA I</td>
<td>MASTER RESET ACIA</td>
</tr>
<tr>
<td>n+4</td>
<td>03</td>
<td></td>
<td></td>
</tr>
<tr>
<td>n+5</td>
<td>A7</td>
<td>STA X</td>
<td>(8004)</td>
</tr>
<tr>
<td>n+6</td>
<td>00</td>
<td></td>
<td></td>
</tr>
<tr>
<td>n+7</td>
<td>44</td>
<td>LSR A</td>
<td></td>
</tr>
<tr>
<td>n+8</td>
<td>A7</td>
<td>STA X</td>
<td>(8004) STORES A0 IN ACIA CONTROL</td>
</tr>
<tr>
<td>n+9</td>
<td>00</td>
<td></td>
<td>REGISTER FOR TTY (11 BITS)</td>
</tr>
<tr>
<td>n+A</td>
<td>A6</td>
<td>LDA X</td>
<td></td>
</tr>
<tr>
<td>n+B</td>
<td>00</td>
<td>(8004)</td>
<td></td>
</tr>
<tr>
<td>n+C</td>
<td>A1</td>
<td>CMP X</td>
<td>(8006) READS ACIA STATUS AND</td>
</tr>
<tr>
<td>n+D</td>
<td>02</td>
<td></td>
<td>COMPARES IT TO LOCATION 8006</td>
</tr>
<tr>
<td>n+E</td>
<td>27</td>
<td>BEQ</td>
<td>IF EQUAL LEAVE ACIA</td>
</tr>
<tr>
<td>n+F</td>
<td>04</td>
<td></td>
<td>PROGRAMMED FOR TTY</td>
</tr>
<tr>
<td>n+10</td>
<td>86</td>
<td>LDA I</td>
<td></td>
</tr>
<tr>
<td>n+11</td>
<td>09</td>
<td>RS232 CONTROL WORD</td>
<td></td>
</tr>
<tr>
<td>n+12</td>
<td>A7</td>
<td>STA X</td>
<td>IF NOT PROGRAM ACIA FOR</td>
</tr>
<tr>
<td>n+13</td>
<td>00</td>
<td>(8004)</td>
<td>10 BIT OPERATION</td>
</tr>
</tbody>
</table>

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ELECTRONIC DESIGN 24, NOVEMBER 22, 1976
Stable constant-voltage supply uses current source to establish reference

The circuit shown employs a FET and an op amp to achieve low output resistance, high supply rejection and a low temperature coefficient (TC). A 7.5-V avalanche diode is used only to force the circuit into the correct mode at switch-on, so the circuit is free of avalanche noise.

The FET, \( Q_1 \), is a low pinch-off p-channel device. It serves as a current source for reference current \( I_e \), which establishes a reference voltage across \( R_1 \). A variable resistor, \( R_\) can adjust the gate-source voltage of \( Q_1 \) to a region of its characteristic curve where its drain current doesn’t vary significantly with temperature. Over a limited temperature range, \( R_\) can be adjusted to compensate for the TC of both the op amp and the circuit resistors by operating the FET in a region where its current changes are in opposition.

The reference current typically is less than 1 mA, and doesn’t appreciably reduce the available output current. A common op amp, such as a 741 or a 101, can source and sink 3 mA as well as provide sufficient gain to attain a load coefficient of less than 10 \( \mu \)V/mA for the regulator circuit.

Because the FET is terminated between two constant-voltage points, the regulator’s voltage coefficient is less than 10 \( \mu \)V/V. Also, an over-all TC of less than 20 \( \mu \)V/°C can be achieved over the temperature range of 0 to 70 C.

With op amps that were selected at random, and not particularly for low noise, a noise voltage of only 20 to 30 \( \mu \)V rms was measured in a noise bandwidth of 10 Hz to 10 kHz.

A convenient alternative to the FET is the recently introduced Siliconix CR068 current-regulator diode. The diode passes 680 \( \mu \)A and features a typical TC of 0.02%/°C.

John A. Roberts, Senior Engineer, Computing Devices Co., P.O. Box 8508, Ottawa, Ontario, Canada K1G3M9.

A regulated voltage supply can be adjusted to a TC of less than 20 \( \mu \)V/°C over the range 0 to 70 C. The TC of the FET can be set with a resistor \( R_\) to compensate for the op-amp and resistor TCs over this limited temperature range.

IFD Winner of July 19, 1976

Paul Kranz, Products Manager, and John Seger, Associate Engineer, Dytron Inc., 241 Crescent St., Waltham, MA 02154. Their idea “A Simple Battery Charger for Gel Cells Detects Full Charge and Switches to Float” has been voted the Most Valuable of Issue Award.

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More efficient diode developed by Siemens

New double-drift Impatt diodes with outputs of 3 W at 7 GHz are expected to be applied where semiconductors hitherto have not been used—i.e., in radio relay systems. Developed by Siemens, West Germany, these diodes have relatively high efficiencies of 11% and result in high outputs. The diode's case contains four mesas, which are mounted on a silver heat sink that can handle thermal losses of up to 30 W. But only two of the four mesas are actually bonded to the heat sink, and these two are selected only after extensive performance tests on the multi-mesa configuration. The result of this approach, says Siemens, is a high-efficiency diode.

Fabricating a double-drift Impatt diode requires such advanced techniques as multilayer epitaxy and ion implantation. The diode's two drift regions are accurately matched to the resonant frequency. Electrons pass through an n-type region, while holes pass through a p-type region.

Further improvements, predicts Siemens, will lead eventually to 10-W devices and will displace traveling-wave tubes in many applications.

'Sideband diversity' cuts transmission-error rate

A 10^4 improvement in the data transmission error rate has been achieved with an experimental mobile radio system using "sideband diversity," a data-modulation method developed at Bath University, England.

The new method, which can be used for speech transmission as well, has been tested by placing three fixed transmitters about 15 miles apart. Vehicles equipped with the special receiving equipment (also developed at Bath) and traveling in areas of varied terrain have obtained signals with error rates of only 6.8 × 10^-2.

Sideband diversity can be operated with two or more transmitters. Identical signals are sent out from each transmitter, but the modulations on the transmitters are phase-shifted relative to each other. In the three-transmitter experimental system, the modulators are phase shifted 120° with respect to each other, but this angle is not critical.

At the receiver, an amplitude comparator looks for the strongest sideband and automatically selects the strongest part of the signal. This selection ensures that any interruption in the signal that might occur because of the terrain will not result in a total loss of signal at the receiver. At least one sideband of the signal will always get through to carry the transmitted information.

The results of the trials conducted so far have show that errors are almost random, with only slight variations caused by terrain. One advantage of the sideband-diversity method is that it overcomes the problem of stationary vehicles located in bad-reception areas. Error-correcting codes known to reduce the error rate considerably can do nothing in this situation.

A combination of error-correcting codes and sideband diversity transmissions might give the best possible results for data transmission, according to Professor Gashing, head of the Bath Electronics School.

Acoustic wave oscillator works at high frequency

An acoustic-wave oscillator developed by Thomson-CSF is said by the company to exhibit noise and short-term stability characteristics on a par with those of resonating bulk-crystal types—but without the latter's upper-frequency limitation.

The fundamental acoustic-wave oscillator operates from 100 to 800 MHz, and work is in progress to push the upper limit up to 2 GHz. Combining this oscillator with a frequency multiplier can produce signals of up to 10 GHz.

To provide acoustic-wave oscillation, an acoustic-wave delay line is connected in the feedback loop of an amplifier adjusted to yield a net loop gain greater than unity. Unlike a conventional, crystal-controlled oscillator, the acoustic, delay-line control element does not resonate. Its operating frequency and mode selection are determined by delay-line parameters, which provide design flexibility.

Long and short-term stabilities of 1 in 10^-3 and 1 in 10^-4 parts per year, respectively, have been demonstrated. The noise figure is -120 dB/Hz, with respect to the fundamental. Output power up to +20 dBm is possible as well as the ability to modulate frequency.
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4. **Long Life**
   10⁶ mechanical operations.

5. **Negligible Chattering**
   Lift-off card system and rebound absorbing structure minimizes contact bounce.

6. **Low Stable Contact Resistance**
   Bifurcated gold clad lift off contacts. Applicable to low level circuits.

---

**Sound advice for the alarm industry.**

You know better components make a better alarm system. So it pays to install the most reliable relays available today: Arrow-M NFE Amber Relays supported by our unique and advanced manufacturing techniques. They offer you:

**Reliability** — The secret is a unique automated modular assembly coupled with lift off bifurcated contacts and a rebound absorbing mechanism. Installed in a sensitive alarm, it can go unused for long periods of time and still work when needed.

**Sensitivity** — NFE Amber Relays use only half the power of ordinary relays.

**Automatic Wave Soldering** — NFE Amber Relays are plastic sealed with N₂ gas.

**High Packaging Density PC Board Mounting** — Flatpack NFE Amber Relays are only 0.425 inches high.

The proven dependability and sensitivity of Arrow-M Amber Relays is based on more than 50 years of meeting the advancing needs of modern technology. So for relays that make it easier to make a better alarm, rely on Arrow-M NFE Amber Relays.

**Relays for Advanced Technology**

For evaluation samples, or for more information on exact specifications, write or call your nearest Arrow-M office.

**Arrow-M Corporation**
250 Sheffield Street
Mountainside, N.J. 07092
(201) 232-4260

Western Office:
22010 S. Wilmington Ave.
Suites 300 & 301
Carson, Calif. 90745
(213) 775-3512

**Arrow-M**
Member of Matsushita Group
DPM building blocks make 93 different instruments


Putting together a measurement system is easier than ever with Digitec's new line of digit:!) panel meters. Building blocks let you construct over 93 different instruments and consist of 3-1/2 and 4-1/2-digit DPMs, compact adapter modules and a comparator block.

These three elements—plus a three-state logic BCD output—provide the basis for measurement of physical parameters, and for display of readings in convenient engineering units.

The adapter modules attach to the rear of the DPM and condition the input signal. All adapters are interchangeable with either of the basic DPMs. By changing the adapter, you can shift, say, from thermocouple temperature measurements to scaled-and-offset millivolt readings.

With the three-state logic BCD, or single-line enable, you can hook up any number of outputs in parallel on a common data bus. Then, by energizing a single TTL-compatible control line, you can call up coded output data from any instrument (see illustration). Thus cumbersome external switching of many BCD lines is avoided.

The comparator building block, an internal PC board, watches for alarm conditions, and it can monitor any number of points. Alarms are “sounded” by relay closure or by a logic-level output when a predetermined, programmable limit is exceeded.

Programming of the comparator is accomplished with jumpers or with external BCD switches. You can also tell the comparator to indicate the alarm momentarily or to lock-and-hold above or below a limit.

Performance specs of the Digitec DPMs include accuracies to 0.01% of reading (4-1/2-digit unit), 115/230-V-ac or 5-V-dc operation, and common-mode rejection of 129 dB (both DPMs). Tempo of the 4-1/2-digit model (the 2780) is 0.001% of full scale per °C. The 3-1/2-digit unit (the 2770) provides an automatic zero.

Prices of the basic DPMs run from $139 to $229, the adapter ranges from $79 to $170, and the comparator sells for $129 (2770) or $149 (2780). The single-line enable feature costs $60 in the 3-1/2-digit 2770 and $75 in the 4-1/2 2780.

Unit shows single events to ±100-ps resolution

Eldorado, 2495 Estand Way, Pleasant Hill, CA 94523. (415) 682-2100. $4850; 12 wks.

Model 797 time-interval meter is specifically designed for single-event measurement and provides an accuracy and resolution of ±100 ps throughout the measurement range of 0 to 999,999,999.9 ns. In addition to measuring the time interval between two separate pulses, the 797 measures the width of a single pulse or one period of a repetitive signal. The start and stop points can be independently controlled so that pulse parameter or waveform measurements can be made. In a programmable system, the 797 can be sequenced to measure rise time, pulse width, and period. BCD or IEEE Std 488-1975 (GPIB) and remote programming are available.

Chart recorder operates from 12-V power source


A single-channel chart recorder operates directly from a 12-V-dc power source. The recorder, Model 102 XLA, takes 6 W of power. It provides an accuracy of 0.5% of full scale and meets the frequency-response specifications of the American Heart Association. The 102 XLA uses no ink; it writes on thermal paper. The trace width is 50 mm. The recorder dimensions are 4 x 6 x 6.25 in.
Compact DPM aims at analog meter market

Analog Devices, Route 1 Industrial Park, P.O. Box 280, Norwood, MA 02062. (617) 329-4700. $33 (100s); 30 days.

The AD2026 is the first digital panel meter to integrate all analog and digital circuitry on one 1-FL LSI chip. The unit is a 3-digit, 5-V-powered device, featuring 0.5-in. LEDs and priced at $39 in 100-piece quantities. The AD2026 is packaged in a small 3.4 $X 2.0 $X 0.7-in. snap-in case requiring no mounting hardware. Weight is less than 2 oz. With just 14 components and a power draw of only 0.6 W, the unit is rated at more than 250,000 hours MTBF. Other features include 0.1% accuracy, full-scale range of -99 mV to 999 mV, bias current of 110 nA, balanced differential input and overvoltage protection of ±15 V dc. Gain tempo is 50 ppm/°C and zero tempo is 10 µV/°C.

CIRCLE NO. 323

4-terminal probes test PC boards

Electro Scientific Industries, 13900 N.W. Science Park Dr., Portland, OR 97229. (503) 641-4141. $95; stock to 60 days.

You can use these probes for making four-terminal resistance measurements on microcircuits. Small enough to probe a pad of 20 mils square, they are useful for checking PC board stripes as well as components. The probe tips are spring loaded into a pen-sized holder. They can be used for extremely low-ohm measurement at high accuracy because a true four-terminal technique, which eliminates lead resistance effects, is employed. Slivers on printed circuit boards, shorts in ICs and open conductor stripes under dual-in-line packages can be detected with these probes, when used with the company’s Model-1700 digital ohmmeter.

These probes are also useful for resistance measurement of physically large parts such as rods and cable couplings.

CIRCLE NO. 324

Logic analyzer accepts 16 channels

Biomation, 10411 Bubb Rd., Cupertino, CA 95014. (408) 255-9500. $5000; 30-60 days.

Model 1650-D, a 16-channel, 50-MHz logic analyzer, is functionally similar to the company’s 851-D eight-channel unit. The 1650-D can freeze the input signals in its 16 $X 512-bit memory. The unit then displays the stored data in a 16-line timing-diagram format on a CRT display or oscilloscope. Also offered is an accessory, the 116 face driver with TM-500 line timing-diagram format. When used with the company’s Model-1700 digital ohmmeter, these probes are also useful for resistance measurement of physically large parts such as rods and cable couplings.

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CIRCLE NO. 322
You'll like **Burr-Brown's one word price story... Down.**

You've always expected high quality from Burr-Brown. Now you can expect Burr-Brown to keep your costs down, too. Take a look at the prices of these high quality Burr-Brown units:

**ADC 80:** Lowest priced hybrid 12 bit A/D on the market. ADC 80 is complete with clock, comparator and reference, and is especially applicable in designs where space is crucial. With a conversion speed of 25 µsec, price is only $47.50 (in 100's).

**DAC 80:** 12 bit DAC's price cut by half. The DAC 80 is a truly self-contained D/A converter with guaranteed monotonicity. It includes internal reference source, output buffer amplifier, maximum non-linearity of ± ½ LSB, and a price of only $19.50 (in 100's).

**3626 Instrumentation Amp:** Modular performance at lower cost. The laser-trimmed 3626 family offers the performance you need. Input offset drift as low as 1 µV/°C at G = 1000, <2 µV/°C at G = 5, gain non-linearity is 0.01%. Prices start at $13.00 (in 100's).

**4127 Log Amp:** Low-cost solution to signal processing problems. 4127 is the first hybrid log amp to accept inputs of either polarity - up to 4 decades of voltage or 6 decades of current input. It functions as a logarithmic, log ratio, or antilog amplifier, and is only $26.00 (in 100's).

Five circuits - typical examples of Burr-Brown's commitment to cost savings. Over the past year, Burr-Brown has cut prices on a substantial number of products, some by more than 50%.

To find out more on how Burr-Brown can help you meet those crucial cost vs. performance specifications, write or call: Burr-Brown, International Airport Industrial Park, Tucson, Arizona 85734. (602) 294-1431.

**Burr-Brown**

**Still at the top, except in price**

CIRCLE NUMBER 92

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Electronics Design 24, November 22, 1976
This new General Catalog is our latest family portrait. In the past twenty-five years (1976 is our Silver Anniversary year) it has grown from a handful of items to almost 500 products for the electronics industry.

Our catalog has grown to 76 pages for 1976, and we are introducing 65 new items this year. It describes and illustrates every member of our family. You're bound to find the solution to your testing problem with one or more of these quality products.

For your free copy, circle the reader service number listed below, or write:

**Electronic Design 24, November 22, 1976**
Here is a designer's dream come true. Minimum form with maximum function.

It's PPG's electronic glass. It lets you combine the sleek, simple elegance of glass and the dazzling magic of solid-state technology.

Which means you can literally change the faces of appliances, timepieces, visual displays, and instrumentation of every description.

The secret is the permanent conductive metallic-oxide coating on the glass.

It can be made to trigger functions at the mere touch of a finger. Like timing a roast, choosing a station, starting the wash, or even figuring the square root of 34.

In short, if it can be done electronically, it can probably be done a little better with electronic glass.

And, since the coating can be applied to form letters, numbers, or any visual display imaginable, there's almost no end to what you can do.

Digital clocks, wristwatches, speedometers, odometers, oscilloscopes, and radar screens are just a few of the obvious possibilities.

As for its reliability, there's really nothing to go wrong. No moving parts. No knobs, dials, switches, buttons—just glass.

It's here. It's now. It's ready.

All it needs is you, and all you need is the vision to use it.

So test your vision. Send the coupon today.

PPG: a Concern for the Future

PPG Industries, Inc.
Industrial Glass Products
One Gateway Center
Pittsburgh, Pa 15222

I want to test my vision.
Send me more information about PPG's exciting electronic glass.

Name: ___________________________
Company: _______________________
Address: _________________________
City: ____________________________
State: __________________ Zip: ______

CIRCLE NUMBER 94
Why Do More Top Designers Insist On Working With Harris Generic PROMs?

The compatibility and depth of our Generic PROM family simplifies selection, application, and production. But that's only the beginning. Here are a few specific reasons for choosing Harris.

- Identical programming specifications means that one programmer programs the entire family.
- Single pulse one millisecond per bit programming achieves fast programming and superior reliability.
- Industry's highest programming yield increases production efficiency, regardless of PROM size.
- Access times are guaranteed over full temperature and voltage ranges and any random addressing sequence.
- Harris is the only JAN-38510 QPL-1 approved PROM supplier.
- Proven Nicrome fuse design and Schottky technology.
- Complete family availability from prototype quantities to production volumes.

Now See How The 1Kx4 PROM Can Improve Your System.

- High-density 16 or 18 pin packages greatly reduce board area.
- HM-7644 (16 pin, no enable) provides direct upgrade for systems using 1K or 2K PROMs and having less than 1024 words.
- HM-7642/43 (18 pin, 2 enables) extends high density packaging to large memory configurations.
- Low power per bit: (Icc < 140 mA or < 180 μW/bit).

For a quick look at our PROM family check the chart. And for complete details call your nearby sales location or write to Harris Semiconductor, P.O. Box 883, Melbourne, Florida 32901.

<table>
<thead>
<tr>
<th>Device #</th>
<th>No. of Bits</th>
<th>Organization</th>
<th>No. of Pins</th>
<th>Max. Access Time*</th>
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<td>256</td>
<td>32x8</td>
<td>16</td>
<td>40ns 50ns</td>
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<td>256</td>
<td>32x8</td>
<td>16</td>
<td>40ns 50ns</td>
</tr>
<tr>
<td>(three state)</td>
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<td></td>
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<tr>
<td>HM-7610</td>
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<td>256x4</td>
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<td>60ns 75ns</td>
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<td>HM-7611</td>
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<td>16</td>
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<td>70ns 85ns</td>
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<td>2048</td>
<td>512x4</td>
<td>16</td>
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<td>1024x4</td>
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<td>HM-7644</td>
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<td>70ns 85ns</td>
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<tr>
<td>(active pullup)</td>
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</tbody>
</table>

*Access time guaranteed over full temperature and voltage range.
Industrial (TA = 0°C to 70°C, VCC ± 5%)
Military (TA = -55°C to 125°C, VCC ± 10%)

Proven PROM Capability

HARRIS SEMICONDUCTOR
A DIVISION OF HARRIS CORPORATION

CIRCLE NUMBER 95
INSTRUMENTATION

Logic clip eases debugging of logic cards

Micro, 10888 N. 19th Ave., Phoenix, AZ 85021. (602) 997-5931. $40,000 to $60,000; 2-4 wk.

The Magiclips system, with guided clip/probe, enables production workers to troubleshoot logic boards with a minimum of time and training. To locate a fault, the operator simply follows simple instructions which automatically appear on the CRT. The system rapidly detects faults to chip, node or run level. Magiclips is an option of the 6500 test/programming station, a modular turnkey system, which enables users to generate board-test programs in-house and perform comprehensive testing and troubleshooting. Optional peripherals include high speed printer, console with dual floppy discs, high speed paper tape punch/reader, card reader, CRT and keyboard. Magiclips guided clip/probe and 500-series test head.

Lightweight scope features multiplication

Philips Test & Measuring Instruments, 400 Crossways Park Dr., Woodbury, NY 11797. (516) 921-8880. $3395.

A built-in 40-MHz multiplier and comprehensive storage facilities are features of a new, lightweight, 50-MHz scope. The PM-3243 has two channels with 5-mV sensitivities and both the product and one of the original signals can be displayed simultaneously. Variable persistence and variable storage allow the study of single-shot events. The use of a direct conversion power supply allows operation from almost any voltage or frequency, including dc, without switching. Any ac supply between 90 and 264 V from 46 to 440 Hz or any dc supply between 100 and 200 V suffice. Power consumption is 39 W.

Ultracompact DMM fits in attache case

John Fluke Manufacturing Co., P.O. Box 43210, Mountlake Terrace, WA 98043. (206) 774-2211. $250; 7 wks.

Model 8030A DMM is designed for service and maintenance applications and is said to be the first 3-1/2-digit instrument to offer features such as true rms ac voltage and current measurements and diode testing. The compact design lets the unit be easily carried in a tool kit or attache case. The diode measurement feature permits the forward drop (in millivolts) across a diode or transistor to be checked, with the semiconductor junction biased at 1 mA. Dc accuracy is ±0.1% of reading +1 digit.
one of the world's largest and most technically competent manufacturers of quartz crystal oscillators, comes this new Primary Frequency Standard. Now, a new source of precision time and frequency generation and measurement systems plus a new standard of reliability and operating simplicity. Most competitively priced.

It is complete — with 110/220 VAC and 24 VDC Power Supplies, a 5-hour Internal Standby Battery, Monitoring and Control Devices — in a 19" rack with 1, 5 and 10 MHz outputs on front and rear.

Heart of this self-contained Primary Standard is the compact cesium beam tube developed by Frequency & Time Systems to permit the exceptional performance-to-size ratio of the Model 3200. ALSO NEW— the Oscilloquartz low-cost Model 3000 Cesium Beam Frequency Source in ½ ATR Rack Size.

Complete engineering and performance specifications available on Model 3200 Cesium Frequency Standard and Model 2200 Quartz Frequency Standard and Clock.

Write: 182 Conant St., Danvers, MA 01923 or call (617) 777-1255

TELEX 94-0518

INSTRUMENTATION

Digital unit reads pressure and temp

Prime Manufacturing, 7730 S. 6th St., Oak Creek, WI 53154. (414) 764-1400. $400 to $700; 4-7 wk.

The Model 769 digital gauge accurately measures both pressure and temperature from a single self-contained unit. The gauge measures absolute pressures up to 999 lb/in², with a ±0.5% variation over the entire range. And it measures temperatures up to 999 F with variations of ±0.1% over the range. The unit contains four probes for any pressure and temperature combination. Buttons on the display-front select one of the four sensors being monitored. Probes are easily installed and can be equipped for remote use, up to 200 ft, without loss of accuracy. Probes are available for almost any media. The unit has a zeroing button to check the system's calibration. It has an easily read display which accommodates rapid changes in pressure or temperature.

CIRCLE NO. 332

4-1/2-digit DMM ranges automatically

John Fluke, P.O. Box 43210, Mountlake Terrace, WA 98043. (206) 774-2211.

The 8040 is an ultracompact 20,000-count multimeter with five measurement facilities, autoranging and autozero. The design enables the unit to be carried conveniently in an attache case or as part of a service kit. Measurement capabilities include dc voltages from 200 mV fs to 1100 V fs, to an accuracy of ±0.05% of reading +2 digits; and ac voltages from 200 mV fs to 750 V fs using a true-rms conversion technique, to an accuracy of 0.5% of reading +10 digits. True rms is also used on ac-current ranges.

CIRCLE NO. 333
Take a plane - military, commercial, or private. Chances are 9 out of 10 you'll find Syntronic Deflection Yokes and Focus Coils in critical cathode ray tube display equipment; weather radar, navigation, weapons systems, landing, monitoring, communicating. The U.S. Navy's/Lockheed S3A anti-submarine plane uses 14 Syntronic components in 7 critical displays.

Other aircraft display applications include the B52 Retrofit, F4 (D&E), F5E, A6, A7, F111, A10A, S3A, F14, F15, F16, AWACS, MCRA, Mirage, Viggen, 707, 727, 737, 747, DC-8, DC-9, DC-10, L1011 and many private aircraft. Call or write Syntronic Instruments, Inc. (312) 543-6444. Ask for Syntronic's Yoke Selection Guide to high-flying, high-performance yokes.
IC tester checks DIPs at 1.3-MHz rate

Biomation, 10411 Bubb Rd., Cupertino, CA 95014. (408) 255-9500. $4500; 60 days.

Model 2400 benchtop digital IC tester is designed for those who use small quantities of many different digital IC types. The 2400 is primarily a functional tester with a test rate of up to 1.3 MHz. It is completely operator programmable and will handle a wide variety of ICs with up to 24 pins, including CMOS, NMOS, ECL and all TTL families, plus open-collector and three-state output devices. The price represents the cost of a 16-pin unit including a programm library for over 1000 different devices. Model 2400 also measures some parametric values.

CIRCLE NO. 334

Counter line features 10 new models

Philips Test and Measuring Instruments, 400 Crossways Park Dr., Woodbury, NY 11797. (516) 921-8880. PM6661, $325; PM6664, $625.

A bunch of brand new timer/counters, universal counters and automatic frequency counters mark the company's attempt to capture a large chunk of the market for frequency/time-measuring products. Included are three timer counters, covering 80, 520 and 1000 MHz (PM6620 series), four universal counters (PM6610) and two automatic frequency counters, with an on-off switch as the only control. Both the 80-MHz PM6661 and the 520-MHz PM6664 offer automatic triggering, noise suppression, range selection and leading-zero blanking. The timer/counters feature nine digits, 20-mV sensitivity and resolution as low as 1 ns.

CIRCLE NO. 335

DMM uses LCDs, reads temperature, too


The Beta is a portable, battery-operated 3-1/2-digit multimeter using a large, liquid-crystal display and a single CMOS IC chip for all analog and digital functions. Among the Beta's 29 ranges is a 10 A ac and dc current range via a separate input, plus temperature-measurement capability with direct reading between -20 and 120 C. Beta operates for over 300 h from four C cells.

CIRCLE NO. 336

New from Standard Grigsby

P/rel

the programmable rotary encoded logic switch everyone will be talking about...

... because no other rotary switch has as much versatility with as low a cost as Standard Grigsby's P/rel switch!

The economy is twofold. This switch not only lends itself to full automation, but installed costs are lower by the use of our printed circuit terminals (solder terminals are also available).

A specially processed printed circuit disc is fully programmable to the truth table of any code. We provide 100% program disc inspection to customer specifications. Up to 60 detent positions are available with our new double ball Dual Flex detent. And, the use of concentric shafts allows up to 120 detent positions from a single switch!

Everyone will be talking about P/rel ... so will you!

Send for your free "Yes" button and literature.

standard grigsby, inc.
920 Rathbone Avenue, Aurora, Illinois 60507, Phone (312) 897-8417

CIRCLE NUMBER 98
Some people just can't leave well enough alone.

Last March, while the other guys were making promises, Advanced Micro Devices was making Am9130's and Am9140's—the first family of 4K static RAM's.

Terrific. Everyone loved them. But were we satisfied? Did we stop there? No.

Advanced Micro Devices announces the 1Kx4/4Kx1 Am91L30/L40, low-power versions of our Am9130/40.

These new circuits provide access times down to 250 nanoseconds with power dissipation of only 367mW. That's half the power of the original. (And that's the same power as the industry standard 1K static RAM. You're getting four times the memory for the same power. Wow!)

There's more. These beauties do everything on a 5-volt power supply. The logic levels are identical to TTL. You get all the features of the original, including full military temperature range availability and, as always, MIL-STD-883 for free. Plus: a freshly minted set of application notes and data sheets awaiting your call, wire or letter.

Some people just can't leave well enough alone.
**New Power Transformers**

**For +5V and ±15V**

**Triple Output**

**Five Plug-ins**

**Five With Standard Leads**

Triad has five new plug-ins and five units in open construction with leads for logic and op-amp power supplies—either regulated or unregulated. Dual secondaries of 9VCT and 24VCT, or 15VCT and 32VCT. Primaries, 115V, 50/500 Hz. Outputs: 1.5 W, 4.5 W, 7.5 W in plug-ins; 4.7 W, 20.3 W, 62 W, 92 W and 122 W in lead types. Specifically designed for “in-house” power supply construction where density packaging and flexibility are important. So call your distributor today for prices, delivery, technical information and Triad quality.

---

**INSTRUMENTATION**

**UV outshines visible for oscillographs**

*EMI Technology, 20 Old Ridgebury Rd., Danbury, CT 06810. (203) 774-3500. From $2000; stock to 30 days.*

Unlike conventional light-beam designs, which sacrifice deflection to achieve wide bandwidth, series-SE6150 multichannel ultra-violet beam oscillographs feature writing speeds of 50,000 in/s, bandwidths of 0 to 10 kHz and deflections of more than 1.2 in. Each instrument in this series offers up to six recording channels, with access to galvanometers either directly or via built-in modular adjustable-gain drive-amplifiers which are calibrated directly in V/cm. Galvanometer modules (magnet blocks) are provided for up to 12 direct channels with 500-V-de insulation, or up to six channels with 5 kV dc insulation. Modules are thermostatically stabilized at 45 ±3°C for stability of sensitivity. Each instrument has auxiliary recording capabilities: to trace its own grids and timing lines over the full 6-in. width of the chart; to control trace and grid intensities; and to add reference markers and event markers. Timing intervals are selectable by panel push-buttons at 0.01, 0.1, 1, 10 and 100 s or may be controlled by external trigger. Twelve servo-regulated chart speeds from 0.008 to 39.37 in/s are selectable by panel push-buttons. Chart-drive linearity is ±3%, in both automatic and continuous modes. The channel-amplifier panel-controls offer a selection of 10 attenuation steps, for sensitivities from 0.008 to 8 in/V, plus a 3:1 vernier adjustment. Input impedance is 10 MΩ up to 1 cm/V and 1 MΩ from 2 to 20 cm/V. The system frequency response is dc to 10 kHz (±1 dB); noise and crosstalk are less than 0.2% of full-scale deflection. The instrument measures 17 x 5 x 18.5 in. and weighs 31 lb.

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**CIRCLE NO. 337**

*Electronic Design 24, November 22, 1976*
WB-713 SPECIFICATIONS

- Frequency Range - Band I: 1 to 500 MHz
  Band II: 450 to 960 MHz
- Sweep Width - Bands I and II: 0.1 to 500 MHz
- Output: +10 dBm
- Flatness: ± 0.25 dB
- Distortion - Band I: -35 dB
  Band II: -30 dB
- Residual FM: Less than 10 kHz
- Sweep Rate: 0.01 to 100 Hz variable
- Linearity: 1%
- Markers: Provisions for up to 7 plug-in harmonic or single frequency markers.
  Marker Tilt Control
  Marker Clip Control
  Marker Width Control from 20 kHz to 300 kHz
- Weight: 15 lbs.
- Size: 9" x 4 3/16" x 12 5/8"

Texscan has sweep generators covering from Audio to 2350 MHz. Please contact your local Texscan representative for a demonstration.

Texscan Corporation 2446 North Shadeland Ave. Indianapolis, Indiana 46219 (317) 357-8781
INSTRUMENTATION

Pulse width and repetition rate are independently adjustable. WR549A operates within 5% (at the calibration points) of the dial settings over the entire range and maintains a pulse width of 100 ns to 0.1 s over an unlimited cycle. Rise and fall time is less than 20 ns on all ranges. Output is adjustable for both TTL and CMOS, covering a range of 0 to 15 V pk-pk. Impedance is selectable at 50 or 600 Ω.

CIRCLE NO. 338

Low-cost pulser offers versatile operation

Viz Test Instruments Group, 335 E. Price St., Philadelphia, PA 19144. (215) 844-2626. $119; stock.

Model WR549A pulse generator is continuously variable over a range of 5 Hz to 5 MHz, positive, negative, or pos/neg square wave.

Amplifier delivers 75 W from dc to 100 kHz


Model 7500 direct-coupled dc-to-1-MHz amplifier is said to be the first such amplifier to offer up to 75 W of continuous power (150 W at dc) and 125 V rms over a bandwidth from dc to 100 kHz. Output is 10 W at 1 MHz. Frequency response is flat to within ±0.1 dB over most of the range. Total harmonic distortion at full power output is less than 0.05% from dc to 20 kHz. Voltage gain is noninverting, and can be selected for either fixed gains of 20 dB (X10) or 40 dB (X100). Gain is continuously adjustable from zero to 40 dB.

CIRCLE NO. 339

Unit checks your contact's chatter

Associated Testing Labs, Northwest Industrial Park, Burlington, MA 01803. (617) 272-9050. See text.

The Contact Monitor is a solid state, chatter checker capable of detecting openings between a set of normally closed contacts, or closure between a set of normally open contacts. The unit detects contact chatter in electrical and electronic components having movable electrical contacts, such as relays, switches, circuit breakers, etc., where it is required that the contacts do not open or close momentarily, for longer than a specified time duration under environmental conditions, such as vibration, shock or acceleration.

Model NCNO 4-5, the four-channel device, meets the requirements of MIL-STD-202D, method 310, paragraph 2.1.2., test conditions A, B, C, D, and E. For calibration, an oscilloscope with calibrated time base from 1 µs to 5 ms/cm and a dc-VTVM are needed. The instrument measures 5.25 x 8.3 x 13.25 in. It has a detection accuracy of ±3% and a detection ratio (normal time to detection time) of 10:1. Price of the four-channel unit is $700 and a six-channel model is available for $980.

CIRCLE NO. 340

5½ DIGIT
ACCURACY.
4½ DIGIT
PRICE.

The 4600 is our brand new 4½ digit multimeter. It gives you the accuracy and resolution of typical 5½ digit multimeters. At half the cost.

And the 4600 stays accurate longer than other DVM's. DC accuracy stays within 0.01% ± one digit for six months at a time. We guarantee it.

80dB normal mode noise rejection produces a 10,000:1 reduction of excess noise. A full decade better than the 1,000:1 reduction of comparable instruments.

Loading errors are virtually eliminated by the 4600's 10,000MΩ input impedance on the two lowest DC voltage ranges.

There's a lot more. Send for a free catalog on our new 4½ digit 4600 multimeter. And find out how to get 5½ digit accuracy without paying for it.

Dana Laboratories, Inc., 2401 Campus Drive, Irvine, California 92715. 714/833-1234.

DANA

Others measure by us.

"NOW AVAILABLE THROUGH ELECTRO RENT"

FOR PRODUCT DEMONSTRATION
CIRCLE # 102

FOR LITERATURE ONLY
CIRCLE # 163

CIRCLE NO. 340

ELECTRONIC DESIGN 24, November 22, 1976
Now you can trade in your SSI and MSI circuits for all these custom I²L “SWAP” chip advantages!

Now with “SWAP” – Stewart Warner Array Programming – you can have all these custom chip benefits without paying the usual custom chip penalties. No large tooling costs and huge entry fees. No gigantic production order requirements. No long waits for deliveries. For as low as $1800, you have delivery of your first custom I²L “SWAP” prototypes in four weeks. “SWAP” is the major price breakthrough in custom logic circuits that makes it easy for you to take that first step. To climb aboard the bandwagon with your buddies in the industry, all you need is $25. That buys you your new SWAP Kit including the Design Manual, vellum work sheets, and 15 sample I²L devices illustrating some of the functional blocks that can be used in a SWAP design. Send for yours!

Okay, here’s my $25.00 (or P.O. No. ________). Rush me my I²L SWAP Design Kit.

I need more information, please have a representative call me.

Tell me about your standard off-the-shelf DTL, TTL, and CMOS circuits. (We have these in stock.)
If low cost and high performance are criteria...our new 82000 Series permanent magnet steppers are the answer.

Here's a new permanent magnet stepper motor line created to meet the design needs of analytical instrumentation and computer peripherals. Applications include tape drives, printer and chart drives and optical disc drives. Both 5 volt and 12 volt models are available.

All utilize 4-phase stators and permanent magnet rotors. Most have 24-pole rotor construction. As a result, they offer excellent pull-in rates and good stepping accuracy. Another advantage is low temperature rise...over 50% lower than comparable variable reluctance stepper motors operating on a similar duty cycle. Gear boxes can be furnished to meet varying torque and speed requirements.

Write for information today!

Available pull-in torques from .750 oz-in. to 7.50 oz-in.
Available stepping rates from 210 steps/sec to 440 steps/sec.

Our 4-page Permanent Magnet Logic Stepper Motor catalog provides all basic details including performance data and charts, dimensional drawings, as well as electronic drive information. Send for a copy.

COMPONENTS

Small thumbwheel switch features J-pin terminals


The T50J-01M is the smallest thumbwheel switch on the market today with 1/2-in. J-shaped pin terminations, according to Cherry. This makes the thumbwheel readily adaptable for both motherboard and wire-wrapping applications. The J-pins are made of brass with a bright tin finish. The switch is matte finished, has a 10-position decimal thumbwheel with in-line readout, and is modular constructed to allow gauging large numbers of switches. A 40-switch assembly uses a panel opening only 3/4-in. high and less than 13-in. wide.

CIRCLE NO. 341

Thick-film pots now range to 100 MΩ

TRW Inc., 401 N. Broad St., Philadelphia, PA 19108. (215) 922-8900. $0.42 (10,000 up); 2 to 4 wks.

A high-voltage thick-film potentiometer with previously unavailable resistance and stability characteristics now has a resistance range of 1 to 100 MΩ. It also features a shield to minimize dust accumulation. Temperature coefficient is a low ±400 ppm. Snap-in installation is standard, but mounting with a self-threading nut is also possible. For added flexibility, the control will accept different types of shafts. Over-all dimensions of the unit are 1-in. wide, 1.277-in. deep and 1.06-in. high.

CIRCLE NO. 342
TCX...the new aluminum capacitors with the super electrolyte.

TCX'tra! For a lot of extra pluses at extra-competitive prices.

Our new electrolyte system is the key. It provides the properties that make TCX capacitors ideal for even the most demanding commercial duty — such as high frequency, power supply, EDP applications.

Great stability, for instance, over a very broad temperature range up to 105°C. Which is about 20° higher than with almost every other capacitor of this type.

Along with low leakage, high ripple current, good volumetric efficiency. And a higher voltage/MFD range... 3 to 100 V, 10 to 22,000 MFD.

TCX'tra! Read all about it in our TCX literature. Just ask your Mallory representative.

MALLORY CAPACITOR COMPANY
a division of P. R. MALLORY & CO. INC.
Box 372, Indianapolis, Indiana 46220; Telephone: 317-636-5353
Switches and indicators receive seismic approval

Stacoswitch Inc., 1139 Baker St., Costa Mesa, CA 92626. (714) 549-1616. $8.95 to $30 per channel; 4 to 8 wks.

Stacoswitch switches and indicators are now seismic qualified to requirements of IEEE Standard 344-1975 and TVA 2200 appendix “C” for use in nuclear-fueled power-generating plants. One-to-four lighted status-message displays per control channel and one-to-one-hundred channels per control unit are available as standard assemblies. Up to 4PDT circuit switching with momentary, maintained or magnetic-latching actions for each control channel provides wide control versatility.

Projected LED light brightens PB switches


The projection of strong LED rays through a big indicator window gives the AML series lighted pushbuttons a bright look. The new design makes the LED easier to see in ambient light and visible from many angles denied most LED indicators, according to the manufacturer. A funnel-shaped reflector at the base of the diode helps beam red, yellow or green lights to the display surface of the pushbutton/indicator. Rated for 5, 10 or 15 V dc, the units have an internal resistor to maintain current at a nominal 20 mA. The switches are available with momentary or two-level alternate actions, and in one and two-pole form-C arrangements.

Popular potentiometer now has slip clutch

Allen-Bradley, 1201 S. Second St., Milwaukee, WI 53204. (414) 671-2000. $1.50 (1000 qty); 6 to 8 wks.

The type EJ potentiometer, a million-cycle rotational-life component, widely used in electronic games now is offered with an optional slip-clutch. The clutch prevents internal damage to the pot or the external knob if the shaft is turned with excessive force. Clutch action allows the shaft to be rotated beyond the stops, and then resume normal electrical operation when the rotating is reversed.
ChipStrates™ cost up to 40% less than other power SCRs and Triacs.

And that's only the beginning.

ChipStrates are glassivated power SCR or Triac chips mounted on solderable ceramic substrates. Since they eliminate the need for expensive metal packages, they cost up to 40% less than other power SCRs or Triacs.

For example, our 55A, 400V, ChipStrate goes for just $3.80 in quantities of 5,000. The electrically equivalent press fit Triac will run you $5.00 in the same quantity.

But that's not all.

ChipStrates are available in ratings from 3 to 55A and up to 800V and come in a rugged, electrically insulated package.

Their exceptionally good form factor will simplify the packaging of your system.

And their reliability is unmatched.

ChipStrate. The new concept in SCRs and Triacs that gives you more. And costs you less.

For the full story, just call or write: Carl Uretsky, Unitrode Corporation, 580 Pleasant St., Watertown, MA 02172. 617-926-0404.
dependability you can afford

SWITCHES Military or industrial/commercial single lamp switches built to exacting specifications for dependability and long service life. Choice of circuit control contact arrangement and solder or new PC terminations.

PUSHBUTTONS All sizes, styles, colors, and legend styles including new photographic film legends with visible or hidden messages. Color matched for visual recognition and operator convenience.

LOW COST Check the bottom line and you'll find Stacoswitch's low purchase price combined with quick and easy installation and maintenance make these your best buy in single lamp pushbutton switches. Write today for General Catalog giving complete description on single lamp and 4-lamp switches and indicators. When you think switch... think Stacoswitch.

PUSHBUTTONS All sizes, styles, colors, and legend styles including new photographic film legends with visible or hidden messages. Color matched for visual recognition and operator convenience.

LOW COST Check the bottom line and you'll find Stacoswitch's low purchase price combined with quick and easy installation and maintenance make these your best buy in single lamp pushbutton switches. Write today for General Catalog giving complete description on single lamp and 4-lamp switches and indicators. When you think switch... think Stacoswitch.

The time you save may be your own.

Used to be you'd get a circuit idea, lay out a pc board, print it, solder everything together, troubleshoot, change your layout, try a new board, and spend absolutely too much time breadboarding. Now A P ACE All Circuit Evaluators let you breadboard in a fraction of the time. Make your changes immediately. Keep full layout on your components. Avoid the heat damage possible with repeated soldering and desoldering. Have a pattern for your board—if you need a board—sitting in front of you. In about as long as it takes to sketch a schematic. Get cooking with ACE. ACE. The All Circuit Evaluator from A P Products.

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<td>10-1/4x4-3/4</td>
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Ohio and California Residents Add Sales Tax

For quick phone service, call the A P distributor nearest you:

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<tr>
<th>A P PRODUCTS INCORPORATED</th>
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<tr>
<td>Box 115-F</td>
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<tr>
<td>Painesville, OH 44077</td>
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<tr>
<td>(216) 354-2101</td>
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<td>TWX: 810-425-2250</td>
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Our Distributor List is growing daily. If none in your area call toll Free 800-321-9668.

Components

New pots designed for electronic games


A new potentiometer designed for the electronic-game market (Ultralife Model 2) has excellent life and low-noise characteristics. Mechanical life is in excess of 250,000 cycles. Its control-spring design results in an initial contact-resistance variation of 0.5%. End-of-life contact-resistance variation (CV) is less than 1.5% of total resistance. The following additional features are provided: resistance range from 5000 Ω to 5 MΩ; linear taper; a power rating of 1/2 W at 40 C; PC or solder-lug terminals; and a bushing for twist-tab mounting.

Precision-pot element is conductive plastic

Maury Instrument Corp., 4555 W. 60th St., Chicago, IL 60629. (312) 581-4555. $21 (100 up).

The 112-P19 is a low-cost, solid-molded raised track, conductive-plastic potentiometer. It offers infinite resolution, long life and extremely rugged vibration characteristics. The unit features a high-pressure wiper-assembly design and high-quality wiper-contact material to obtain rotational life under extreme environment that exceeds conventional film devices. Gold-plated terminals, beryllium-copper wiper spring as well as a stainless-steel shaft and ball bearings are standard. Size is 1-1/8-in. dia. with a 1/8-in. dia. shaft. Resistance range is 500 Ω to 100 kΩ, standard linearity ±0.5% and life is in excess of 100-million revolutions.
Panel controls set X-Y position


Cambi-Grid is a two-axis positioning control for use where all movements along either axis are some multiple of a fixed increment such as 0.1 in. Applications include drilling, insertion, inspection, punching, packaging, etc. The system is programmed directly on its own control panel as opposed to paper-tape programmed systems. Features include nonvolatile program memory, programmable tool function, manual and automatic operation modes, adjustable control of positioning-motor speeds. The rack mountable unit has a G4 instruction memory, which allows the programming of up to 960 X-Y coordinates. A line of compatible stepping motor drivers is available.

CIRCLE NO. 348

Pressure transducer offered in new packages

National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. (408) 737-5000. $79 (25 up); stock.

The LX1700 series pressure transducers, in new package designs, are designated PX7-1 in zinc packages and PX7N-1 and PX7D-1 in nylon packages. They feature internal captive O-rings that eliminate leakage. The devices are fully signal conditioned and temperature compensated (operating range 0 to 85°C). And they can measure pressure ranges from ±5 psi to 0 to 300 psi. In addition a flexible cable is key locked so it can't be pulled out of the package. They come with five-pin connectors for easy insertion into a test socket or PC board.

CIRCLE NO. 349

Now, a single integrated circuit, our TAD-32 (Tapped Analog Delay), can provide filtering with passband-to-stopband ratios of 40 DB or more per device. Simple variation of the clock sampling rates over 5 decades will accordingly shift a given filter characteristic. Transversal or recursive filters can be constructed with over 60DB dynamic range and linear phase. Tapped delays up to several hundred milliseconds are possible.

Discrete time analog signal processing using charge transfer devices is a reality at RETICON.

The TAD-32 is just one device in this growing family.

We don't just talk about them, we make them.

THIS DIP DOES IT ALL.

TAPPED DELAYS MATCHED FILTERS CORRELATION CONVOLUTION

RETICON

910 Benicia Avenue, Sunnyvale, California 94086
PHONE: (408) 738-4266 TWX: 910-339-9343
CIRCLE NUMBER 111
20-A rectifiers offer 35-ns turn-off time

NAE, Inc. Semiconductors, 69 Bennett St., Lynn, MA 01905. (617) 598-4800. $7.80 to $16.25 (1-99); stock.

A new series of superfast 20-A rectifiers for dc applications—inverters, converters, choppers and switching regulators—handles up to 200 V. Designated 1N5812 through 1N5816 with voltage ratings from 50 to 150 V in 25-V increments, these new 35-ns units have a low forward drop of 0.9 V at 10 A, and they are housed in the JEDEC DO-4 packages. The 200-V version, designated NSR-7025, offers the same recovery features as the lower-voltage units.

CIRCLE NO. 350

Is there a recorder just for spectrum analyzers?

The new 19" rack-mounting SPECTRUM ANALYSIS RECORDER from Raytheon. It's the first dry paper line scanning recorder specifically developed for direct plug-in operation with commercially available spectrum analyzers.

Any new or existing spectrum analyzer equipped with the SAR-097 will have a lot more going for it. Like infinitely variable 100:1 speed range—5 sec/scan to 50 millisec/scan...stylus position encoder...automatic recorder synchronization...computer/analizer compatibility...high resolution and dynamic range...all-electronic drive. And more.

If you design and build—or buy and use—spectrum analyzers, you don't have to settle for multi-purpose recorders any more. The SAR-097 is here. For full details write the Marketing Manager, Raytheon Company, Ocean Systems Center, Portsmouth, Rhode Island, 02871. U.S.A. (401) 847-8000.

CIRCLE NUMBER 112

LED numerical displays need 1/3 usual power


LED seven-segment numerical displays, 0.175-in. high, require only 2 mA per segment, about 1/3 the power required by presently available displays. These HP 5082-7265, 7275, 7285 and 7295 indicators are available in five and 15-digit packages. Models 5082-7265 and 7275 five and 15-digit clusters, respectively, have a center decimal point. Models 5082-7285 and 7295, also five and 15-digit clusters, have a right decimal point. Devices may be mounted with edge connectors or with soldered wires.

CIRCLE NO. 354

700-V transistors feature 0.7 µs fall time

International Rectifier, 233 Kansas St., El Segundo, CA 90245. (213) 322-3331. $3.78 to $4.79 (100-999); stock.

A new series of power transistors, 2N6573 through 2N6575, with very fast switching times and ratings to 700 V at 15 A, features fall times as fast as 0.7 µs. Hard-glass passivation of the chips provides high-temperature stability and long operating life for application in TV deflection circuits, switching regulators and high-voltage switching power supplies.

CIRCLE NO. 355
The best buy ever in an Autoranging Portable DMM

Look at what you get from Weston® for only $195.

Specially developed, high reliability LCD display

Automatic polarity

LSI microcircuits

Five standard measurement functions

26 ranges, automatic zero

Low power transistor batteries

Small size, light weight

0.35% Accuracy

Autoranging

Portable or bench

Overrange and low battery indicators

Special 10 amp current range

Hold input retains readings indefinitely

Rugged high impact case

Performance, quality, reliability and price. The Weston Model 6000 is a total value package and the best buy ever in a portable digital multimeter. It offers the simplicity and speed of automatic ranging at 0.35% accuracy. Superior performance at minimum cost through use of custom LSI microcircuitry and laser trimmed resistor networks. Specially developed LCD display for long life and high legibility, even in bright sunlight. Powered by two inexpensive, easily available 9V transistor batteries with more than 200 hours of operating life. Weston has packed the Model 6000 with every type of performance and convenience feature... at an unbeatable price.

To get the full details, contact any Weston distributor. Or, write direct to Weston.

Canada: 1480 Dundas Highway, Mississauga, Ontario.
Europe: Ingolstädter Str. 67a 8 Munchen 46, W. Germany.

CIRCLE NUMBER 113
DISCRETE SEMICONDUCTORS

Fast diode chips rated to 100 A

Solid State Devices Inc., 14830 Valley View Ave., La Mirada, CA 90638. (213) 921-8660. $0.25 to $5 (100 up); stock.

A new line of 1-to-100-A ultra-fast-recovery diode chips allows hybrid manufacturers to obtain circuit performance previously obtainable only with packaged devices, according to Solid State Devices. The HSR and HVE chip families are processed with Epion ion-implantation techniques to give 9-to-90-ns reverse-recovery times—about 10 times faster than conventional devices. The HSR Series are 20-to-150-V-peak reverse-voltage chips with 1 through 100-A forward-current capabilities. Maximum reverse-recovery times are 9 to 75 ns. Maximum full-cycle average forward-voltage drop is 450-mV, and maximum instantaneous forward-voltage drop is 900-mV. Leakage currents range from 50 µA for the 1-A units to 500 µA for the 100-A devices. Maximum surge currents are 10 times greater than rated currents on the 100-A units and 50 times greater on the 1-A devices. The HVE Series chips have peak reverse voltages ranging from 200 to 600 V with the same rated currents, leakage and maximum-surge currents as the HSR chips. Reverse recovery times are 15 to 90 ns. Maximum average forward-voltage drop is 500 mV, and maximum instantaneous forward-voltage drop is 1.2 V.

CIRCLE NO. 356

Filler

It wasn't a miracle, Joyce Lekas of Tektronix informs us, when sharks formed a clear-passage corridor for the patent attorney swimming ashore from his sinking boat. It was professional courtesy.
REFLEX? HERE'S MY REFLEX! IT'S INCREDIBLE! NOW MICRODATA'S UNHOOKING MY DISC MEMORY BUSINESS!

THIS NEW REFLEX DRIVE HAS THE RELIABILITY OF FIXED MEDIA AND THE SPEED OF WINCHESTER TECHNOLOGY AT A LOWER COST PER BIT THAN ANYTHING ELSE ON THE MARKET.

THEY'VE CUT ACCESS TIME WITH FASTER HEAD POSITIONING, FASTER ROTATION AND TWO HEADS PER SURFACE. THERE'S EVEN A FIXED HEAD-PER-TRACK OPTION.

YOU'D THINK THAT WOULD BE ENOUGH. BUT NOT FOR MICRODATA, THEY LOVE TO PILE IT ON. COMPATIBILITY WITH STORAGE MODULE, BETTER RELIABILITY, BETTER PERFORMANCE, COMPACT 7-INCH RACK MOUNT PACKAGE. IT JUST NEVER STOPS.

MY ONLY HOPE IS MAYBE THEY CAN'T DELIVER.

Sorry, Chuck, we're taking orders right now. OEM's should call or write directly to Microdata Corporation, P.O. Box 19501, Irvine, California 92713, Telephone: 714/540-6730.

Microdata

- Unformatted Storage Capacity: 12.5, 376 or 62.7 megabytes
- Bit Density: 5,636 bits/inch
- Data Transfer Rate: 708 MHz
- Rotation Speed: 2964 rpm
- Track Density: 300 tpi
- Position Time: 30 msec avg.
- Track-to-Track Position Time: 6 msec
- Error Rate: Recoverable, 1 bit in 1x10^10 bits; Nonrecoverable, 1 bit in 1x10^10 bits
- MTBF: 6500 hrs.
- Size: 7"Hx17"Wx28"D.


FOR IMMEDIATE USE CIRCLE NUMBER 114
FOR INFORMATION ONLY CIRCLE NUMBER 115

Fast recovery rectifiers handle to 30 A

TRW Power Semiconductor, 14520 Aviation Blvd., Lawndale, CA 90260. (213) 679-4561. $2.48: 1N3899, $3.10: 1N3909 (100-999); stock.

Two series of fast-recovery power rectifiers feature peak-inverse voltages of 50 to 400 V. Series 1N3899 through 1N3903 has an average forward current of 20 A and a reverse-recovery time of 200 ns maximum. The operating temperature range is -65 to 150 C. The 1N3909 through 1N3913 series also has a reverse-recovery time of 200 ns maximum, but an average forward current of 30 A. Both series are JEDEC registered.

CIRCLE NO. 357

Voltage regulators provide low impedance

Semtech Corp., 652 Mitchell Rd., Newbury Park, CA 91320. (213) 628-5392. $6.55 (100 up); stock.

Mini-stud, types MY6.8 through MY120—a series of voltage regulators—offers low dynamic impedance and good efficiency as voltage regulators. The units also are suited for use as transient-voltage suppressors. Encased in Metoxilite, which makes the units hermetic and rugged, they can handle peak pulse power of 30 W at nominal voltages from 6.8 to 120 V (±5%). The temperature coefficient of the regulators is 0.05 to 0.10%/°C.

CIRCLE NO. 358

Electronic Design 24, November 22, 1976
If we're Number 1, it's your fault.

Computer Products, Inc., is the world's leading manufacturer of encapsulated power supplies. And we owe it all to you, for recognizing the value of:

- "Triple-testing" before delivery to insure reliable performance
- Internal short circuit protection
- 24 month warranty
- Flexibility—single and dual outputs from 3.6V to 28V with output currents from 65mA to 2,000mA.
- Low cost and fast delivery

With 49 models to choose from, chances are we can fill your every need. Like to find out more? Just circle our number on the Reader Service Card, and we'll send you our new Power Supplies catalog. If you just can't wait, give Bill Ford a call at 305-974-5500. He can't wait to send it to you.

Computer Products, Inc.
1400 NW 70 Street, Fort Lauderdale, Florida 33309
(305) 974-5500. TWX (510) 956-9895.

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**LED lamps sealed in metal case**

Hewlett-Packard, 1501 Page Mill Rd., Palo Alto, CA 94304, (415) 493-1501. $15.55: 4787; $17: the other models; (10-99); stock.

In four colors, these hermetically sealed solid-state lamps are designed for high-reliability applications and for protection against RFI panel leakage. The lamps are easily mounted by drilling a 0.323-in. hole (P drill). Mounting hardware includes a lockwasher and hex nut. The metal case is electrically isolated. Three models have a typical forward current of 20 mA. Model 5082-4787 is red with an axial luminous intensity of 1 mcd typical; Model 5082-4687 is high-efficiency red, with 2.5 mcd typical; and Model 5082-4587 is yellow with 2.5 mcd. However, Model 5082-4987 is green with typical operating forward current of 25 mA and axial luminous intensity of 1.6 mcd typical.

---

**Culton's New Quiet Non-Impact Thermal Numeric Printer**

Featuring... ultra quiet operation... seven columns of numbers or six columns of numbers with ± sign... fast paper roll loading... up to four line per second print rate... complete with interface electronics... compatible with all popular digital panel meters.

Introducing Gulton's answer to noisy, complicated mechanical printers. The NP-7 panel-mounting printer requires only one moving part, the paper advance motor, which sends the paper silently beneath a non-impact thermal print head. You'll be pleased at the price, too.

Write or call for detailed catalog.

Gulton Industries Inc., East Greenwich, Rhode Island 02818
401-884-6800 • TWX 710-387-1500

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**3 and 4-A rectifiers reverse recover in 50 ns**

Microsemiconductor Corp., 2830 S. Fairview, Santa Ana, CA 92704, (714) 979-8220. $5.20 to $7.34 (100-499); stock to 2 wks.

Fast, high-voltage 3 and 4-A rectifiers, designated MX2130 to 2160 and MY3130 to 3160, handle from 300 to 600 V. Reverse recovery times for all of these miniature glass-package units is typically 50 ns. The units are hermetically sealed in hard glass cases, are metallurgically bonded and are voidless. Leads are solderable silver, markings are solvent resistant and the cathode band is a contrasting color.
Compact 12-bit s/d converter cuts size, weight by 50%

Not only does the SD402 synchro-to-digital converter offer 12-bit resolution, but it does so at half the size and price of its 12-bit competitors. Developed by Natel Engineering, the unit measures 2.625 x 2.625 x 0.42 in. and costs only $199 in single-unit quantities. It is also, reportedly, the first s/d converter that can operate from a single +5-V supply.

The s/d converter uses a continuous tracking circuit in a Type II servo loop to eliminate lag and zero-velocity error at input rates of up to 8000°/s. Over-all accuracy of the converter checks in at ±15 arc minutes and holds for tracking rates of up to 10,800°/s.

Even though the converter weighs just 3 oz, all inputs are transformer-isolated, and both synchro and resolver inputs are accepted. The standard SD402 is designed for 400-Hz signals and handles 11.8 or 90-V rms for synchro inputs, 11.8, 26 or 90-V rms for resolver inputs, and 26 or 115-V rms for the reference input. The reference input has an impedance of 100 kΩ. For 60-Hz operation, a separate transformer module ($50) is required.

The 12-bit digital output is constantly available, except during the converter-update period (indicated by a converter-busy signal). Updating can be prevented by applying a ZERO to the inhibit line, and the converter can be kept in the hold mode as long as the ZERO remains on the inhibit line.

Some of the SD402's competitors feature higher tracking rates and less power consumption for a price.

The SDCl700 12-bit converter from Analog Devices, Norwood, MA, has an accuracy of ±8.5 arc minutes and a tracking rate of 12,960°/s. It does, however, require ±15 and +5-V supplies and costs $365. But even though the SDC-1700 from Analog Devices requires three supplies, it does draw less power—only 1.1 W vs 1.5 W for the Natel SD402.

Recently introduced hybrid converters, series HSDC-10, from ILC Data Device Corp., Bohemia, NY, provide tracking rates of 36,000°/s and are even smaller than the Natel SD402. However, these hybrids are only 10-bit single-package units and require +15 and +5-V supplies. And they cost $345. For 12-bit resolution, DDC has larger modules in its 522/622 series that start at $395.

In addition to its commercial SD402, Natel offers a militarized version that operates over a -55 to +105 °C range and costs $299 (1 to 24 pieces), as well as 14 and 16-bit converters with slightly larger packages. Natel Analog Devices ILC Data Device Corp. 1410 W. Pioneer Drive • Irving, Texas 75061 214/259-2676

CIRCLE NO. 301

CIRCLE NO. 302

CIRCLE NO. 303

CIRCLE NUMBER 118
Nonlatch multiplying d/a is self-contained

Micro Networks, 324 Clark St., Worcester, MA 01606. (617) 852-5400. $59 (1-25); 3 wks.

The MN3100 four-quadrant multiplying d/a converter is a self-contained, hermetically sealed unit, ready to use. It includes an internal op amp and laser-trimmed resistors, and is guaranteed not to latch up. Linearity is better than \( \pm 0.2 \) LSB from 0 to 70 C and settling time for a full 20-V step is 50 \( \mu \)s. The unit has CMOS inputs, consumes 210 mW of power and is packaged in an 18-pin DIP.

CIRCLE NO. 362

Store 3D display data from a microprocessor

Optical Electronics Inc., P.O. Box 11140, Tucson, AZ 85734. (602) 624-8358. $261 (10-29 qty); stock. The 6711 interfaces with standard 8-bit microprocessors and its recirculating memory stores 256 three-dimensional points, with 8-bit resolution. The device provides three analog outputs representing each of the three mutually perpendicular axes and may be hard-wired directly to the company's Model 6114, 3-D display-generator module. A \( \mu \)P accesses the 6711 as a memory location. The module connects to a \( \mu \)P's 8-bit data bus, or an 8-bit data-output port, and two address lines. In addition the unit requires a strobe or read/write command and sends the \( \mu \)P an execution bit when it is ready to receive a data byte. Programs can be furnished for the F-8, 8080A, 6800, 2650, 1802 and SC/MP \( \mu \)Ps. Interfacing details are also available showing exact connections to the various evaluation kits that use these microprocessors. The module operates from standard \( \mu \)P power (+5 V at 300 mA and -12 to -15 V at 100 mA). It outputs analog currents of \( \pm 1 \) mA max. Data can be written in at random or at any rate up to 1.2 kHz. Information is read-out at 300 kHz. Internal address-counters can be incremented by the \( \mu \)P or left to free run. These address counters simplify addressing by the \( \mu \)P.

CIRCLE NO. 363
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**Whereas:** Raytheon brought you RAYASM, the powerful micro-assembler available on the NCSS computer network,

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**2906** A 4-bit Bus Transceiver with parity—is equivalent to the 2905 but with the addition of an on-chip parity generator/checker.

**2907** A 4-bit Bus Transceiver—similar to the 2906 with the two-way multiplexer at the input to the bus driver register eliminated to allow the device to be packaged in the space saving 20-pin DIP.

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**93415** A 1024 x 1-bit Fully Decoded Random Access Memory—for your high-speed data and control stores.

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For complete details, contact your local distributor or Raytheon Company, Semiconductor Division, Dept. 2900, 350 Ellis Street, Mountain View, CA 94042, (415) 968-9211.

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RAYTHEON
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CIRCLE NUMBER 122
**MODULES & SUBASSEMBLIES**

**FVCs aren't fussy about input shape**

Dynamic Measurements, 6 Lowell Ave., Winchester, MA 01890. (617) 729-7870. Under $40; 10 days.
The 9001 frequency-to-voltage converters accept ragged input waveforms without pulse-shaping. Internal timing makes them insensitive to variations in input waveform duty cycle. They offer standard input-frequency ranges of 100, 20 and 10 kHz, with all units factory-trimmed within 0.4% (max) of full-scale. Typical linearity is within 0.01%, and peak ripple is typically less than 25 mV. Gain tempco is 100 ppm-max. All models operate from a single +15-V supply.

**You choose input code with this micro-TTE**

Telenetics, 4120 Birch St., Suite 109, Newport Beach, CA 92660. (714) 752-8363. $28 (1000 qty); stock to 4 wk.
The 7603-01 telephone-tone encoder (TTE), a 32-pin dual-in-line hybrid, is 0.3 x 0.9 x 1.8-in. You get standard telephone dual-tone multiple-frequency (DTMF) outputs from three logic-selectable input codes: 1-of-16 lines, 2-of-8 lines in a row-column keyboard-type matrix, or parallel binary. The device can be hardwired to generate a four-or-eight-digit telephone number on command. Either a dedicated-line or the input data itself actuates the automatic dialing feature. Positive station-identification can be established for individual stations, seeking access to a computer bank, reporting alarms or sharing a communications voice-channel. Applications for the encoder range from manual-keyboard entry (for standard telephone service) to automatic alarms, repertory dialers, point-of-sale terminals and mobile-telephone signaling. This low-voltage PMOS device uses 3 to 8 V with a non-operating current-drain of 500 µA. Signal-frequency stability over temperature and time is controlled by a quartz oscillator. Harmonic distortion is less than 1%.

**Analog multiplexer settles in 3µs**

Teledyne Philbrick, Allied Dr. at Rte. 128, Dedham, MA 02026. (617) 329-1600. $125 (unit qty).
Model 4550 16-channel analog multiplexer contains digital input buffers, decoder logic, analog switches, and an output buffer amplifier—all in a single package. The multiplexer accepts an input voltage range of ±10 V and has an output accuracy of ±0.01%. The input is overvoltage protected even with no supply voltage to the unit. Digital inputs are buffered with Schmitt-trigger logic and have an overvoltage capability of ±19 V. Output settling time for a 20-V step to ±1 mV is 3 µs maximum, including a 1-µs switching time.
Ise introduces five new ways to make the competition turn green.

Your competition probably already thinks they're using the perfect display in whatever it is they make. Let them keep thinking it. While you prove them wrong with a new Itron display. They're designed to make the competition turn green. Which also happens to be the color of the segments.

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CIRCLE NUMBER 124
Texas Instruments SR-52 Programming power from Texas Instruments. Easy hand held programming for scientists, engineers, students — anyone who works with advanced mathematics. Check these features: 224 program locations, 20 addressable memory registers, 23 preprogrammed key functions, indirect addressing, permanent program storage on magnetic cards.

Texas Instruments SR-56 More power from Texas Instruments. Hand held key programmable calculator. 100 program steps, 5 program levels (up to 4 levels of subroutine may be defined). Easy single step editing. Main features include 26 preprogrammed key functions, 10 addressable memory registers, algebraic logic and 9 levels of parentheses.

PC-100 Lock down printer; for a hard copy of your results; step by step listing of programs, or "debugging" programs. The PC-100 printer may be used with the SR-56 or SR-52.

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CIRCLE NUMBER 125

DATA PROCESSING

Portable programmer has personality


A series-92 programmer, weighing 15 lbs, consists of the M020 master control unit and a plug in PROM personality module, packaged in an attaché case. Using the same personality modules as the company's earlier series 90 PROM programmer, this system can program all major MOS or bipolar PROMs. Prices for personality modules range from $350 to $550. The Series 92 features a 20-mA current loop and is compatible with any terminal, computer or microprocessor development system having this interface. You can use this system to program, list, duplicate and verify PROMs. The duplicate function is controlled by a single pushbutton. Run and fail lights indicate machine status and whether or not a PROM has been successfully programmed. PROMs are mounted into the unit via quick-load, zero-insertion-force sockets. Options include an RS232 interface, a parallel interface and an ultraviolet erase light.

CIRCLE NO. 367

Data set transmits over one mile


A data set accepts serial data and transmits data over one mile of four-wire cable. The unit is called the Nodem, because it is "not a modem." The Nodem generates a balanced-current signal at synchronous or asynchronous rates up to 19.2 kbit/s.

CIRCLE NO. 368

Label reader senses a change in color


A color label sensor, the Model 8010 Omnimek, uses a multi-colored solid-state light source and matched detector. The unit can detect all colors including green or blue. In operation, a background color reference is established from the surface under inspection. When the color changes as the unit scans, an output is generated. Two separate outputs are provided, one indicating a change from a dark background to a light mark and one from light to dark. Each output is a 5-V digital signal. The sensor-head size of the Model 8010 is 35 x 74 x 48.25 mm.

CIRCLE NO. 369

Numeric-data terminals can be tailored


The 3070A and 3071A numeric-data entry terminals have a set of keys and LED indicators that can be labeled by the user to match special computer programs. The 3070A operates with the manufacturer's computers, and the 3071A connects to other type computers. Both models have numeric-only keypads and 16-digit displays. The 3070A can also connect to an industry-standard bus, the HP1B. The terminals weigh 10.3 lb and measure 10.9 x 4.6 x 15.7 in.

CIRCLE NO. 370
New unique design
OAK rotary switch

Accurate.
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Up to 60 positions.
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Low cost.

The Oak Communicator Series switch features a patent-applied-for rotor design for long-term contact registry and integrity. Programming is accomplished on a metal-clad, laminated rotor of exclusive construction.

High dependability is assured because the stationary wiping contacts never touch the insulation surface. Instead, they move from electrically live to electrically inactive metal surfaces. Tracking is eliminated due to Oak's exclusive clean-out grooves and rotor circuit design. In addition, erosion or the formation of particles between contact and insulation surface is drastically reduced.

Intermittent opens or shorts are almost impossible.

Complex wiring problems are eliminated, because all switching logic, wiring and contact arrangements are programmed within the factory-assembled switch.

Small size (1.665 x 1.5 x 0.4), simple construction, accurate registration, and low cost permit the Oak Communicator Series to be adapted to almost any application.

For additional information and specifications, contact your nearest Oak sales office or call 815-459-5000.
DATA PROCESSING

CRT terminal handles APL characters


The 2641A CRT terminal can be switched from APL to ASCII operation. It offers a full 28-character APL set, a 64-character APL overstrike set and a 64-character upper-case Roman set that can be optionally expanded to 128 characters. The terminal's CRT displays the complete APL overstruck characters. It operates either in an asynchronous or synchronous (bi-sync) mode at selectable transmission rates from 110 to 4800 baud. The unit is RS232C-compatible, and transmits synchronous ASCII data point-to-point in character or block mode. A multipoint polling option allows as many as 32 terminals to be connected on the same line. The unit's 5 x 10-in. display has a 24-line by 80-column format.

CIRCLE NO. 371

Memory system requires 1/4 the space of others

Intel Memory Systems, 1302 N. Mathilda Ave., Sunnyvale, CA 94086. (408) 734-8102.

The in-1670 offers up to 4 Mbyte of add-on memory for the DEC PDP-11/70. The system is said to offer four times as much as competing memories in the same amount of space. The memory's cycle and access periods run 750 and 550 ns, respectively. The system includes error correction checking and error logging circuits. All single-bit failures are automatically corrected.

CIRCLE NO. 372

Optical bar-code reader observes from 0.5 in.

Identicon Corp., One Kenwood Circle, Franklin, MA 02038. (617) 528-6500. $400 (single qty).

The Model 515 reads codes printed on badges or envelopes. It is available in two versions, one reading at a distance of 0.25 in., the other at 0.5 in. from the reader's face to the label. The depth of field is greater than 0.125 in. The units resolve bar-to-bar spacings down to 0.008 in. The Model 515 uses a large-area silicon photodetector and a diamond-shaped reading aperture, so that the signal is integrated over 0.3 to 0.36 in. of bar length. This allows the reader to ignore voids in dark bars and spots in white bars. The optical system is sealed by a hard-surface sapphire window. The internal light source consists of infrared LEDs operating at 900 mm. Output is a 100-mV signal at a dynamic impedance of less than 100 Ω. Bandwidth is in excess of 20 kHz. Both gain and offset are adjustable.

CIRCLE NO. 373

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CIRCLE NUMBER 127

ELECTRONIC DESIGN 24, November 22, 1976
Paper-tape reader connects to the PDP-8A
Forte Technology, Inc., 15 Strathamore Rd., Natick, MA 01760. (617) 655-5885. $1195; 30 days.

The Model 400 paper-tape reader connects to the DEC PDP-8A computer. It is interfaced with DEC software codes by an eight-word interface. Six additional words and flags remain on the interface for other data input requirements. The system includes a 150 char/s photoelectric reader, a power supply, cabinet, cable, and the eight-word interface board.

CIRCLE NO. 374

Programmer also simulates PROMs

Electro Design, Inc., 8141 Engineer Rd., San Diego, CA 92111. (714) 277-2471. $3000; 60 days.

The ED6000 simulates and programs TTL-compatible PROMs. The instrument consists of an addressable simulator, a cassette-tape unit and a programmer. Data come either from a hex keyboard having address and data LED readouts, an 8-bit data bus, RS-232 or current-loop driver. A switch controls data transfer between the ED6000 and external circuits through a plug-in cable connected to a 16 to 24 pin socket. Address incrementing is either automatic or manual. Data are accessible in 4-bit increments.

CIRCLE NO. 375

Acoustic-coupler kit fits TI's 733 terminal

Omnitec Corp., 2405 S. 70 St., Phoenix, AZ 85034. (602) 258-8244. $289.32 (1 up); stock.

An acoustic-coupler kit enables Texas Instruments' Model 733 terminal to communicate over phone lines. The kit, called the Model 1733, is installed in 10 minutes. All parts, including modem card, muff assembly and hardware are included.

CIRCLE NO. 376

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**DATA PROCESSING**

**Computer-in-a-cable drives four tape units**

**Computer Automation, Inc., 18651 Von Karman, Irvine, CA 92713.** (714) 833-8830. $300.

A parallel-interface magnetic-tape intelligent cable (MTIC) drives up to four phase-encoded (PE) or nonreturn-to-zero (NRZ) magnetic-tape units. The MTIC is used with the manufacturer's distributed I/O system and an external-tape formatter. The unit incorporates microprogrammed control using a self-contained processor that supports standard magnetic tape-drive control functions. The functions include transfer, device protocol, device status monitoring and interrupt generation. The control processor is embedded in a 6-ft cable near the tape formatter, and mounts to any flat surface by screws or adhesive. The formatter is compatible with standard tape speeds up to 75 in./s, with densities from 290 to 1600 char/in., and with seven or nine tracks.

**Interface unit relays data at 1-Mbaud rate**

**Computrol Corp., Berkshire Industrial Park, Bethel, CT 06801.** (203) 792-4060. $300; 120 days.

The Model CCI-4000 transmits data over coaxial cable at a 1 mega-baud rate. The unit connects to a 16 or 32 bit-per-word computer, or peripherals. Up to 64 CCI-4000s, each having a unique address, can connect to one cable. The unit accepts data in the form of two 16-peripheral characters, each having a unique address, can connect to one cable. The unit accepts data in the form of two 16-peripherals. Up to 64 CCI-4000s, bit words, then serializes these data and formats them into a 32-bit word. Current drivers couple the serial data into the coaxial cable. In a network, one computer initiates data transmission through its own CCI-4000. When another unit recognizes its address it transfers the received data to its own associated computer. Optional peripheral-driver boards can also plug into a CCI-4000. One board drives eight individually-addressable peripherals and costs $795. Up to five peripheral-driver boards may be installed in a CCI-4000.

**Printer head moves under software control**

**Practical Automation Inc., Trap Falls Rd., Shelton, CT 06484.** (203) 929-5381. $200-up (single qty); 6 wk.

The DMTP-6 series printer makes the ASCII set of 64 characters. The printer-head movement is under software control. Both the pitch of 8, 10 or 12 character/in. and character enhancement can be programmed. Characters are formed by a $7 \times 5$ needle matrix that forms characters with dimensions of $0.110 \times 0.08$ in. Three models of the series take rolls of paper having widths of 3.438, 6 or 8 in. Other models accept fanfold paper. The units print, on ordinary paper, one to five copies. The paper advances with a programmable motor or ratchet mechanism, depending on model. The effective print rate is 120 char/s. Input is via eight-bit parallel characters, through serial RS-232C or 20-mA current loop.

**Minicomputer has a standard adapter port**

**General Robotics Corp., 57 N. Main St., Hartford, WI 53027.** (414) 673-6800. $4995 (5-9); 30-45 days.

The GRC11/03 central processor has the DEC LSI-11 microcomputer module, and a PDP-11 Unibus adapter port. The GRC11/03 includes the extended instruction set, floating-point arithmetic, 20-k words of RAM, memory addressing capacity of 512-k words and a serial I/O module with switch selectable data rates. It also has a pseudo switch register accessible with software or ODT, and eight additional dual-height module slots.
Solderless breadboards easily handle 600-mil DIPs

Continental Specialties Corp., 44 Kendall St., P.O. Box 1942, New Haven, CT 06509. (203) 624-3103. Unit-qty prices: $9.95 (300); $10.95 (600); stock.

Solderless breadboards never seem to have enough tie points when you design circuits with 600-mil wide DIPs. To solve this problem, Continental Specialties developed the Experimentor 600, a solderless breadboard with 550 tie points and 600-mil center spacing.

Although many of the older 300-mil center solderless breadboards offered at least as many tie points, about 30 to 50% of these points were of no use since the 600-mil-wide DIPs covered them. On the old sockets only one or two tie points for each DIP lead were available; with the Experimentor 600, four points for each pin are available.

There are two versions of Continental Specialties' breadboard available: the Experimentor 600 and the Experimentor 300. Both have a thickness of 0.375 in. and a length of 6 in., but the 600 has a width of 2.4 in. while the 300 is only 2.1 in. wide. The 300 has a 0.3-in.-wide center channel and the 600, a 0.6-in.-wide channel.

Sockets can be snapped together and mixed or matched to provide optimum configurations for any circuit breadboard. Both models also have two 40 point power busses.

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For complete data write: HOFFMAN ENGINEERING COMPANY Division of Federal Cartridge Corporation DEPT. ED652, ANDOKA MN 55303

Hoffman ELECTRICAL ENCLOSURES
Thermocouple connector features small size

Omega Engineering, Inc., Box 4047, Stamford, CT 06907. (203) 359-1660. $3.70 per pair (1-10); stock.

The SMP series of thermocouple connectors is claimed to be the smallest quick-disconnect thermocouple connector available. The series comes in 10 different thermocouple calibrations, including tungsten-rhenium. Each connector consists of male and female mates, with insulation of glass-filled nylon. The connector takes fine-gauge thermocouple wires and protection tubes. Tube clamps are not required because each male connector is supplied with several different-sized brass bushings to which protection tubes can be soldered or braised.

CIRCLE NO. 381

... in new combination plastic film models, offer extremely low temperature coefficients in a miniature 100 and 200 VDC line. This unique combination material results in a lower priced capacitor than the polycarbonate units now used in low TC applications. For higher voltage units, consult the factory. Get complete information on these unique capacitors from Electrocube, 1710 So. Del Mar Ave., San Gabriel, CA 91776; (213) 573-3300.

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CIRCLE NUMBER 131

Digital micrometer resolves 0.0001 in.


The CM-400-D digital micrometer displays displacement data directly in inches. It permits the operator to resolve changes in displacement to ±0.0001 in. Front-panel indicators monitor the status of the control circuitry, warn of over, within or under a set tolerance reading. System accuracy is 0.25 to 1.0%, full scale, depending on the transducer used. It can be interfaced with computers or remote data printout systems. A front-panel potentiometer provides a ±2% full-scale vernier adjustment to calibrate the system to standard gauge-block references. For $1295 you get the readout unit, one transducer, stand, mounting adaptors and test points.

CIRCLE NO. 382

Paper-like ceramic resists 2300 F

Cotronics Corp., 5008 Ave M, Brooklyn, NY 11234. (212) 531-9376. Prices: $122 (0.02 in., 400 ft²), $126 (0.04 in., 250 ft²), $124 (0.08 in., 120 ft²).

The 300 series of ceramic paper has a melting point of 3200 F. The paper can be used to 2300 F. It is made from high-purity refractory fibers containing no asbestos. It can be cut with ordinary hand scissors and formed into complex shapes. The ceramic paper can be folded, wrapped or rolled. The paper comes in thicknesses of 0.020, 0.040 and 0.080 in. Rolls of the material are 24 in. wide.

CIRCLE NO. 383

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CIRCLE NUMBER 132

AUTHOR'S GUIDE

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Circle No. 250

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CIRCLE NUMBER 133

223
PACKAGING & MATERIALS

High voltage bushings operate in a vacuum


A line of insulating bushings is specified for high-vacuum use. They leak at a rate less than $1 \times 10^{-6}$ atm/cc/s of helium. The bushings are open-ended with gaskets having voltage ratings from 10 to 100 kV rms. Flashover is 25% above rated voltage, and all units leak less than 5 pC. The bushings operate continuously at 150°C and intermittently to 200°C. They have either porcelain insulation and stainless steel conductors, or high-alumina ceramic with nickel-iron conductors. For the 50-kV bushing, part no. 947-B-9373-1, the 10-up price is $38.

CIRCLE NO. 384

DIP-socket board has a card-edge connector

Garry Mfg. Co., 1010 Jersey Ave., New Brunswick, NJ 08902. (201) 545-2424. $120 (1-4); 2-4 wk.

A series of wire-wrapable boards comes with 60 DIP positions and a 61-pin card-edge connector. Designated the EP120 series, the boards are constructed of 0.125-in. glass epoxy. The boards also have 2-oz solder-plated copper voltage and ground planes. Options include one, two, or three-level wrapped-wire posts, 14 or 16-pin positions, and voltage and ground sockets. Each DIP position can be provided with a socket for a decoupling capacitor. The socket terminals may have 10, 30, 40 or 100 µin. of gold plating, over 50 or 100 µin. of ductile nickel plating.

CIRCLE NO. 385

PC cards hold up to 50 wafer probes

Probe-Rite, Inc., 2725 Lafayette St., Santa Clara, CA 95050. (408) 249-1255. See text; stock to 2 wk.

The P50 probe-card series holds semiconductor-wafer probing and holding fixtures. The series contains four basic cards and each card holds 50 individual probe points. The P50 series cards are fabricated on white laminate for photon shielding. They contain die stepping, serialization and product identification. Either 48-pin or 110-pin card-edge connectors are available. You may also build your own card to accept three types of wafer-probe point assemblies. Prices run $18 for a blank card to $300 for a complete assembly.

CIRCLE NO. 386

Kit contains 17 types of epoxies


The 51-piece Epoxylab kit contains 17 different epoxy adhesives. The assortment includes fast curing, thixotropic, heat resistant, rigid, low outgassing, steel filled, flexible, high dielectric, low density, low viscosity, high impact, and clear epoxies. Each adhesive comes in an individual package that contains resin and hardener.

CIRCLE NO. 387

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CIRCLE NUMBER 135
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For more information and a free sample, come out of your shell and write or call Sal Mucario, UID Electronics Division, AMF Incorporated, 4105 Pembroke Road, Hollywood, Florida 33021. Telephone (305) 981-1211.
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CIRCLE NUMBER 140

PACKAGING & MATERIALS

IC socket takes wide pin-spacing tolerances

Textool Products, Inc., 1410 W. Pioneer Drive, Irving, TX 75061.
(214) 259-2676. Socket, $2.93-$5.74; receptacle, $4.98-$9.41 (100-up).

The Zip Dip II series consists of disposable zero-insertion-force sockets that plug into chassis mounted receptacles. Each socket features an enlarged entry that accepts a wide range of pin spacing. The IC pins may vary ±0.13 in. from the nominal row spacings of 0.3 to 0.6 in. Contacts in the rows are spaced in increments of 0.1 in. Sockets are available for ICs with 14 to 40 pins. The socket has a typical life of 25,000 to 50,000 IC insertions. A built-in “stop” ensures that the locking handle can’t be overstressed. Top mounted assembly screws facilitate replacing worn internal parts.

PC board is either flexible or rigid

Schoell er and Co., Elektronik GmbH 3552 Wetter, Postfach 20, West Germany.

A multilayer circuit board, called Multiflex, can be made partly rigid and partly flexible. The Multiflex circuits contain flexible printed wiring inside a rigid multilayer PC board. The flexible layer extends beyond the rigid material to provide electrical connections to other PC boards, connectors and controls.
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This patented design holds a film of mercury rather than a fragile glass reed switch. Every operation, the mercury film renews the switch contacts, two spst switches, and two or three external capacitors for the voltage doubler/tripler. Power consumption with the display off is 2 μA typical. Both circuits are guaranteed to operate over a -10 to +60 C range.

Three-terminal regulator series has 7 fixed units

Texas Instruments, P.O. Box 5012, Dallas, TX 75222. (214) 238-2011. $1.38 (100-up); stock.

The 7800 and 7900 series of three-terminal positive regulators are available with seven fixed output voltages. Ranging from 5 to 24 V, the regulators are designed for use in logic systems, instrumentation, hi-fi and other solid-state applications. They are pin-for-pin equivalent to the Fairchild 7800 and 7900 series. The units are housed in plastic TO-220 packages. Regulator features include internal thermal-overload protection, output transistor safe area protection and internal short-circuit current limit.

IC timer has delays of microseconds to hours


The MCC-555 timer circuit, available in a standard 8-lead DIP, acts as either a time delay (monostable mode) or as an oscillator (astable mode). All input-output terminals are TTL/DTL compatible. Resettable time delays ranging from microseconds to hours can be accurately obtained over the single power supply range from 5 to 15 V. The output of the MCC-555 can either sink or source up to 200 mA.
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Electronic Design 24, November 22, 1976

INTEGRATED CIRCUITS

Low cost ARLS works with 75-ns clock

Fairchild Bipolar Memory, 464 Ellis St., Mountain View, CA 94042. (415) 962-3816. $12 (100-up); stock.

An arithmetic logic register stack (ALRS), the 9405A, operates with a 75-ns clock period. It is claimed to be 30 ns faster than guaranteed operating times of the nearest competitive circuits. The 9405A has a two-address architecture, in which addresses are multiplexed to achieve cost advantages that make the circuit the industry's lowest priced four-bit slice, the company claims.

CIRCLE NO. 395

Analog multiplexers handle big overvoltages

Burr-Brown, International Airport Industrial Park, P.O. Box 11400, Tucson, AZ 85734. (602) 294-1431. $10 (100-up); stock.

Monolithic analog multiplexers, the MPC4D and MPC8S, provide input overvoltage protection of up to 20 V above either supply. Channel interaction is eliminated during overvoltage conditions and also during power loss. In addition, the CMOS construction keeps the power dissipation to only 7.5 mW standby and 15 mW operating at 100 kHz. The MPC4D is a 4-channel differential input/output multiplexer and the MPC8S is a single-ended 8-channel device. Both units have access times of 500 ns typical, sampling rates to 200 kHz, and accuracies compatible with 12-bit converter systems. The multiplexers have break-before-make switching to protect input sources. Off-channel isolation is 65 dB typical. The supply range spans ±5 to ±20 V and the input/output range is equal to the supply voltage.

CIRCLE NO. 396
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ELECTRONIC DESIGN 24, NOVEMBER 22, 1976
INTEGRATED CIRCUITS

Bipolar RAMs dissipate only 125 mW but are fast

National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. (408) 737-5832. From $3.73 (100-up) stock.

Low-power bipolar memories with full military capabilities, the DM74LS289 and 74LS189, can handle 16 four-bit words. The random-access memories require only 25 mA maximum input current while maintaining the high speed (35 ns) of the older DM5489D and DM7599D, which they replace. Available with either open-collector (DM74LS289) or three-state outputs (DM74LS189), the RAMs are ideal for scratch-pad applications. Both commercial and MIL-temp-range versions are available.

CIRCLE NO. 397

Dual memory drivers handle up to 600 mA

Fairchild Camera & Instrument, 564 Ellis St., Mountain View, CA 94042. (415) 962-3816. From $2.62 (100-up); stock.

Dual memory drivers, the 55/75326 and 55/75327, can sink or source up to 600 mA and operate from a 5-V supply. The 55326 and 75326 can only sink 600 mA. Their output-transistor base current can be increased by connecting an external resistor. Each output collector is protected from voltage surges during inductive switching by a clamp diode in parallel with an internal pull-up resistor. The 55327 and 75327 memory switches can source or sink up to 600 mA, and operate from one 5-V supply and one 4.5- to-24-V supply. Each switch can function either as a sink driver or source driver. An internal base-drive resistor is available on the chip, and can be used by connecting two pins externally. All memory drivers are available in either ceramic DIPs (55326DM, 55327DM) or military flatpacks (55326FM, 55327FM) for operation over the military temperature range. For commercial use these circuits are available in both ceramic (75326DC, 75327DC) and plastic (75326PC, 75327PC) DIPs.

CIRCLE NO. 398

Monolithic v/f converter operates from 5 to 36 V

Analog Devices, Rte. 1 Industrial Park, P.O. Box 280, Norwood, MA 02062. (617) 329-4700. 100-up prices: $9.50 (J), $13.75 (K); $19.50 (S); stock.

Able to operate from a single 5- to-36-V supply, the AD537 series of voltage-to-frequency converters have typical nonlinearity of 0.05% at 10 kHz. The single-chip converter requires only a single external RC network to set up any full-scale frequency up to 100 kHz and any full-scale input voltage up to +30 V. The converter maintains its linearity even down at low frequencies (0.001 Hz). Over-all tempco of the v/f converter is typically ±30 ppm/°C. A temperature proportional output, scaled to 1 mV/°K, permits the AD537 to also be used as a temperature to frequency converter. The output of the v/f converter is a square wave that can drive up to 20 TTL loads. Quiescent-current drain of the AD537 is only 1.2 mA. On the input is a low drift (1 µV/°C) amplifier that has a 250 MΩ input impedance. There are three versions of the 14-pin-DIP-housed unit: The AD537J, K and S. The J and K are specified for 0- to -70-C operation and the S for -55 to +125 C.

CIRCLE NO. 399

4-k static RAMs run from only a 5-V source

Electronic Memories & Magnetics Corp., 12621 Chadron Ave., Hawthorne, CA 90250. (213) 644-9881. $15.10 (100-up); stock.

Two 4-k static RAMs, the 4801 and 4804, use only one 5-V power source. The devices are configured as 1 k x 4 and 4 k x 1, and both are housed in 18-pin packages. Typical device power at room temperature is 225 mW. Maximum access and cycle time is 450 ns, even at 70 C.
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4. If you need special switch closure programming, DIPSITCH's six independent cams can be factory assembled to perform your programming.

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CIRCLE NUMBER 154

CIRCLE NUMBER 155

ELECTRONIC DESIGN 24, November 22, 1976

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CIRCLE NUMBER 156

233
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INTEGRATED CIRCUITS

CMOS RAMs require only 50 nW/bit

American Microsystems, 3800 Homestead Rd., Santa Clara, CA 95051. (408) 246-0330. From $15.25 (100-up); stock.

The S5101 family of CMOS RAMs is organized as 256 × 4. Standby power required by the RAMs is only 50 nW/bit and only a +6-V supply is needed. The devices are completely static and require no refresh signal. Access time of the 5101s is 450 ns, with other versions available at 650 ns. Outputs of the RAMs are three-state. With the device deselected, current drawn is either 10 or 140 µA, depending on the model. Units are available with guaranteed data retention at power-supply voltages as low as +2 V. The RAMs are housed in 22-pin plastic or ceramic DIPs.

CIRCLE NO. 404

8-bit registers have new package

Advanced Micro Devices, 901 Thompson Pl., Sunnyvale, CA 94086. (408) 732-2400. From $4.30 (100-up); stock.

Three new high-speed low-power eight-bit registers come in a new 20-pin configuration. These low-power, serial-in/parallel-out universal shift-registers are available with either synchronous-or-asynchronous-clear modes and three-state outputs. The low-power Schottky devices (Am25LS23, Am25LS299 and Am154/74LS299) offer four modes of operation—hold (store), shift left, shift right and load data. The Am25LS23 has a synchronous clear function while the Am25LS299 has an asynchronous clear. Both devices have a typical shift frequency of 50 MHz. The Am54/74LS299—pin compatible with a like-numbered TI unit—is a reduced-performance version of the Am25LS299. All three circuits are available in molded and hermetic DIP packages, and are specified for operation over the commercial and military temperature ranges. They undergo 100-percent processing to the requirements of MIL-STD-883.

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CIRCLE NUMBER 157

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POWER-ONE, INC.

CIRCLE NO. 405

ELECTRONIC DESIGN 24, November 22, 1976
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Needs extensive background in core memory organization, circuits and magnetics, and familiarity with logic design. Experience in the design of precise high current, high frequency digital circuits essential. BS/MSEE.

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Requires BS/MSEE and 10 years diversified experience in design & application of digital computers to airborne applications; customer liaison experience; ability to formulate responses to customer requirements as well as satisfactory execution of contractor requirements in a computer development program.

SIGNAL PROCESSING ENGINEERS

Involves analysis and design of Signal Processing-Digital Communications Equipment for avionics plus TDMA and ICN applications. Requires BSEE degree, Master’s preferred, plus 2-5 years experience in communications theory, digital filters, coding theory, signal processing techniques, A/J analysis, error correction, phase locked loops, and related digital and RF hardware design.

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Requires BS/MSEE and 2-5 years experience with the development of FORTRAN programs to simulate electronic systems for signal processing of RF, Baseband, noise, etc.

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CIRCLE NO. 406

Module watches the input line

Calex Mfg., 3305 Vincent Rd., Pleasant Hill, CA 94523. (415) 932-3911. $49; stock to 2 wk.

The Model 829 LineSensor protects equipment against “brown-out” and overvoltage conditions. The module monitors the average value of an ac line voltage and provides a logic-level indication of the out-of-tolerance condition. Also, the unit is sensitive to sudden drops in line voltage. The nominal input is 115 V, 50 to 440 Hz. Other power sources are not needed—the module operates from the line voltage being monitored. Its comparator output is isolated from the input by means of a phototransistor (Model 829T) or by a set of relay contacts (Model 829R).

CIRCLE NO. 407

Stevens-Arnold Inc., 7 Elkins St., South Boston, MA 02127. (617) 268-1170. $160.00 (1-9); stock to 6 wks.

Single-output 25-W low-noise isolated and regulated dc/dc converter modules, the P Series, accepts input levels of 12, 24 or 48 V dc and supplies dc outputs of 5 V, 6 A; 6 V, 4 A; 8 V, 3 A; 12 V, 2 A; or 15 V, 1.6 A. Regulation is ±0.2% max. Output setting accuracy is typically ±0.5%; average voltage is ±0.01%/°C; and stability is ±0.05%/24 h. Sense leads are also provided for point-of-load regulation and the reduction of IR-voltage losses normally experienced when delivering amperes of load current. Power transfer efficiency is 65%; isolation is 1 × 10⁹ Ω min at 500 V dc min; wideband noise is 40 mV pk-pk over a 5-Hz-to-20-MHz bandwidth; and converter switching frequency is 20 kHz and inaudible.

CIRCLE NO. 408

‘Dynamic Variac’ fakes brownouts

Berman Corp., Box 1043, Nashua, NH 03060. (603) 888-1300. 2-3 wks.

Why would anybody want a power source that produces mini-brownouts on purpose? To determine the “ride-through” capability of your product, of course. The PLM103 will deliberately drop from one to 999 half-cycles of line power, if you simply set the desired number on thumbwheel switches. Both manual and automatic operation (0.3 to 5 Hz) are provided. When used in conjunction with the Model CT-50 current transformer, surge current values and waveforms can be measured.

CIRCLE NO. 409
Tenney finds 25 year old working Chamber!

Dick Wagner, Chief Engineer The Triplett Corporation, leading manufacturers of test instruments and panel meters, Bluffton, Ohio accepts contest prize from Bob Schiffman Executive Vice President of Tenney.

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Available off-the-shelf, the new Bowmar TP-3120 thermal printer does a lot more than many of the others for a lot less. With a speed of 1.07 lines per second, this quiet printer continues to maintain its economical advantage by using low-cost, high contrast, non-smear paper. Small in size and cost, yet big in capabilities, it's equipped with such Bowmar quality features as 12 position, dual read-out standard connector, right or left justification and 5x5 matrix design. Other highlights of the new Bowmar TP-3120 include:

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**CIRCLE NUMBER 167**

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**CIRCLE NO. 410**

**Broadband isolators span 2 to 8 GHz**

Western Microwaves, 1260 Birchwood Dr., Sunnyvale, CA 94086. (408) 734-1631. $550 (1 to 9); 30 days.

Covering a frequency range of 2 to 8 GHz, the PMI-2280 series of broadband isolators can handle loads of up to 10 W cw. There are three models available: one unit spans 2 to 2.2 GHz; the next, 2.2 to 6 GHz; and the last, 6 to 8 GHz. Isolation losses are 20 dB for the first two models and 17 dB for the last unit. Insertion losses are 1.25, 1.1 and 1.3 dB, respectively, and the VSWR stays at 1.3:1 for all three models. All isolators have an operating range of 0 to 55 C and measure 3.28 x 2.08 x 1.08 in. (excluding connectors, which are SMA female).

**CIRCLE NO. 411**

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**CIRCLE NO. 412**

**Bandpass filters use YIG tuning at 20 MHz/mA**

Systron-Donner, Advanced Components Div., 735 Palomar Dr., Sunnyvale, CA 94086. (408) 735-9660. From $700 to $1200; stock.

YIG-tuned reciprocal bandpass filters are available in two, three, four, or dual two-stage versions. The SDYF-4000 series covers seven frequency bands from 0.5 through 26.5 GHz. Typical characteristics include an insertion loss of 1 dB (or less) per stage, basic 3-dB bandwidth varying from 3% at 500 MHz to 0.3% at 18 GHz and a skirt selectivity of 6 dB/octave per stage. Typical tuning sensitivity is 20 MHz/mA, while the tuning rate is less than 10 ms/frequency band. Standard packages are 1.45 in. and 1.7 in. cubes, with a maximum weight of 9 and 17 oz, respectively.

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ELECTRONIC DESIGN 24, November 22, 1976

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CIRCLE NO. 426

Heat sinks

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CIRCLE NO. 429

Control panels

"Control Panel Layout Design Guide" discusses such design considerations as operator requirements, environmental considerations, manual controls, visual displays and maintainability, as well as the use of color in panel and control housing, coding and illumination. Micro Switch.

CIRCLE NO. 430

Washers

Flat, shoulder and finishing washers designed to be used with threaded and unthreaded fasteners as spacers, insulators, seats, shims, seals and bearings are listed on a wall chart. Sherman Metal Works.

CIRCLE NO. 431

Triacs and SCRs

A 32-page cross-reference guide indicates the RCA types recommended as replacements for more than 2100 triacs and silicon controlled rectifiers. RCA.

CIRCLE NO. 432

IC sockets

A fold-out easy-to-read selection chart shows each group of Cambion IC sockets. Detailed dimensional drawings as well as part numbers are included. Cambridge Thermionic.

CIRCLE NO. 433

Component parts

Nylon, acetal, polyester and phenolic parts for use in product assemblies are shown in a 16-page design guide. Sample parts are available. Security Plastics.

CIRCLE NO. 434

Relays

An 18-page relay selection guide provides an easy reference for selecting and specifying the right relay for a particular application. Arrow-M.

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Time-delay relays

A 28-page time-delay catalog includes application data, descriptions of delay functions, a glossary of terms and complete specifications, selection guide and dimensional drawings. Magnecraft Electric, Chicago, IL

Computing system

The 2200 portable computing system is described in a four-page brochure. The brochure discusses a variety of optional features and peripherals, and photos and specifications illustrate the capabilities of this system. Wang Laboratories, Tewksbury, MA

PROMs

Features that make TI's Schottky PROM family a low-cost, highly reliable, space-saving solution for system designers are described in a four-page brochure. Texas Instruments, Dallas, TX

Fluoropolymers

Properties and performance of Tefzel fluoropolymers as wire insulation are listed in a 12-page guide. Dupont, Wilmington, DE

Circular connectors

Standard circular connectors designed to MIL-C-5015 are highlighted in a 32-page brochure. ITT Cannon Electric, Santa Ana, CA

Switches

Photos, line drawings, specifications and ordering information on over 300 switches are contained in a 24-page catalog. Chicago Switch, Chicago, IL

Minicomputer

Complete specifications of the GA-16/440 16-bit systems and OEM minicomputer are detailed in a 24-page brochure. Hardware features and options are covered. General Automation, Anaheim, CA

Industrial switches

A well-illustrated, 256-page publication describes position sensing and manual switches designed for pilot duty industrial applications. The catalog is organized into three sections: no-touch position sensing controls; electromechanical position sensing switches and manually operated controls. Micro Switch, Freeport, IL

Security equipment

An informative 64-page guide to alarm equipment application includes alarm system discussion, installation procedures and detailed connection diagrams. Mountain West Alarm Supply, Phoenix, AZ

Linear circuit tester

Testing methods for a wide variety of op amps, comparators, voltage followers and regulators plus other linear ICs are described in a 10-page brochure. The tests are defined and illustrated in block diagrams. GenRad, Concord, MA

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PRD ELECTRONICS

CIRCLE NUMBER 179

246

ELECTRONIC DESIGN 24, NOVEMBER 22, 1976
Rechargeable batteries

Rechargeable nickel-cadmium batteries are described in a 14-page Microprocessor Battery Selector Guide. The guide explains the phenomena of voltage depression—memory—and cell reversal. General Electric, Battery Dept., Gainesville, FL

CIRCLE NO. 446

Connectors

Circular electrical/electronic connectors are covered in a 32-page catalog. The catalog outlines 11 series of connectors and includes military specifications and configuration drawings as well as accessories. Malco, Montgomeryville, PA

CIRCLE NO. 447

Sealed relays

Engineering specifications, outline drawings and mounting information on sealed relays are provided in a 16-page catalog. Arrow-M, Mountainside, NJ

CIRCLE NO. 448

Transistors or chips

Npn small signal transistors or chips are described in a series of six data sheets. Sprague Electric, North Adams, MA

CIRCLE NO. 449

Programmable controllers

Photos, system descriptions and schematics highlight a 12-page programmable-controller catalog. Allen-Bradley, Cleveland, OH

CIRCLE NO. 450

Voltage regulators

A Voltage Regulator Handbook places special emphasis on design techniques. The handbook starts with the basics of power-supply design and covers transformer specification, rectifier circuits and how to specify them, filtering and load effects. To buy this handbook, send $3 (CA residents add 6% sales tax) to the Marketing Services Dept., National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051.

CIRCLE NO. 451

SCR power supplies

Specifications and pricing information on single and three-phase SCR power supplies, ranging from 50 to 10,000 W, are given in a 14-page catalog. Electronic Measurements, Neptune, NJ

CIRCLE NO. 452

μP controller system

The EPTAK microprocessor controller system—designed for process control, machine control and other applications calling for advanced programmable control—is described in an eight-page brochure. Eagle Signal, Davenport, IA

CIRCLE NO. 453

Rental program

A new leasing/rental/instal­­­ment purchase program offered by the 3M Industrial Electrical Products Div. is described in an eight-page brochure. 3M, St. Paul, MN

CIRCLE NO. 454

Ironless rotor dc motor

An illustrated bulletin shows the 9904 120 12601 series of 12-V-dc ironless rotor motors. A specification chart provides essential operating characteristics. North American Philips Controls, Cheshire, CT

CIRCLE NO. 455

μC development system

A four-page brochure describes the Servant-8 microcomputer development system. Logical Services, Mountain View, CA

CIRCLE NO. 456

Data-conversion components

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**Vendors Report**

**Vishay** now stocks its S102-type Bulk Metal precision resistors in all the standard values outlined by the MIL-R-55182 0.5% resistor tables. The resistors are available either immediately from stock or within 10 days at reduced prices.

**CIRCLE NO. 457**

**Fairchild** has set a new pricing range for its 5-V, logic-powered DPMs. Prices for the Model 32 3-1/2-digit meters are $75 (1-49), $71 (50-99), and $67 (100-up). Pricing for the Model 42 4-1/2-digit meters are $119, $110 and $99 for the same quantity ranges.

**CIRCLE NO. 458**

**Intech/Function Modules** has introduced the A-733J, a multiple-function mathematical module, which is a direct replacement for Analog Devices' 433J. The A-733J is priced at $70 (1-24).

**CIRCLE NO. 459**

**Biomation** has reduced prices for its Model 810-D logic analyzer and 810-D accessories. The 810-D has been reduced from $1995 to $1495. Probes for the 810-D have been reduced to $100.

**CIRCLE NO. 460**

**Electro Corp.** has redesigned its line of 5/8-in. thread magnetic sensors. The improvements include integral connector designs, improved magnetic efficiency, a uniform monolithic encapsulation method and fewer internal components.

**CIRCLE NO. 461**

**Monolithic Systems** has reduced the price on its fully hardware and software compatible PDP-11, including the 11/04, MONOSTORE® VII add-in memory system. Single quantity prices are $795 for 4 k x 16, $1075 for an 8 k x 16 and $1350 for a 12 k x 16 system.

**CIRCLE NO. 462**

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**Electronic Design** 24, November 22, 1976
CERAMIC CHIP CAPACITORS. SPLIT-CHIP, is a new concept in ceramic chip capacitor technology. These new units have two broad electrodes on one face and eliminate conventional wrap-around end terminations. This new concept provides lower cost and easier assembly. SPLIT-CHIPS are available in five standard sizes from .040" x .030" to .130" x .090" and .015" thick and in all popular dielectrics and capacitance ranges. JOHANSON DIELECTRICS, INC., Box 6456, Burbank, Ca. 91510 213-848-4465

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RCA FLAMEPROOF FILM RESISTORS. Design engineers prefer them because they won't flame or short under the most severe conditions. These resistors have a 2% tolerance, and are available in 1/4 watt, 1/2 watt, 1 watt, and 2 watt ratings. Resistance values range from 10 Ohms to 1.5 Megohms, depending on wattage rating. 475 film resistors to choose from. RCA Distributor & Special Products Division, Sales Promotion Services, Cherry Hill, N. J. 08101.

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MEMODYNE INCREMENTAL LOW POWER DATA LOGGER Model 2221, is ideal for remote or unattended collection of sporadic measurements. Features 16 channels, 0 to +10 volt analog input, 12 bit resolution, over 2 megabit capacity per 300 foot cassette. Standby current is less than 50 micromamps. Available for line or battery operation. Unit price is $1670.00. Memodyne Corporation, 385 Elliott Street, Newton Upper Falls, Massachusetts, 02164. (617) 527-6600.

New Electronic Gage, Easy To Use. Thickness, Alignment . . . .diameter or deviation measurements, concentricity, orbit tracing, etc. Accuracy up to ± micro-inches (± 0.001 inch), resolution <10 microinches. Utilizes non-contacting inductive measuring techniques—unaffected by oil, grease, or water. Replaces LVDT, air gage, dial indicator, micrometer, $1.995. Ask for information on KD-2602-2S. Kaman Sciences Corporation, P.O. Box 7463, Colorado Springs, Colorado 80933. (303) 599-1500

EC's new Digitally Programmable T-L Logic Delay lines feature Schottky T-L input and output; 15 models with time delays to a max of 255ns; 16 delay steps available with 1 ns, 2 ns, 3ns, 5ns, 10 ns or 16ns resolution; propagation delays fully compensated; 32-pin dip package (.250 high); 4ns max rise time on all delays; 10 T-L fanout; programming by remote switching or automatically by computer-generated data. Engineered Components Company, P.O. Box Y, San Luis Obispo, Ca. 93406 (805) 544-3800

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Free New '76 catalog contains over 34,500 quality power supplies from the world's largest manufacturer, Power/Mate Corp. Power Supplies for every application including submodulars, open frame, vari- rated, encapsulated, laboratory & system. All units UL approved and meet most military and commercial specs for industrial and computer uses. Power/Mate Corp., 514 S. River St., Hackensack, NJ 07601 (201) 343-6294

PRACTICAL DESIGN FOR ELECTROMAGNETIC COMPATIBILITY, ed. by R. Ficchi. A complete guide to elec. compability for electronic systems and equipment, including semiconductor, microelectronic, and digital computer equipment. Numerous charts, graphs, and nomographs. ±0.1%. Universal 115/230Vac inputs from 47 to 440Hz. Single unit prices from $49. STANDARD POWER Inc 1400 So. Village Way, Santa Ana, CA 92705 (714) 558-8512.

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MICROPROCESSOR COURSE 229
P&B CZS-01 Ground Line Integrity Monitor is intended for application where continuous verification of ground line integrity is required. When the potential difference between ground and neutral exceeds 15V rms—due to ground conditions—the CZS-01 contacts open removing power from the system. Power must be manually disconnected and reapplied after the ground fault has been corrected before the output contacts can be closed. Potter & Brumfield Division AMF Incorporated, Princeton, Indiana 47671, (812) 386-1000.

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EC's new Digitally Programmable T'L Logic Delay lines feature Schottky T'L input and output; 15 models with time delays to a max of 255ns; 16 delay steps available with 1ns, 2ns, 3ns, 5ns, 10ns or 16ns resolution; propagation delays fully compensated; 32-pin dip package (.250 high); 4ns max rise time on all delays; 10 T'L fanout; programming by remote switching or automatically by computer-generated data, Engineered Components Company, P.O. Box Y, San Luis Obispo, Ca. 93406 (805) 544-3800.

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